

Edmonton Valley Line West LRT – Noise and Vibration Impact Report

City of Edmonton

Project Number: 60528911

October 24, 2018

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Revision	Revision date	Details	Name	Position
R0	2018-09-21	Original Document	Brian Bulnes	Acoustic Engineer
R1	2018-10-24	Revised to include noise contours	Brian Bulnes	Acoustic Engineer

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Executive Summary

AECOM Canada Ltd. (AECOM) has been retained by the City of Edmonton to update the operational noise and vibration assessment for the planned Valley Line West light rail transit (LRT) system. The proposed line within the study area runs along several major Edmonton roadways from east of Anthony Henday Drive to 101 St. NW. Additionally, eleven Traction Power Substations (TPSS) along the corridor and the Maintenance and Storage Facility (MSF), which includes its own TPSS inside the crew building, were also added to the assessment. The MSF is proposed to be located south of the Lewis Farms Transit Centre.

The proposed line contains both stationary (TPSS and MSF) and transportation (road traffic and LRT vehicles) noise sources. Stationary noise sources are subject to the Edmonton Community Standards By-Law (14600) by-law, while transportation noise sources are subject to the Edmonton Urban Traffic Noise Policy (C506A).

A review of the municipal and provincial guidelines indicated that there were no specific vibration limits for the operation of transportation and stationary noise sources. Similar to many other LRT projects in Canada, limits from the U.S. Federal Transit Administration Noise and Vibration Impact Assessment guide (the FTA guide) were used to assess vibration impacts.

Section 2 of this report corresponds to a stationary noise assessment of the TPSS and MSF within the study area.

The results of the stationary noise assessment indicate that the noise levels at the property lines (assessment location as per by-law 14600) of residential and non-residential locations are expected to comply with the applicable By-Law limits, except east of the MSF doors. However, this land is part of the transportation and utility corridor, and no further development is expected. Therefore, no mitigation is anticipated to be required.

Section 3 of this report summarizes the assessment of predicted noise impacts during operation of the LRT along the project corridor to abutting private back yards (the assessment location as per policy C506A).

Results indicate that noise mitigation should be further investigated for one receptor location (R028). Noise barrier recommendations are provided in Section 3.4, and barrier extents and location can be found in Appendix B2.

Section 4 of the report summarizes the assessment of predicted vibration impacts of the LRT along the project corridor. The vibration assessment incorporates United States Federal Transit Administration (FTA) prediction procedures and criteria.

Results indicate that vibration mitigation is recommended for multiple locations along the proposed corridor. Vibration mitigation recommendations are provided in Section 4.3. Sections of LRT track requiring vibration mitigation are shown on figures provided in Appendix B2. Vibration mitigation is not predicted to be required for the track located at the MSF.

Table of Contents

Exec	utive S	ummary	5
1.	Intro	duction	7
2.	LRT	Operations – Stationary Source Noise Assessment	8
	2.1	Criteria	8
	2.2	Stationary Noise Source Summary	8
	2.3	Points of Reception	8
	2.4	Impact Assessment and Results	g
	2.5	Conclusions and Recommendations	10
3.	Oper	ational Noise Assessment – Transportation Sources	11
	3.1	Criteria	11
	3.2	Assessment Methodology	11
	3.3	Sound Source Data	11
		3.3.1 LRT Operations	11
		3.3.2 Road Traffic Noise	11
	3.4	Impact Assessment and Results	13
	3.5	Noise Barrier Investigation	21
	3.6	Discussion and Recommendations	21
4.	Oper	ational Vibration Assessment	22
	4.1	Guidelines and Criteria	22
	4.2	Assessment Methodology	22
	4.3	Results and Recommendations	23
	4.4	Conclusion	23
5.	Refe	rences	24
Glos	sary		25
Appe	endices		26
Tak	oles		
Toble	. 1. Edr	nonton Community Standards By-law – Part III – Sound Level Limits	c
		se Assessment Results – Stationary Sources	
		se Assessment Results – Standby Generator	
		nparison of Measured vs. Modeled Noise Levels - Existing Conditions	
		se Assessment Results - Transportation Noise	
		se Assessment Results - Comparison of LRT, Road Traffic, and Overall Noise Levels	
		se Assessment Results - Transportation Noise - With Mitigation	
		ration Level Limits	
rable	9: ACC	litional Vibration Sensitive Locations - Recommendations	23

Appendices

Appendix A – Stationary Source Receptor Locations

Appendix B1 – Transportation Noise Receptor Map

Appendix B2 – Transportation Noise Mitigation – Barrier Locations

Appendix B3 – Transportation Noise Contours

Appendix C1 – Vibration Calculations

Appendix C2 – Vibration Mitigation Locations and Discussion

1. Introduction

AECOM Canada Ltd. (AECOM) has been retained by the City of Edmonton to update the operational noise and vibration assessment for the planned Valley Line West light rail transit (LRT) system. The proposed line within the study area runs along several major Edmonton roadways from east of Anthony Henday Drive to 101 St. NW. Additionally, eleven Traction Power Substations (TPSS) along the corridor and the Maintenance and Storage Facility (MSF), which includes its own TPSS inside the crew building, were also added to the assessment. The MSF is proposed to be located south of the Lewis Farms Transit Centre.

The proposed line contains both stationary (TPSS and MSF) and transportation (road traffic and LRT vehicles) noise sources. Stationary noise sources are subject to the Edmonton Community Standards By-Law (14600) by-law, while transportation noise sources are subject to the Edmonton Urban Traffic Noise Policy (C506A).

A review of the municipal and provincial guidelines indicated that there were no specific vibration limits for the operation of transportation and stationary noise sources. Similar to many other LRT projects in Canada, limits from the U.S. Federal Transit Administration Noise and Vibration Impact Assessment guide (the FTA guide) were used to assess vibration impacts.

2. LRT Operations – Stationary Source Noise Assessment

2.1 Criteria

Stationary noise sources in the City of Edmonton are subject to Part III of the Edmonton Community Standards By-Law. Sound level limits are applicable at property lines of residential and non-residential areas for day (7:00AM to 10:00PM) and night time (10:00PM to 7:00AM) periods. Table 1 summarizes the applicable sound level limits.

Table 1: Edmonton Community Standards By-law - Part III - Sound Level Limits

Time Period	Receptor Location	Residential [dBA]	Non-residential [dBA]
Daytime (7:00AM to 10:00PM)	Property Line	65	75
Night time (10:00PM to 7:00AM)	Property Line	50	60

The by-law allows for exemptions during the daytime only for noise sources operating under the following conditions at residential property lines:

- 1. No greater than 70 dBA lasting a total period of time not exceeding two hours in one day;
- 2. No greater than 75 dBA lasting a total period of time not exceeding one hour in one day;
- 3. No greater than 80 dBA lasting a total period of time not exceeding 30 minutes in one day;
- 4. No greater than 85 dBA lasting a total period of time not exceeding 15 minutes in one day;

2.2 Stationary Noise Source Summary

Project related stationary noise sources are predicted to emanate from operations of the eleven TPSS buildings along the project corridor, and the Lewis Farms Maintenance Facility (which includes a TPSS within the crew building).

The dominant TPSS related noise sources are the HVAC units (located on the sides of each TPSS building), and transformer noise breakout through the TPSS walls. Each TPSS location is designed to have an approximately 4.5 metre high wall surrounding all components. Noise emissions from the TPSS buildings were sourced from a recent LRT project located in Canada. Secondary buildings (communication, signal, electrical, and utility rooms) were assumed to only have small comfort heating equipment, and are considered negligible near any TPSS noise.

Stationary noise sources predicted to be included at the Lewis Farms Maintenance Facility include: a compressor, a standby generator (assumption of 400 kW with an outdoor weather enclosure and a residential grade muffler), on-site LRT and bus movement, and indoor maintenance and wash noise intake emitting through the northern bay doors. Noise data was obtained from similar LRT maintenance facility projects located in Canada.

Note that the standby generator is assumed to be tested for a maximum of one hour per day, during daytime hours. As such, the generator was assessed separately from other stationary noise sources as stated in the by-law exemptions mentioned in Section 2.1.

2.3 Points of Reception

The worst case (most exposed and closest) residential and non-residential properties closest to project stationary sources were included in the assessment. As the criteria are property line based, noise contour lines were generated to review all points along respective property lines. Noise receptors were placed at the property line locations with the highest noise contour levels. These receptors are listed in Table 2, along with noise impact levels.

Figures presenting the worst case receptor locations can be found in Appendix A.

Impact Assessment and Results 2.4

The stationary noise sources described in Section 2.2 were used as inputs to the noise impact model. Noise impacts were predicted using the ISO 9613-2 noise prediction algorithm, implemented in the CadnaA modeling package.

The stationary source noise impacts at worst case property line receptors are presented in Table 2. Where a nonresidential receptor was more exposed (closer) to stationary source noise than a residential receptor, the closest residential and non-residential receptors were both assessed. Where a residential receptor was closer, only the residential receptor was assessed, as limits for residential receptors are more stringent. As stationary source facilities (with the exception of the standby generator) are assumed to operate 24 hours a day, the night-time limits were chosen as the overall criteria.

Table 2: Noise Assessment Results – Stationary Sources

Receptor ID	Property Line Type	Closest Stationary Source (s)	With Project Noise Levels [dBA]	Property Line Criteria (Night time) [dBA]	Exceeds Property Line Criteria? (Y/N)
RS1A	Residential	Lewis Farms Maintenance Facility – South End	45	50	N
RS1B	Residential	Lewis Farms Maintenance Facility – North End	47	50	N
RS1C	Non-Residential	Lewis Farms Maintenance Facility – North End	60	60	N
RS1D	Non-Residential ¹ Lewis Farms Maintenance Facility – Eas		74	60	Y
RS2	Residential	TPSS – 86A Ave NW	46	50	N
RS3	Residential	TPSS - 182 St	35	50	N
RS4	Residential	TPSS - 169 St	41	50	N
RS5	Residential	TPSS - 89 St	48	50	N
RS6	Residential	TPSS – 156 St and 94A Ave	46	50	N
RS7A	Residential	TPSS – 156 St and Stony Plain Rd	33	50	N
RS7B	Non-Residential	TPSS – 156 St and Stony Plain Rd	46	60	N
RS8A	Residential	TPSS - 143 St	35	50	N
RS8B	Non-Residential	TPSS - 143 St	43	60	N
RS9	Residential	TPSS – Glendora Cres. NW	43	50	N
RS10A	Residential	TPSS – 123 St and Stony Plain Rd	29	50	N
RS10B	Non-Residential	TPSS – 123 St and Stony Plain Rd	43	60	N
RS11A	Residential	TPSS - 116 St and 104 Ave	17	50	N
RS11B	Non-Residential	TPSS - 116 St and 104 Ave	47	60	N
RS12A	Residential	TPSS - 107 St	38	50	N
RS12B	Non-Residential	TPSS - 107 St	46	60	N

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¹ This land is part of a transportation and utility corridor, and no further development is expected.

As mentioned in Section 2.2, the standby generator was assessed separately from other sources, with an operation assumption of less than one hour per day. Generator noise impact to the nearest property line receptor is presented in Table 3. As a generator location had not been determined as of time of modeling, the generator was assumed to be located next to the maintenance building, conservatively modeled on the closest side to residential receptors.

Table 3: Noise Assessment Results - Standby Generator

Receptor ID	Property Line Type	Closest Stationary Source (s)	With Project Noise Levels [dBA]	Property Line Criteria (Night time) [dBA]	Exceeds Property Line Criteria? (Y/N)
RS1A	Residential	Lewis Farms Maintenance Facility – Standby Generator	66	75	N

2.5 Conclusions and Recommendations

The results of the stationary noise source assessment indicate that the noise levels at the property lines of occupied residential and non-residential locations are expected to comply with the applicable By-Law limits, except for a small area of exceedance east of the maintenance area doors. However, this land is part of the transportation and utility corridor, and no further development or access for recreation is expected. Therefore, no mitigation is anticipated to be required.

3. Operational Noise Assessment – Transportation Sources

3.1 Criteria

Transportation noise in the City of Edmonton is regulated by the Urban Traffic Noise Policy (C506A). The policy provides sound level limits applicable to private back yards abutting the proposed project transportation corridor. The policy sets a 24 hour equivalent sound level (Leq,24hr) limit of 65 dBA for each back yard location. Noise attenuation will be considered for back yards with predicted noise levels exceeding this limit.

3.2 Assessment Methodology

Similar to the approved Environmental Assessment, noise impacts from transportation sources were assessed using the ISO 9613-2 noise prediction algorithm, and TNM (Federal Highway Administration Traffic Noise Model) module for roadway sources, both implemented in the CadnaA modeling package. The noise model was based on the previous Environmental Assessment model produced by Acoustical Consultants Inc., and updated by AECOM in 2013, with the following updates:

- Future LRT alignment + extended length
- Future Roadway alignments
- LRT and roadway elevations
- Updated road traffic volumes(vehicles per hour) for both:
 - Existing conditions (2017)
 - Future "with project" traffic volumes (2047)
- Additional noise receptors
- LRT wheel squeal noise
- LRT crossover noise

3.3 Sound Source Data

3.3.1 LRT Operations

Sound level data for the LRT was sourced from the existing Environmental Assessment, which used measured LRT noise data from existing Edmonton LRT operations, as well as existing LRT operations from Houston, Texas, USA. These measured levels were adjusted for changes in speed along the track alignment. Trains on this line are approximately 80 metres in length, with an average volume of 4.3 trains per hour in the daytime, and 2.6 trains per hour during the night. LRT length, speeds, and alignment were obtained from the design team.

Crossover noise was calculated using the project light rail vehicle (LRV) sound level and applying a correction for crossover noise from the *Nordic Prediction Method for Rail Traffic Noise – NORD 2000* rail noise prediction method. The project crossover noise levels were adjusted for expected duration (accounting for speed, vehicle length, and service frequency) over the assessment period.

The source noise level for wheel squeal was obtained from a measurement of a LRV operated by an Ontario-based transit agency. Similar to the crossover noise, the level was adjusted to account for the expected duration (accounting for speed, vehicle length, and service frequency) over the assessment period.

3.3.2 Road Traffic Noise

Road traffic noise levels were calculated using the TNM module implemented in CadnaA. Only roadways with substantial traffic volumes along and crossing the proposed LRT corridor were modeled. The following parameters were used as inputs to the noise model:

- Volume data (vehicles per hour)
- Traffic speed
- Road gradient
- Road width
- Heavy truck and bus percentages

Existing traffic data was sourced through the City of Edmonton, while future 2047 traffic data was provided by the design team. Future traffic data was provided as peak PM volumes, and was converted to annual average daily traffic (AADT) by multiplying by a factor of 10.

To verify the traffic noise predictions, the noise model was compared with measurements of existing noise levels. Measurements were conducted at several locations along the project corridor during the months of November and December 2017. Receptors were then modeled in these locations, and existing traffic noise levels were calculated at these receptors. The Leq,24hr results for both measured and calculated results were compared and can be found in Table 4.

Table 4: Comparison of Measured vs. Modeled Noise Levels - Existing Conditions

Measurement Location	Measured Noise Level (L _{eq, 24hr}) [dBA]	Calculated Noise Level (L _{eq, 24hr}) [dBA]	Difference [dBA]	Notes
M1	65.3	64.8	0.5	-
M2	57.9	60.4	2.5	-
М3	63.9	65.7	1.8	-
M4	64.5	59.6	4.9	Difference may be due to construction noise across street from monitor (Northeast corner of 142 St NW and Stony Plain Road W intersection).
M5	58.1	59.6	1.5	-
M6	61.9	57.5	4.4	Higher measured level likely due to bus stop located in front of residence (idling and accelerating bus noise).
M7	63.3	58.4	4.9	Difference likely due to noise from nearby swaying metal watering cans in the wind, located hanging on the railing of the resident's porch. Higher ground reinforcement from frozen snow surface is also a potential contributor, as well as bus acceleration noise (nearby bus stop).
M8	62.9	61.5	1.4	-
M9	64.6	61.2	3.4	Slightly higher measured level likely due to rustling tree near monitor. Hard packed snow on the lawn during monitoring may also reflect sound with greater effect than in the noise model.
M10	60	59.9	0.1	-
M11	61.9	59.8	2.1	-
M12	58.8	58.8	0	-
M13	60.3	59.8	0.5	-
M14	60.3	59.3	1	-

Results indicate that the difference in modeled and measured existing traffic noise sound levels are between 0-3 dB at 10 of the 14 monitored locations, which is considered reasonably accurate. Other discrepancies are due to localized and temporary effects. Figures displaying noise monitoring locations can be found in Appendix B1.

3.4 Impact Assessment and Results

Traffic noise levels were assessed at the worst case (most exposed, closest) back yard receptors. Figures presenting receptor locations can be found in Appendix B1.

The noise sources described in Section 3.3 were used as inputs to the noise model. The predicted existing and future (2047) noise impacts at each assessed receptor were then compared with the sound level limit described in Section 3.1. Table 5 presents the existing, future, and change in predicted 24 hour equivalent noise levels at each receptor. Noise contours of the road and LRT 24 hour equivalent noise levels have been generated and can be found in Appendix B3.

A comparison of noise level contributions between road and LRT noise is presented in Table 6. Note that decibels are added logarithmically, not arithmetically (e.g. the overall sound pressure level of 60 dBA and 54 dBA at a certain point will be 61 dBA).

Table 5: Noise Assessment Results - Transportation Noise

Receptor	Existing Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]	Requirement for Noise Mitigation Investigation (>65 dBA)
R001	53.9	52.1	-1.8	No
R002	42.3	42.5	0.1	No
R003	43.2	44.1	0.8	No
R004	41.6	41.1	-0.4	No
R005	59.9	54.9	-5.0	No
R006	56.9	52.9	-4.0	No
R007	61.1	55.7	-5.4	No
R008	63.2	57.2	-6.0	No
R009	65.1	61.4	-3.7	No
R010	56.9	57.3	0.4	No
R011	64.1	59.6	-4.4	No
R012	57.6	59.5	1.8	No
R013	53.3	47.6	-5.7	No
R014	62.8	63.9	1.1	No
R015	64.2	62.4	-1.8	No
R016	58.7	54.9	-3.8	No
R017	56.7	55.6	-1.1	No
R018	58.0	49.1	-8.9	No
R019	65.3	61.3	-4.0	No
R020	66.2	62.1	-4.1	No
R021	65.1	59.7	-5.4	No
R022	65.7	61.8	-3.9	No
R023	53.7	51.5	-2.2	No
R024	59.5	56.2	-3.3	No
R025	58.9	57.8	-1.1	No
R026	62.5	58.3	-4.2	No
R027	61.3	62.4	1.1	No

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Receptor	Existing Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]	Requirement for Noise Mitigation Investigation (>65 dBA)
R028	65.5	66.7	1.2	Yes
R029	62.4	59.5	-2.9	No
R030	54.5	50.6	-3.9	No
R031	54.8	52.6	-2.2	No
R032	63.1	61.0	-2.1	No
R033	60.3	63.3	3.0	No
R034	66.3	63.4	-2.9	No
R035	46.6	44.8	-1.4	No
R036	64.9	60.5	-4.4	No
R037	60.3	56.6	-3.7	No
R038	65.5	61.8	-3.7	No
R039	65.4	61.7	-3.7	No
R040	62.5	58.1	-4.5	No
R041	39.9	42.9	2.8	No
R042	39.2	42.0	2.6	No
R043	40.5	45.0	4.3	No
R044	51.8	54.4	2.6	No
R045	48.4	49.9	1.5	No
R046	52.4	58.8	6.4	No
R047	51.2	56.8	5.6	No
R048	58.7	59.6	0.9	No
R049	58.8	59.2	0.4	No
R050	61.5	61.8	0.3	No
R051	59.6	60.7	1.1	No
R052	52.7	52.2	-0.5	No
R053	59.0	57.1	-1.8	No
R054	44.5	45.1	0.4	No
R055	45.5	44.2	-1.3	No
R056	42.8	42.4	-0.4	No
R057	49.7	51.7	-0.1	No
R058	49.2	50.8	-0.6	No
R059	50.7	52.5	-0.1	No
R060	47.4	49.1	-0.2	No
R061	54.4	44.4	0.0	No
R062	48.8	51.6	0.6	No
R063	53.0	55.8	0.4	No
R064	49.1	53.6	2.8	No
R065	39.2	48.3	8.7	No
R066	48.0	50.6	0.7	No
R067	35.6	45.2	9.5	No
R068	49.6	52.5	2.9	No

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Receptor	Existing Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]	Requirement for Noise Mitigation Investigation (>65 dBA)
R069	34.5	41.7	7.0	No
R070	46.7	51.4	4.6	No
R071	44.6	44.8	0.2	No
R072	46.0	45.1	-0.9	No
R073	57.4	56.7	-0.7	No
R074	57.5	56.5	-1.0	No
R075	46.8	46.0	-0.8	No
R076	47.1	48.1	1.0	No
R077	46.5	51.9	5.4	No
R078	42.0	45.8	4.0	No
R079	40.6	44.3	3.8	No
R080	42.7	46.5	3.8	No
R081	43.6	46.7	3.2	No
R082	40.9	40.8	0.0	No
R083	53.5	57.5	4.0	No
R084	39.8	40.6	0.9	No
R085	53.3	57.8	4.5	No
R086	36.3	39.2	2.9	No
R087	42.5	45.5	3.0	No
R088	47.1	49.6	2.5	No
R089	49.5	51.4	1.9	No
R090	40.2	43.9	3.7	No
R091	34.3	37.8	4.3	No
R092	43.5	45.6	3.2	No
R093	45.4	46.4	2.4	No
R094	59.6	61.6	2.0	No
R095	54.9	56.5	1.7	No
R096	53.4	55.0	1.6	No
R097	59.7	62.1	2.4	No
R098	55.3	56.5	1.2	No
R099	44.5	45.6	1.1	No
R100	56.4	57.3	0.9	No
R101	55.6	56.3	0.7	No
R102	60.6	61.8	1.2	No
R103	57.1	59.4	2.4	No
R104	60.4	63.7	3.3	No
R105	58.4	61.5	3.1	No
R106	57.6	60.6	3.0	No
R107	59.7	64.1	4.4	No
R108	58.3	62.3	4.0	No
R109	59.0	63.8	4.9	No

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Receptor	Existing Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]	Requirement for Noise Mitigation Investigation (>65 dBA)
R110	58.9	63.2	4.3	No
R111	59.3	63.7	4.5	No
R112	59.0	62.0	3.1	No
R113	59.7	62.3	3.8	No
R114	59.1	61.4	2.8	No
R115	59.3	61.4	2.3	No
R116	59.4	61.4	2.3	No
R117	60.4	61.8	1.6	No
R118	60.7	61.4	0.7	No
R119	59.2	61.8	2.1	No
R120	58.3	61.6	1.9	No
R121	55.7	57.6	1.5	No
R122	59.7	63.0	2.5	No
R123	57.3	60.9	2.8	No
R124	57.3	60.7	2.9	No
R125	58.4	61.8	3.3	No
R126	58.4	62.0	3.5	No
R127	59.3	63.7	4.3	No
R128	58.1	62.5	4.4	No
R129	55.8	60.1	4.3	No
R130	56.2	60.5	4.2	No
R131	58.9	61.8	2.9	No
R132	58.6	61.9	3.3	No
R133	58.9	62.4	3.5	No
R134	58.3	62.6	4.3	No
R135	58.1	62.9	4.8	No
R136	58.3	63.2	4.9	No
R137	59.0	64.7	5.7	No
R138	59.4	64.3	4.9	No
R139	57.6	61.1	3.5	No
R140	57.4	61.7	4.3	No
R141	58.7	61.9	3.2	No
R142	59.5	64.2	4.7	No
R143	60.0	63.0	3.0	No
R144	59.5	64.0	4.5	No
R145	60.3	63.0	2.7	No
R146	60.2	62.7	2.5	No
R147	59.6	62.6	3.2	No
R148	57.6	61.7	4.1	No
R1_2018	50.6	52.6	2	No
R2_2018	52.7	52.9	0.2	No

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Receptor	Existing Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]	Requirement for Noise Mitigation Investigation (>65 dBA)
W01	40.5	51.4	10.9	No
W02	44.6	51.7	7.1	No
W03	46.6	52.6	5.9	No
W04	46.8	52.0	5.3	No

Table 6: Noise Assessment Results – Comparison of LRT, Road Traffic, and Overall Noise Levels

Receptor	Future LRT Only Predicted Noise Level (Leq, 24hr) [dBA]	Future Road Traffic Only Predicted Noise Level (Leq, 24hr) [dBA]	Future Overall (Road Traffic + LRT) Predicted Noise Level (Leq, 24hr) [dBA]	Highest Noise Contribution
R001	42.9	51.5	52.1	Road
R002	36.9	41.1	42.5	Road
R003	36.0	43.3	44.1	Road
R004	32.9	40.4	41.1	Road
R005	49.6	53.4	54.9	Road
R006	48.3	51.1	52.9	Road
R007	51.5	53.7	55.7	Road
R008	52.7	55.3	57.2	Road
R009	54.8	60.3	61.4	Road
R010	49.4	56.5	57.3	Road
R011	53.3	58.5	59.6	Road
R012	48.0	59.2	59.5	Road
R013	39.2	46.9	47.6	Road
R014	44.2	63.9	63.9	Road
R015	50.1	62.1	62.4	Road
R016	48.7	53.7	54.9	Road
R017	50.2	54.2	55.6	Road
R018	42.8	47.9	49.1	Road
R019	55.0	60.1	61.3	Road
R020	55.1	61.2	62.1	Road
R021	54.6	58.1	59.7	Road
R022	55.5	60.6	61.8	Road
R023	45.9	50.1	51.5	Road
R024	51.0	54.7	56.2	Road
R025	55.0	54.6	57.8	LRT – near crossover(s)
R026	55.2	55.3	58.3	Road
R027	61.6	54.8	62.4	LRT – near crossover(s)
R028	65.5	60.2	66.7	LRT – near crossover(s)
R029	57.4	55.3	59.5	LRT – near crossover(s)
R030	45.4	49.0	50.6	Road

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	Future LRT Only	Future Road Traffic	Future Overall	
Receptor	Predicted Noise Level	Only Predicted Noise	(Road Traffic + LRT)	Highest Noise Contribution
	(L _{eq, 24hr}) [dBA]	Level (L _{eq, 24hr}) [dBA]	Predicted Noise Level (L _{eq, 24hr}) [dBA]	
R032	58.1	57.8	61.0	LRT – near crossover(s)
R033	62.7	54.1	63.3	LRT – near crossover(s)
R034	58.9	61.5	63.4	Road
R035	40.2	43.0	44.8	Road
R036	56.6	58.2	60.5	Road
R037	51.9	54.8	56.6	Road
R038	55.9	60.5	61.8	Road
R039	55.3	60.6	61.7	Road
R040	53.0	56.4	58.1	Road
R041	27.3	42.8	42.9	Road
R042	36.2	40.7	42.0	Road
R043	37.6	44.1	45.0	Road
R044	42.4	54.1	54.4	Road
R045	40.4	49.3	49.9	Road
R046	57.6	52.5	58.8	LRT – near crossover(s)
R047	55.4	51.2	56.8	LRT – near crossover(s)
R048	53.9	58.2	59.6	Road
R049	52.5	58.1	59.2	Road
R050	53.9	61.0	61.8	Road
R051	53.1	59.9	60.7	Road
R052	43.3	51.7	52.2	Road
R053	44.8	56.9	57.1	Road
R054	40.5	43.2	45.1	Road
R055	32.8	43.8	44.2	Road
R056	34.8	41.5	42.4	Road
R057	46.7	50.0	51.7	Road
R058	45.6	49.2	50.8	Road
R059	47.2	51.0	52.5	Road
R060	44.0	47.5	49.1	Road
R061	39.5	42.7	44.4	Road
R062	47.4	49.5	51.6	Road
R063	51.3	53.9	55.8	Road
R064	47.1	52.5	53.6	Road
R065	46.5	43.4	48.3	LRT – near crossover(s)
R066	44.8	49.3	50.6	Road
R067	44.1	38.7	45.2	LRT – near crossover(s)
R068	50.3	48.5	52.5	LRT – near crossover(s)
R069	39.7	37.3	41.7	LRT – near crossover(s)
R070	50.3	44.8	51.4	LRT – near crossover(s)
R071	37.9	43.8	44.8	Road

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	Future LRT Only	Future Road Traffic	Future Overall	
Receptor	Predicted Noise Level	Only Predicted Noise	(Road Traffic + LRT)	Highest Noise Contribution
	(L _{eq, 24hr}) [dBA]	Level (L _{eq, 24hr}) [dBA]	Predicted Noise Level (L _{eq, 24hr}) [dBA]	
R072	24.5	45.1	45.1	Road
R073	28.7	56.7	56.7	Road
R074	42.1	56.4	56.5	Road
R075	30.6	45.9	46.0	Road
R076	43.2	46.4	48.1	Road
R077	50.1	47.1	51.9	LRT – near wheel squeal
R078	42.8	42.8	45.8	Approximately Equal
R079	38.5	42.9	44.3	Road
R080	43.8	43.2	46.5	LRT – near crossover(s)
R081	34.6	46.5	46.7	Road
R082	31.1	40.3	40.8	Road
R083	52.3	56.0	57.5	Road
R084	33.3	39.7	40.6	Road
R085	52.5	56.2	57.8	Road
R086	33.9	37.7	39.2	Road
R087	32.9	45.2	45.5	Road
R088	45.3	47.6	49.6	Road
R089	45.9	49.9	51.4	Road
R090	38.0	42.6	43.9	Road
R091	32.8	36.1	37.8	Road
R092	38.7	44.6	45.6	Road
R093	38.6	45.6	46.4	Road
R094	49.5	61.3	61.6	Road
R095	46.3	56.1	56.5	Road
R096	45.5	54.4	55.0	Road
R097	49.5	61.9	62.1	Road
R098	46.3	56.0	56.5	Road
R099	32.0	45.4	45.6	Road
R100	47.7	56.8	57.3	Road
R101	40.1	56.2	56.3	Road
R102	47.5	61.7	61.8	Road
R103	47.7	59.1	59.4	Road
R104	51.5	63.4	63.7	Road
R105	48.9	61.2	61.5	Road
R106	48.6	60.3	60.6	Road
R107	49.7	63.9	64.1	Road
R108	49.6	62.1	62.3	Road
R109	50.8	63.6	63.8	Road
R110	50.0	63.0	63.2	Road
R111	50.0	63.6	63.7	Road

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Description	Future LRT Only	Future Road Traffic	Future Overall (Road Traffic + LRT)	Henhant Meles Oc. 4 No. 4
Receptor	Predicted Noise Level (L _{eq, 24hr}) [dBA]	Only Predicted Noise Level (L _{eq, 24hr}) [dBA]	Predicted Noise Level (L _{eq, 24hr}) [dBA]	Highest Noise Contribution
R112	53.8	61.3	62.0	Road
R113	55.9	61.2	62.3	Road
R114	53.0	60.7	61.4	Road
R115	52.4	60.8	61.4	Road
R116	52.9	60.7	61.4	Road
R117	52.5	61.2	61.8	Road
R118	51.8	60.9	61.4	Road
R119	56.6	60.2	61.8	Road
R120	57.7	59.3	61.6	Road
R121	50.4	56.7	57.6	Road
R122	57.6	61.5	63.0	Road
R123	55.4	59.5	60.9	Road
R124	54.1	59.6	60.7	Road
R125	53.0	61.2	61.8	Road
R126	51.0	61.6	62.0	Road
R127	51.0	63.4	63.7	Road
R128	51.4	62.2	62.5	Road
R129	49.2	59.7	60.1	Road
R130	51.0	59.9	60.5	Road
R131	52.6	61.2	61.8	Road
R132	54.1	61.2	61.9	Road
R133	55.8	61.3	62.4	Road
R134	52.0	62.2	62.6	Road
R135	55.4	62.0	62.9	Road
R136	56.7	62.2	63.2	Road
R137	61.9	61.5	64.7	LRT – near crossovers
R138	56.9	63.4	64.3	Road
R139	54.1	60.2	61.1	Road
R140	51.5	61.3	61.7	Road
R141	54.4	61.1	61.9	Road
R142	52.1	63.9	64.2	Road
R143	56.7	61.9	63.0	Road
R144	51.9	63.7	64.0	Road
R145	57.2	61.6	63.0	Road
R146	57.0	61.3	62.7	Road
R147	56.5	61.3	62.6	Road
R148	36.3	61.7	61.7	Road
R1_2018	50.3	48.8	52.6	LRT – near crossover(s)
R2_2018	47.9	51.3	52.9	Road
W01	50.8	42.4	51.4	LRT – near crossover(s)

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Receptor	Future LRT Only Predicted Noise Level (Leq, 24hr) [dBA]	Future Road Traffic Only Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Overall (Road Traffic + LRT) Predicted Noise Level (L _{eq, 24hr}) [dBA]	Highest Noise Contribution
W02	50.3	46.0	51.7	LRT – near crossover(s)
W03	50.6	48.2	52.6	LRT – near wheel squeal
W04	49.4	48.6	52.0	LRT – near wheel squeal

3.5 Noise Barrier Investigation

As presented in Table 5, future transportation noise is only predicted to exceed criteria at one receptor, located at the 136 St. and Stony Plain Road intersection (R028). A noise barrier has been modeled at this receptor, and the results are presented in Table 7 below.

Table 7: Noise Assessment Results - Transportation Noise - With Mitigation

Receptor	Barrier Height (m)	Barrier Length (m)	Future Predicted Noise Level (L _{eq, 24hr}) [dBA]	Future Predicted Noise Level – With Noise Barrier (Leq, 24hr) [dBA]	Change in Predicted Noise Level (L _{eq, 24hr}) [dBA]
R028	1.75	21	66.7	61.5	-5.2

It is predicted that a 1.75 metre high noise barrier will successfully reduce transportation noise at receptor R028 to a level noticeably below the Leq,24hr criteria level of 65 dBA. A figure presenting the noise barrier location and extents can be found in Appendix B2. All other receptors are not predicted to require noise mitigation per the Urban Traffic Noise Policy criteria.

3.6 Discussion and Recommendations

Results indicate that noise levels will exceed by-law criteria at one receptor location. With the recommended noise barrier from Section 3.5 implemented, noise levels at all receptors will comply with Urban Traffic Noise Policy criteria.

Any future planned double boarded privacy fencing (without gaps) from the City should reduce some noise to the yard. However, as privacy fencing of these types can greatly vary (density, height, build); the level of expected improvement is uncertain.

Although the project will comply with applicable noise level limits, please note that the Urban Traffic Noise Policy sets out criteria for a 24 hour noise energy average. When considering this 24 hour average, it was generally found that road traffic (not the LRT) was the controlling source of noise at most back yard locations. This can be seen in many of the receptors along Stony Plain Road east of 139 St. NW where levels are predicted to decrease due to a reduction in lanes and road traffic.

These results can be expected as the average LRT volumes are relatively low over the duration of the 24 hour assessment period (4.3 trains per hour during the day, 2.6 per hour during the night). As shown in Table 6, exceptions to this typically occurred where LRT crossovers or track curvature (potentially causing wheel squeal) were located near a noise sensitive receptor.

It is likely that the LRT will be noticeable at back yard receptors during pass-bys, as the LRT has a different noise characteristic when compared against traffic noise. LRT pass-bys occur as discrete events with a higher peak instantaneous noise level in comparison to road traffic noise which operates more similarly to a continuous flow.

It is also worth noting that while wheel squeal noise is not predicted to be the cause of criteria exceedance at any receptors, wheel squeal noise can especially stand out and irritate nearby residents. Lubrication of wheels is therefore recommended at track curves.

4. Operational Vibration Assessment

4.1 Guidelines and Criteria

A review of the municipal and provincial guidelines indicated that there were no specific vibration limits for the operation of stationary or transportation noise sources (road traffic and LRT vehicles). Similar to many other LRT projects in Canada, limits from the U.S. Federal Transit Administration Noise and Vibration Impact Assessment guide (the FTA guide) were used for this project. The vibration level limits used in this analysis have been presented in Table 8.

Table 8: Vibration Level Limits

Maximum Vibration Velocity Level (VdB²)	Maximum RMS Velocity (mm/s)	Receptor Type
90	0.80	Industrial/Workshop
84	0.40	Office
78	0.20	Residential (Day)
72	0.10	Residential (Night), Operating Rooms

In addition to the receptor types mentioned in Table 8, a number of special case vibration sensitive locations were flagged for investigation. Vibration level limits for special case locations near the project line are dependent on the equipment used at the location. The FTA guide (Section 8.1, Table 8-1) sets out a general assessment limit of 65 VdB for most moderately sensitive equipment (e.g. hospitals with vibration sensitive equipment, university research operations, etc.).

4.2 Assessment Methodology

Vibration from LRT operations on the project corridor and MSF LRT track were predicted using the general vibration prediction method in the FTA guide. Relevant factors affecting vibration at the receptor included:

- Vehicle type (LRT, freight, bus)
- Vehicle speed
- Track conditions (this includes special track work, which is used to implement crossovers, frogs, etc.)
- Type of transit structure (at grade, elevated structure, etc.)
- Soil conditions

The ground was assumed to have efficient soil propagation based on the previous assessment, which noted that much of the soil in the area was clay based. In order to efficiently determine the potential need for mitigation, zones where vibration impact will exceed criteria was calculated for sections of the track based on the above inputs. Where receptors fell within these zones, mitigation was investigated based on distance to the source of vibration.

Additional investigation also took place for the following potentially vibration sensitive locations:

- Misericordia Community Hospital (16940 87 Avenue)
- Insight Medical Imaging Meadowlark (200 156 St NW)
- Insight Medical Imaging West End (9509 156 St NW)
- Insight Medical Imaging (11560 104 Ave NW)
- Stony Plain Road Dental Plaza (149 St. NW and Stony Plain Rd NW Intersection)

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² Reference velocity: 1 micro-inch/sec

4.3 Results and Recommendations

Vibration caused by MSF LRT movement along the site is not predicted to exceed FTA limits at nearby sensitive receptors. However, results indicate that vibration mitigation is recommended for multiple locations on the project LRT corridor. Vibration calculations are presented in Appendix C1, and sections of LRT track requiring vibration mitigation are presented in Appendix C2. To allow flexibility in mitigation design, the required reductions for each section of track are shown in Appendix C2.

Typical vibration mitigation measures and expected vibration reduction include:

- Ballast mats 10 to 15 VdB reduction
- Resilient rail fasteners 4 to 8 VdB reduction
- Resilient supported sleepers/ties approximately 10 VdB reduction
- Booted sleepers/ties approximately 10 VdB reduction
- Tire-derived aggregates 8 to 14 VdB reduction
- Floating slab track with continuous elastomer layer 6 to 12 VdB reduction
- Floating slab track with discrete elastomer bearing 15 to 18 VdB reduction

The effectiveness of specific vibration mitigation measures is dependent on several factors such as the component design, installation techniques, localized soil characteristics, train axle load, and frequencies of concern. For track sections requiring greater than a 15 VdB reduction (crossover locations), moving crossovers to less sensitive locations may be worth considering. A more detailed discussion and further description of LRT vibration considerations and mitigation is provided in Appendix C2.

Table 9 provides investigation results for the additional vibration sensitive locations.

Table 9: Additional Vibration Sensitive Locations - Recommendations

Vibration Sensitive Location	Recommendation (s)
Misericordia Community Hospital	No mitigation required –Low vibration levels due to elevated track section
Insight Medical Imaging – Meadowlark	No mitigation required – Outside of vibration zone of influence
Insight Medical Imaging – West End	Mitigation required – See Appendix C2
Insight Medical Imaging – 11560 104 Ave NW	Mitigation required – See Appendix C2
Stony Plain Road Dental Plaza	Mitigation required – See Appendix C2

4.4 Conclusion

With the vibration reduction recommendations from Section 4.3 and Appendix C2 implemented, the LRT is predicted to comply with FTA guide vibration limits at nearby sensitive locations, and the special case vibration sensitive locations described in Section 4.2.

5. References

- 1. International Organization for Standardization, ISO 9613-2: Acoustics Attenuation of Sound during Propagation Outdoors Part 2: General Method of Calculation, Geneva, Switzerland, 1996.
- 2. City of Edmonton, By-Law Number C506A. Urban Traffic Noise Policy, 2013.
- 3. City of Edmonton, By-Law Number 14600. Community Standards Bylaw, Part III, 2017.
- 4. Federal Transit Administration (FTA), US Department of Transportation, *Transit Noise and Vibration Impact Assessment*, Report No. FTA-VA-90-1003-06. May 2006.
- 5. AECOM, SEtoW Edmonton LRT Preliminary Design Noise and Vibration Report West Line. July, 2013.
- 6. Acoustic Consultants Inc., Edmonton Southeast LRT Noise Impact Assessment, October, 2010.

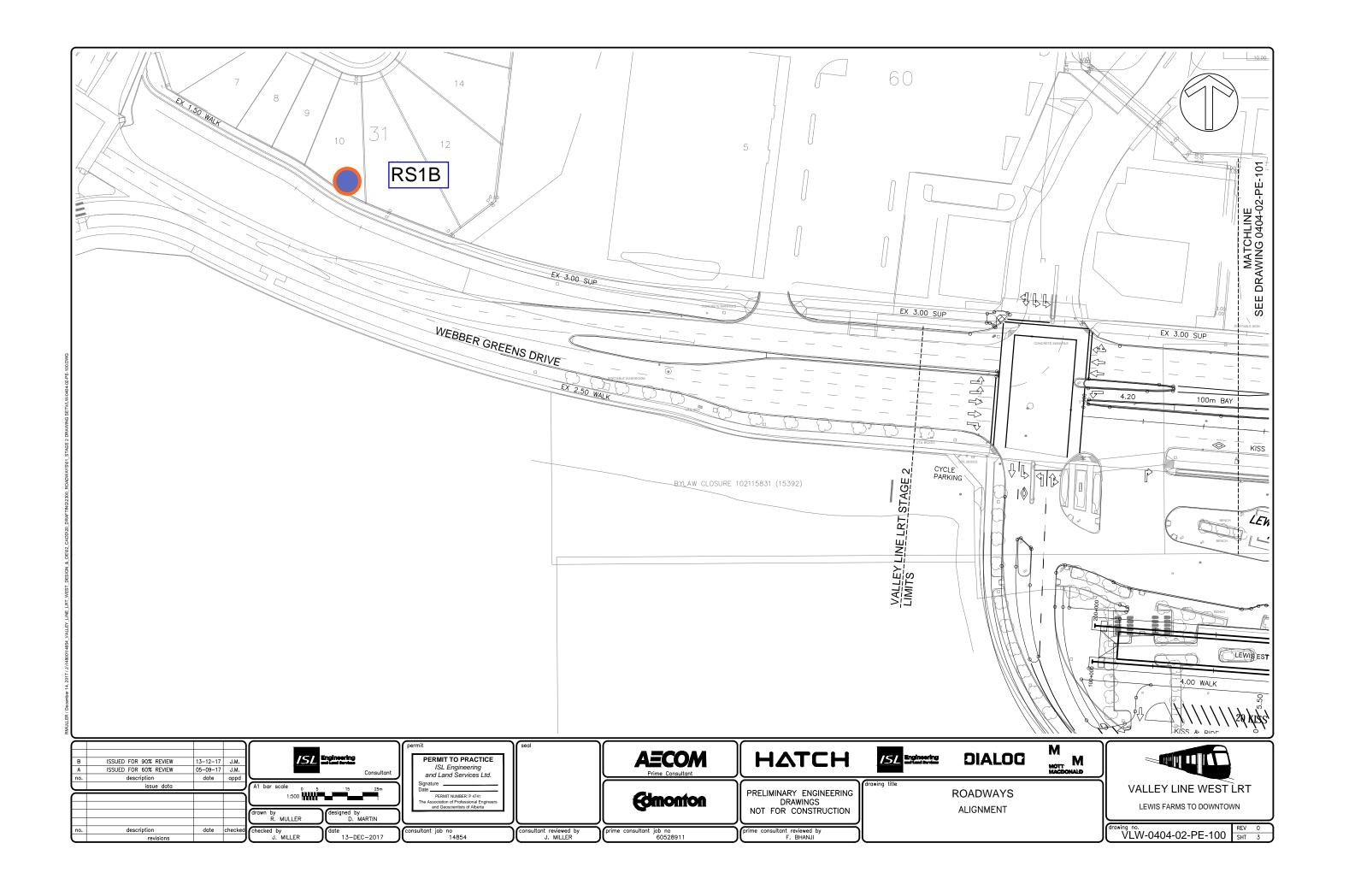
Glossary

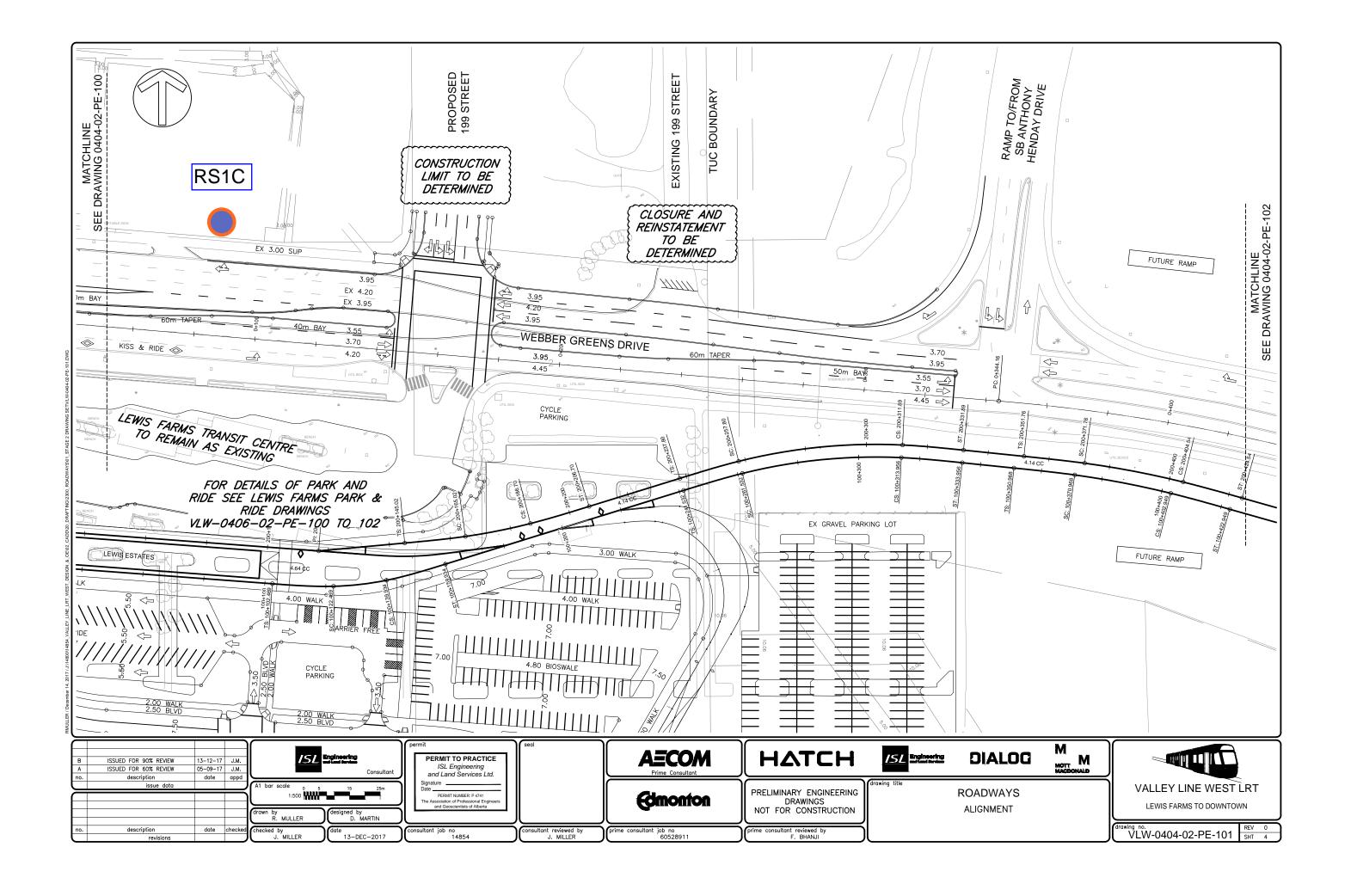
Sound	Pressure wave travelling through a medium, such as air.
Noise	Unwanted sound.
Acoustics	The science of sound propagation and transmission.
Vibration	Oscillation of a parameter that defines the motion of a mechanical system.
Decibel, dB	A logarithmic ratio, not strictly a unit, used to describe sound levels. For sound pressure, the reference level is 20 micropascals (threshold of hearing).
Frequency	The rate at which an event is repeated. Measured in Hertz (Hz), where 1 Hz = 1 oscillation/sec. Normal human hearing extends over a range of frequencies from about 20 Hz to about 20 kHz.
Octave Band	A band of frequencies where the upper limiting frequency is twice the lower limiting frequency. Octave bands are identified by their centre-frequencies. The octave bands standardized for acoustic measurements include those centered at 31.5, 63, 125, 250, 500, 1000, 2000, 4000, & 8000 Hz.
A-Weighting Network, dBA	A frequency weighting network intended to represent the variation in the ear's ability to hear different frequencies. Overall sound levels calculated or measured using the A-weighting network are indicated by dBA rather than dB.
Sound Power Level (PWL, L _w)	A measurement of the total acoustic energy output from a noise source, per unit time. Reported and measured in decibels (dB or dBA), using a reference power of 10 ⁻¹² Watts (0 dB).
Sound Pressure	The instantaneous difference between the air pressure produced by sound and the average barometric pressure at a given location.
Sound Pressure Level (SPL, L _p)	The ratio of the instantaneous sound pressure and a reference sound pressure of 20 μ Pa (0 dB). Reported and measured in decibels (dB or dBA).
L _{eq} - "Equivalent sound level"	Value of a constant sound pressure level which would result in the same total sound energy as would the measured time-varying sound pressure level over equivalent time duration. The $L_{eq,1hr}$, for example, describes the equivalent continuous sound level over a 1 hour period.
Peak Particle Velocity (PPV)	The peak signal value of an oscillating vibration velocity waveform. Can be expressed in mm/s.
Root Mean Square Velocity (RMSV)	The square root of the mean-square value of an oscillating vibration velocity waveform, where the mean-square value is obtained by squaring the value of amplitudes at each instant of time and then average these values over the sample time.

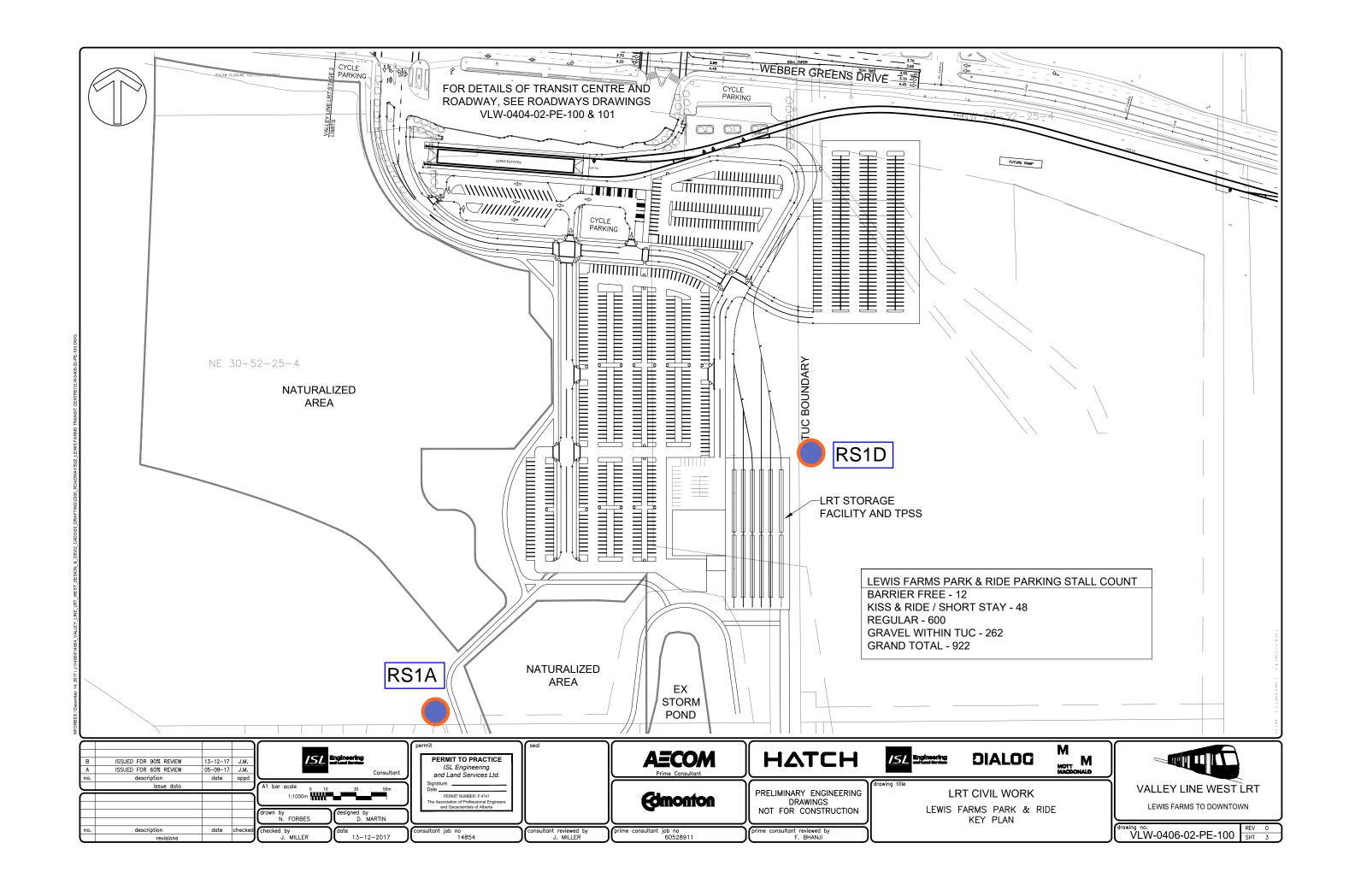
Appendices

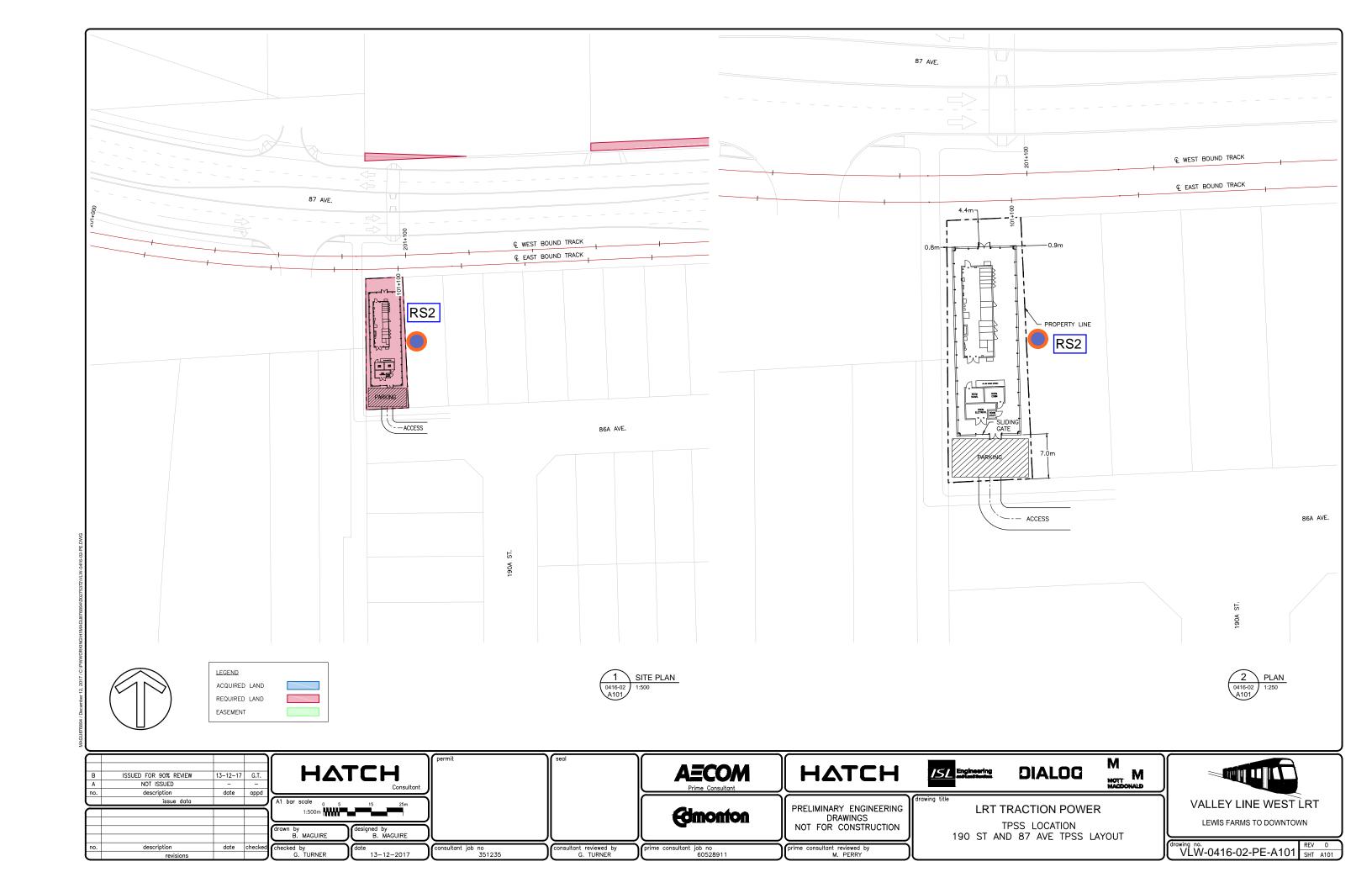


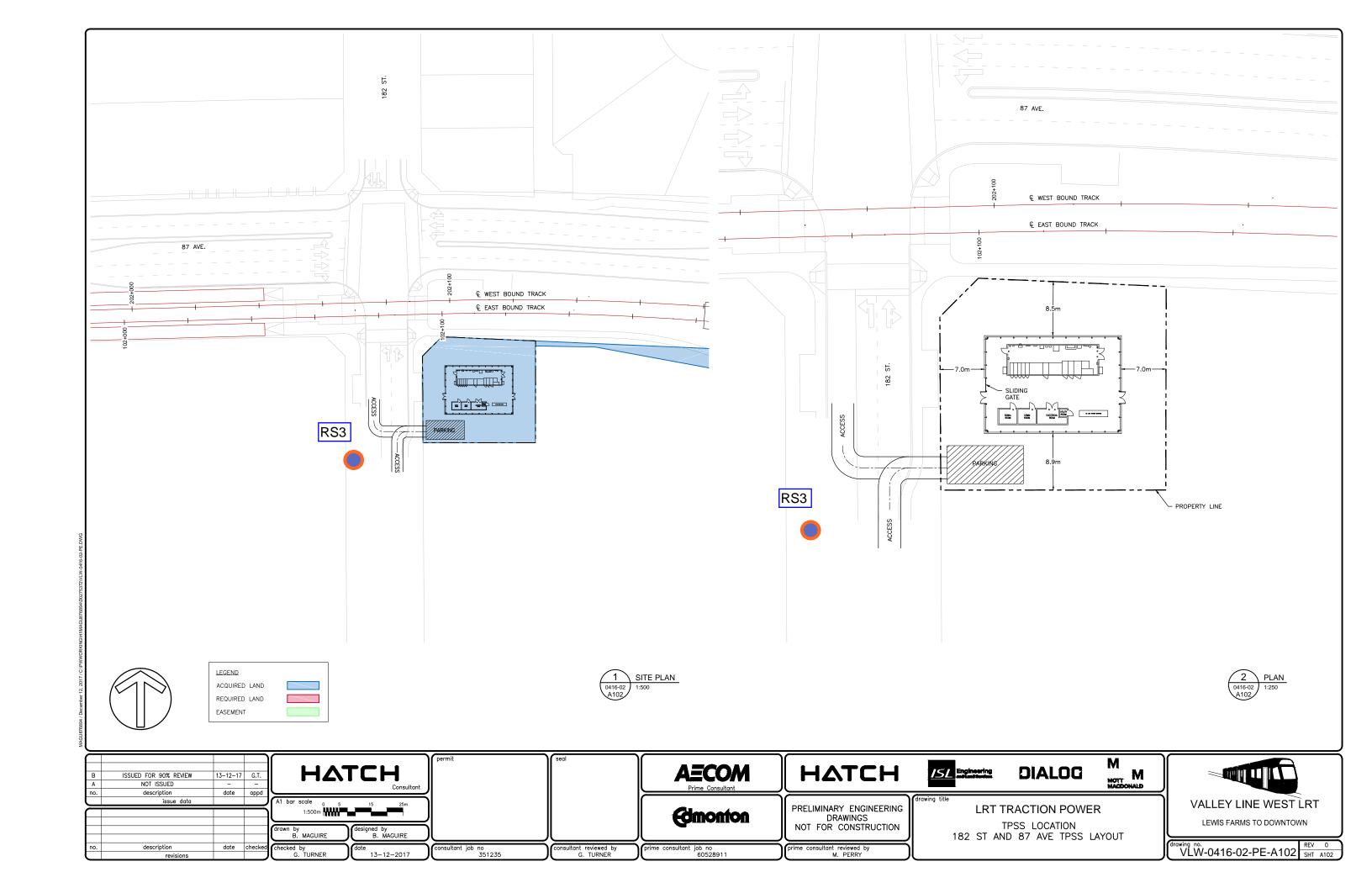
Appendix A Stationary Source Receptor Locations aecom.com

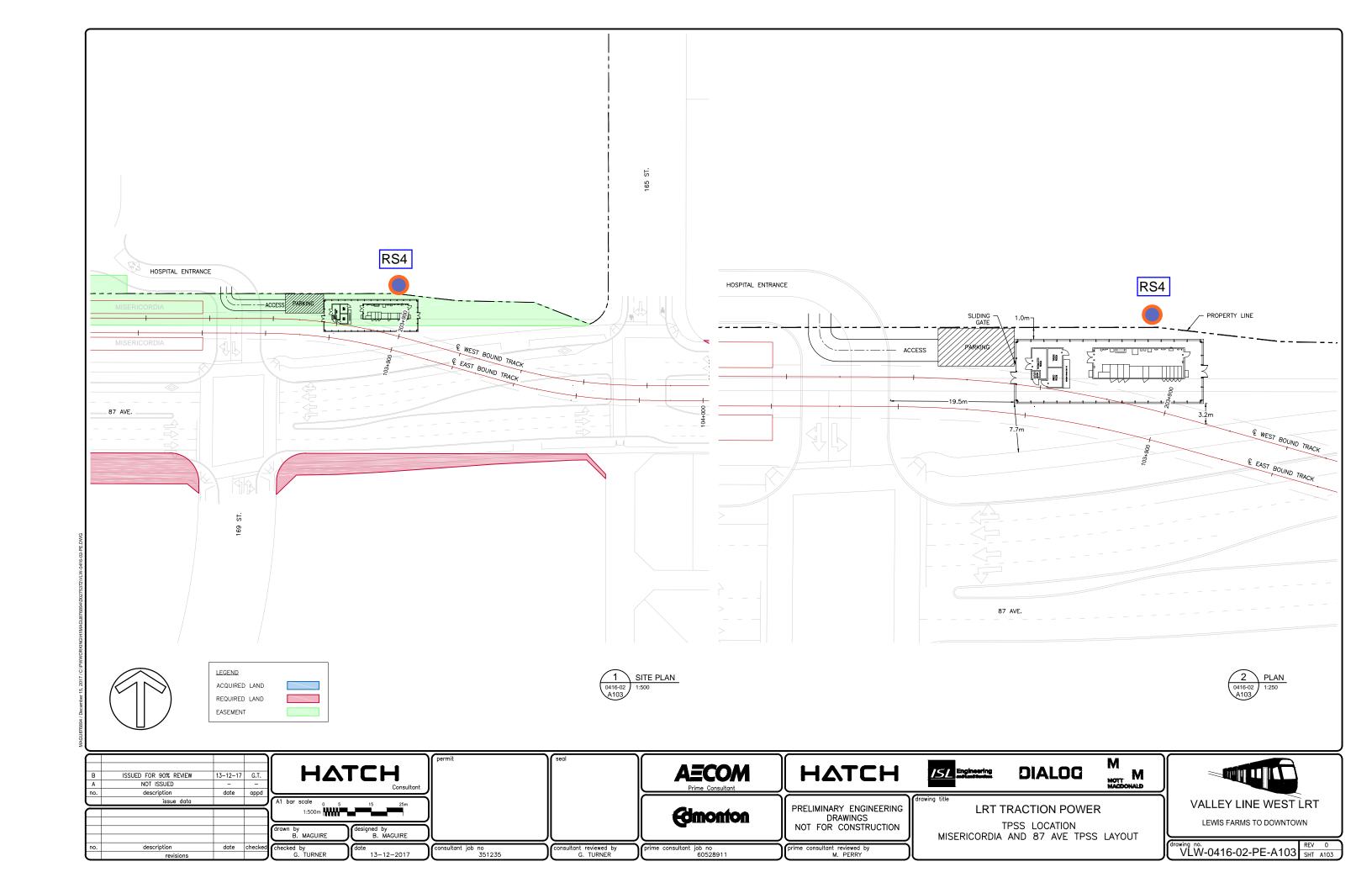


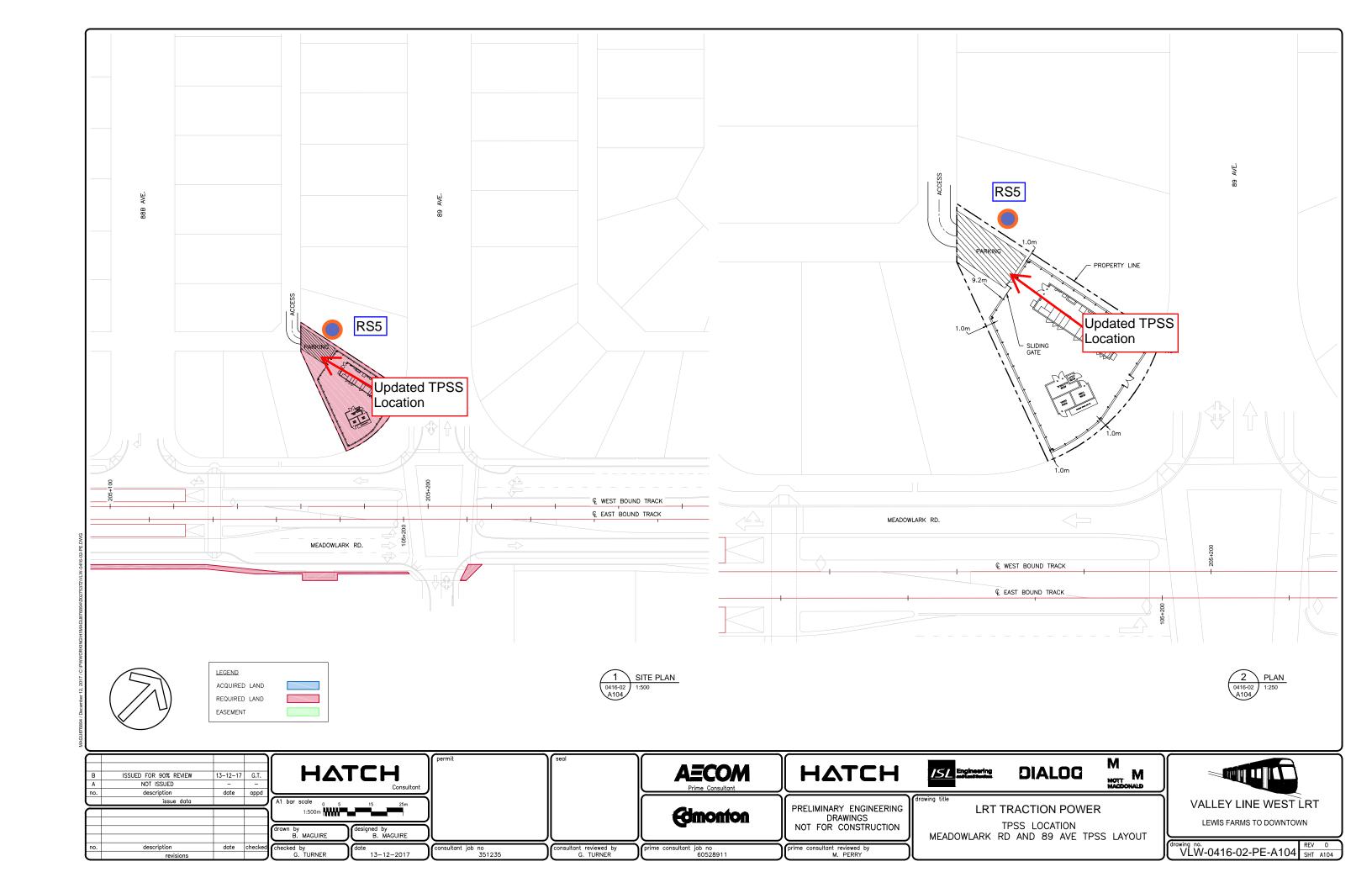


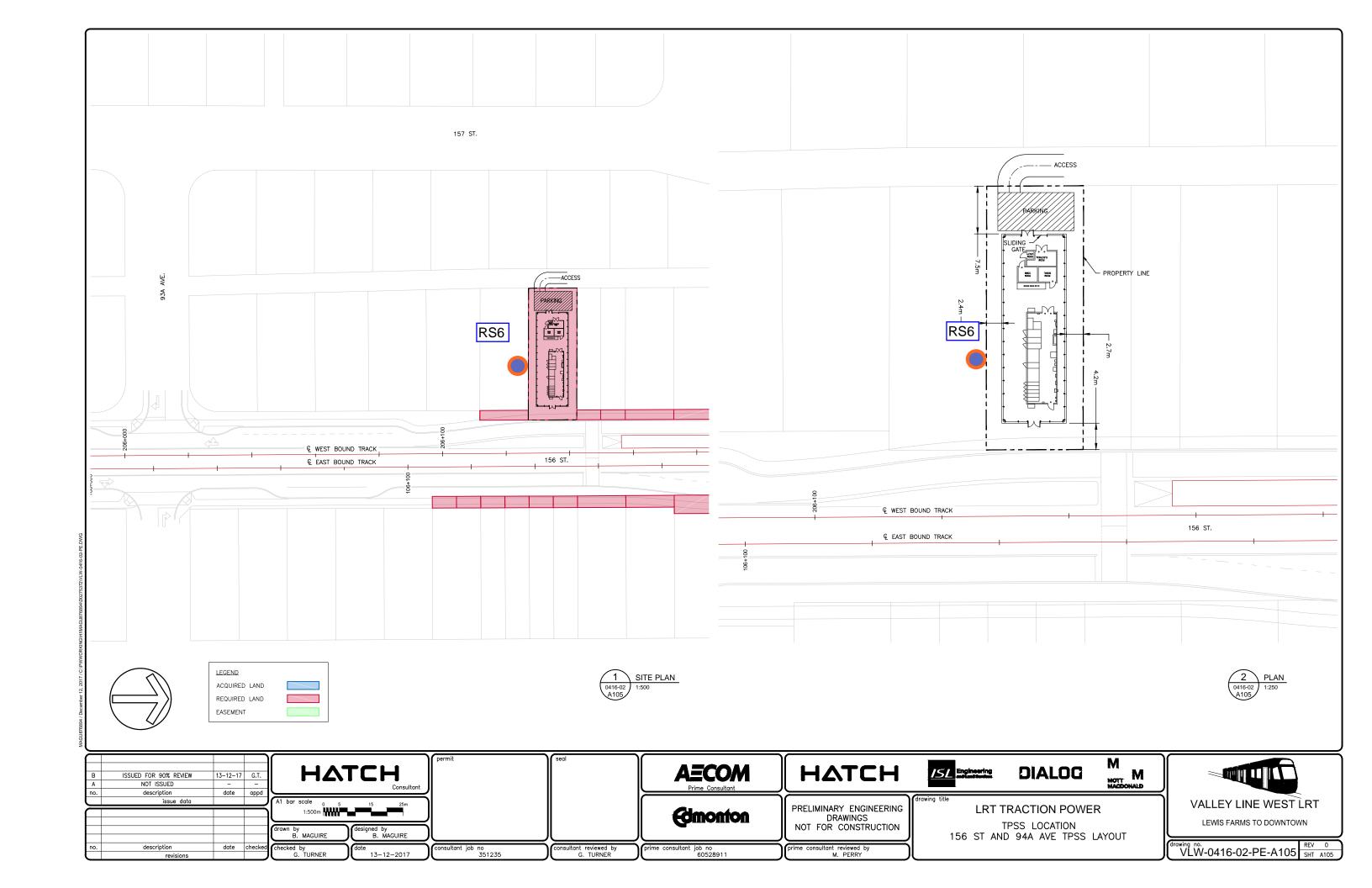


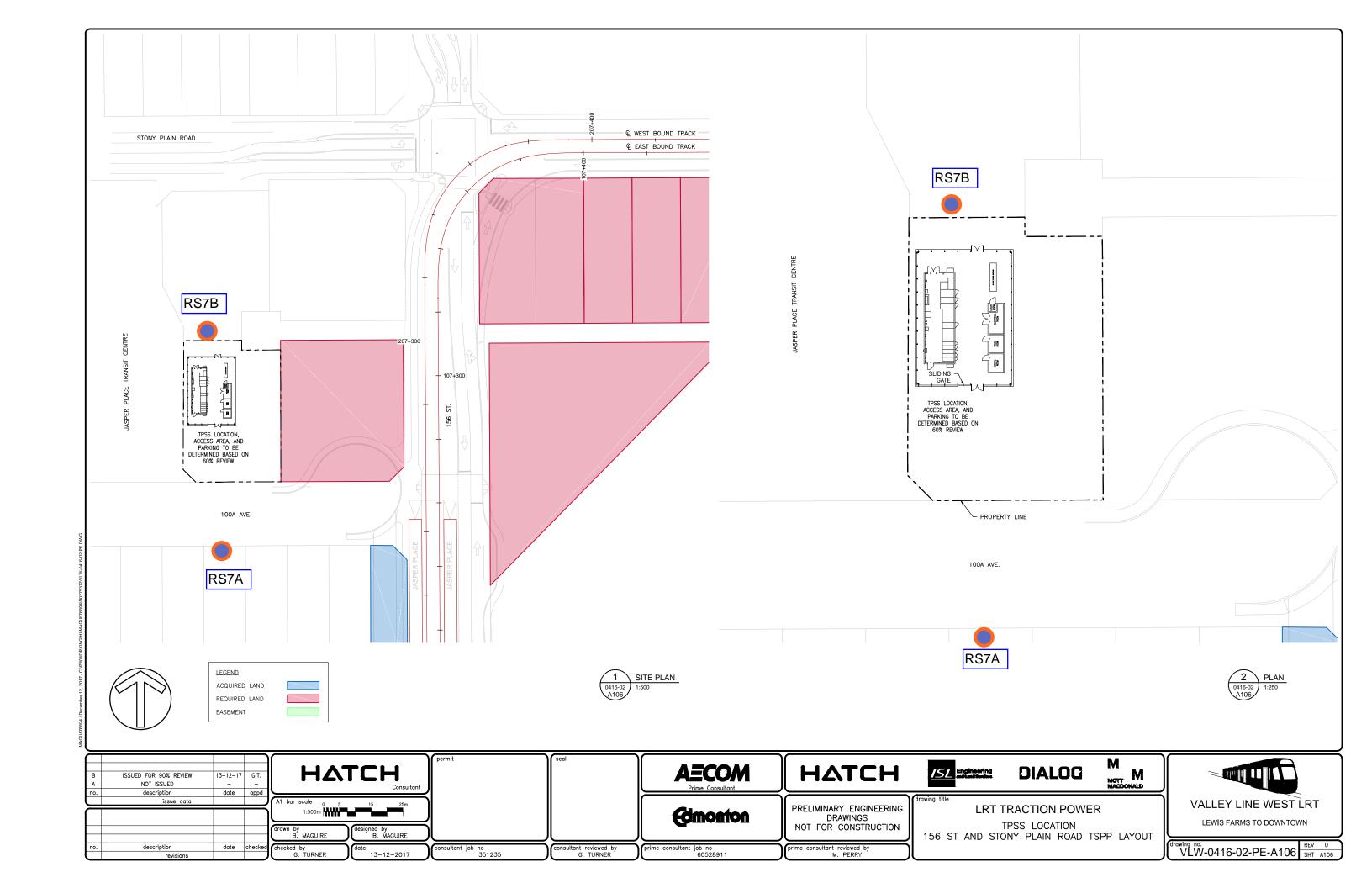


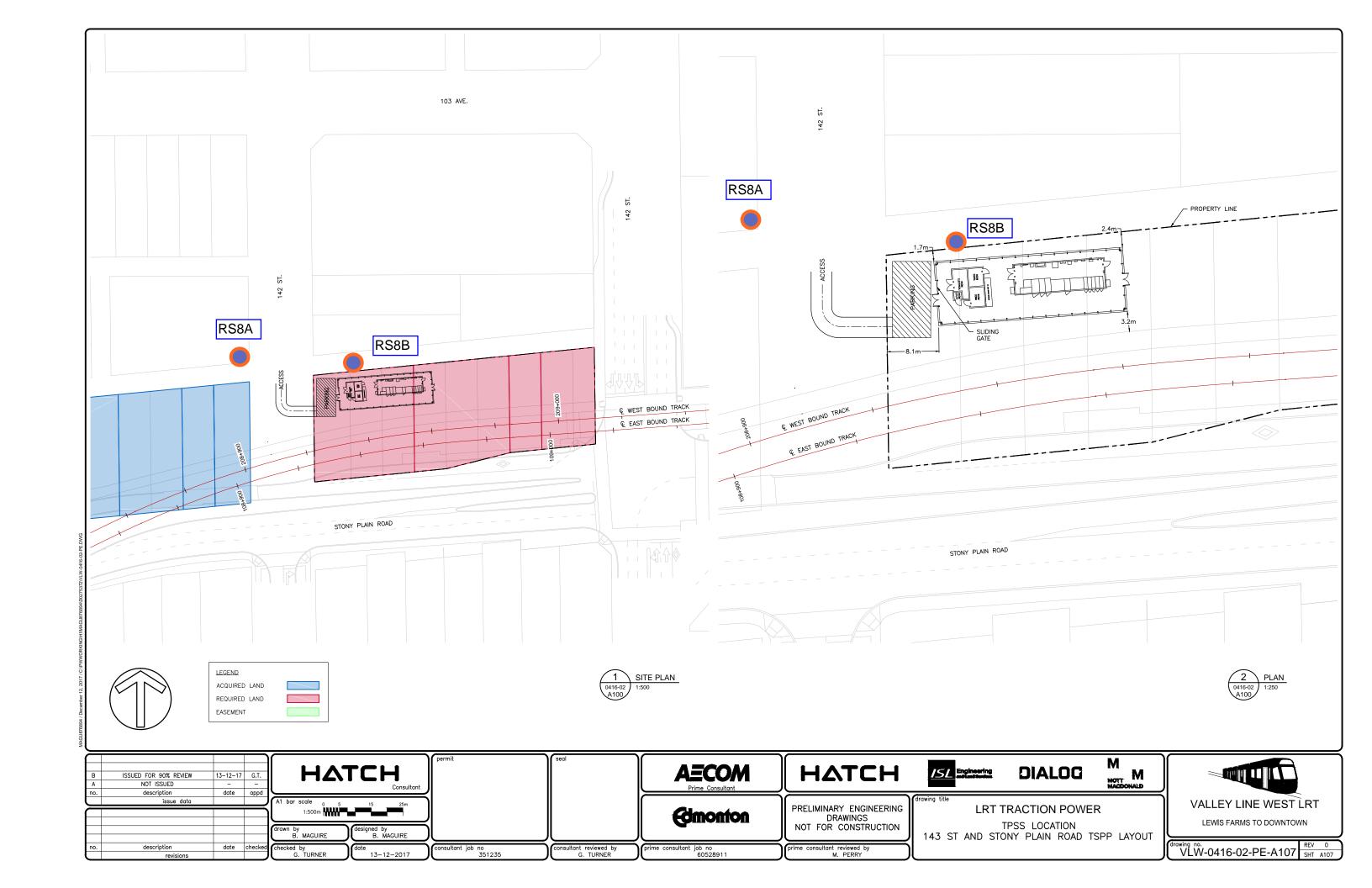


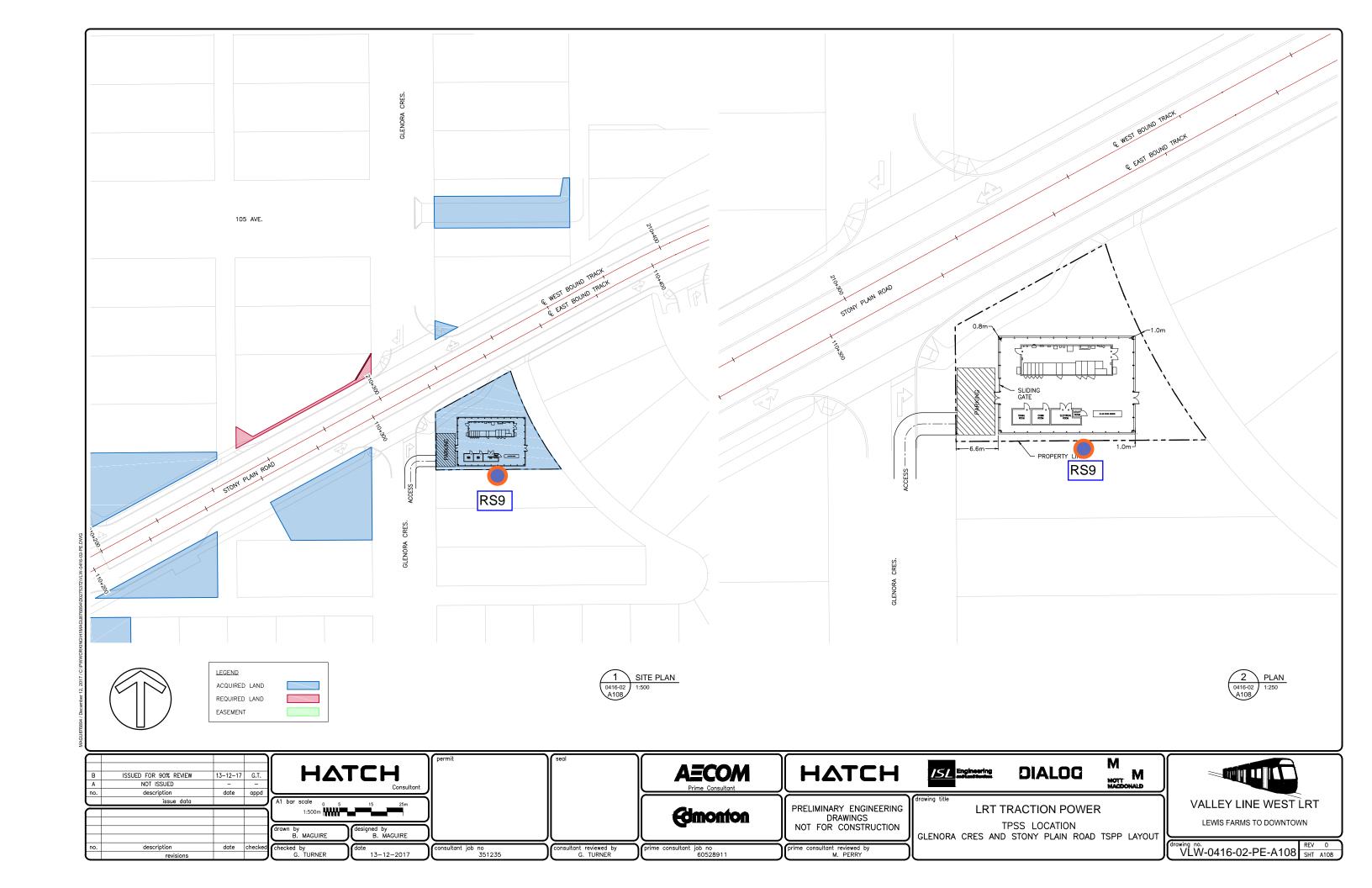


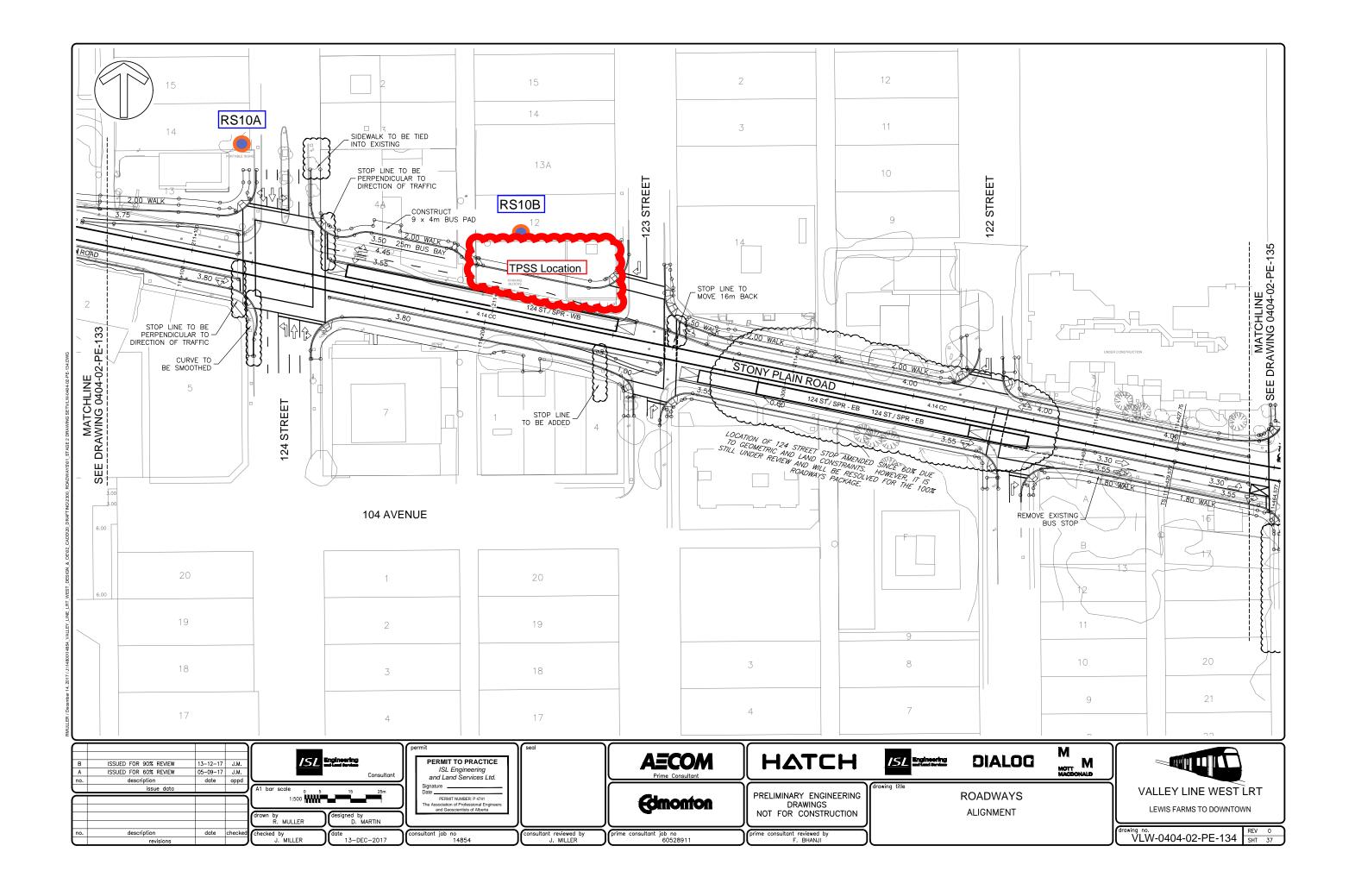


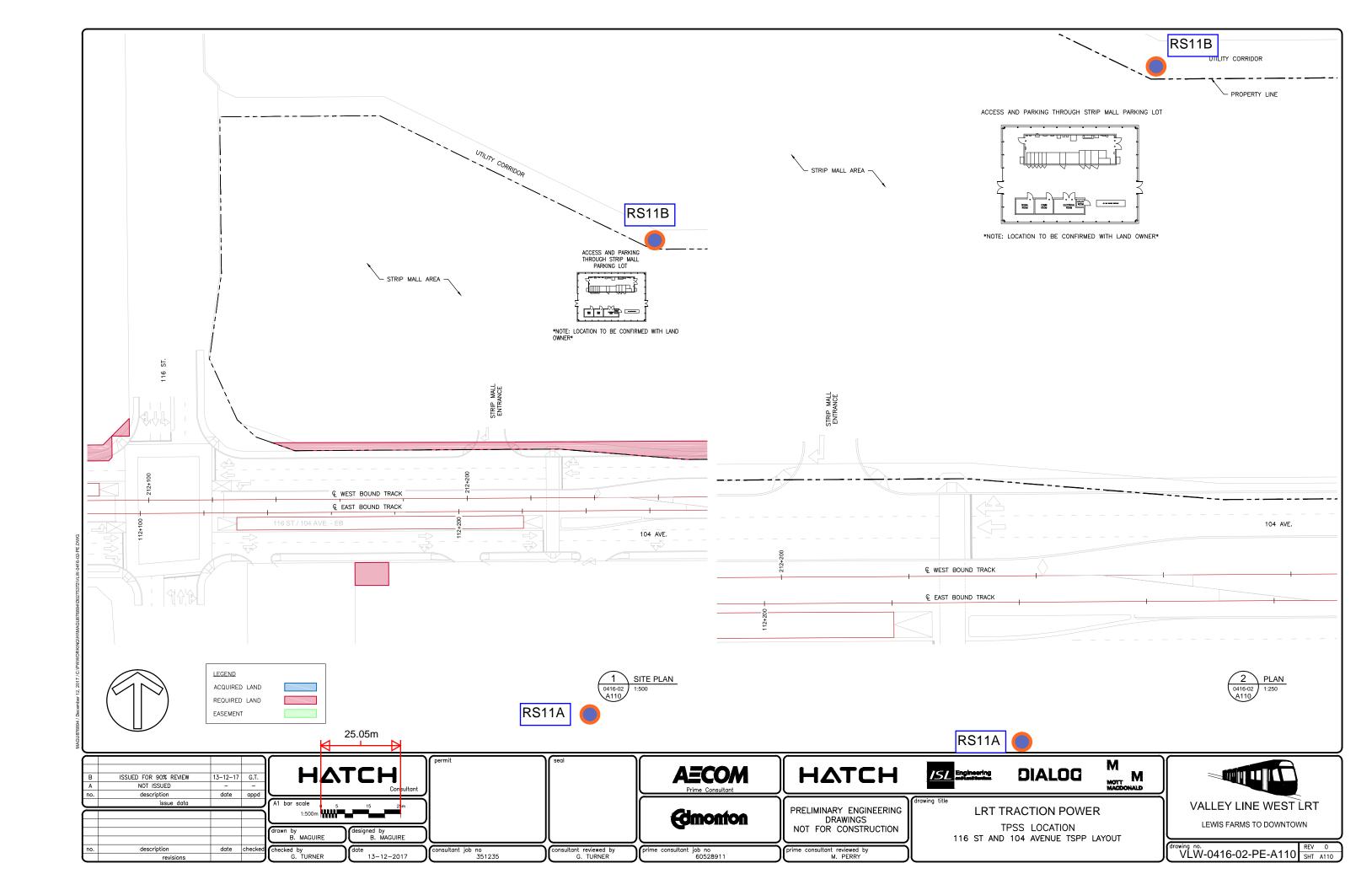


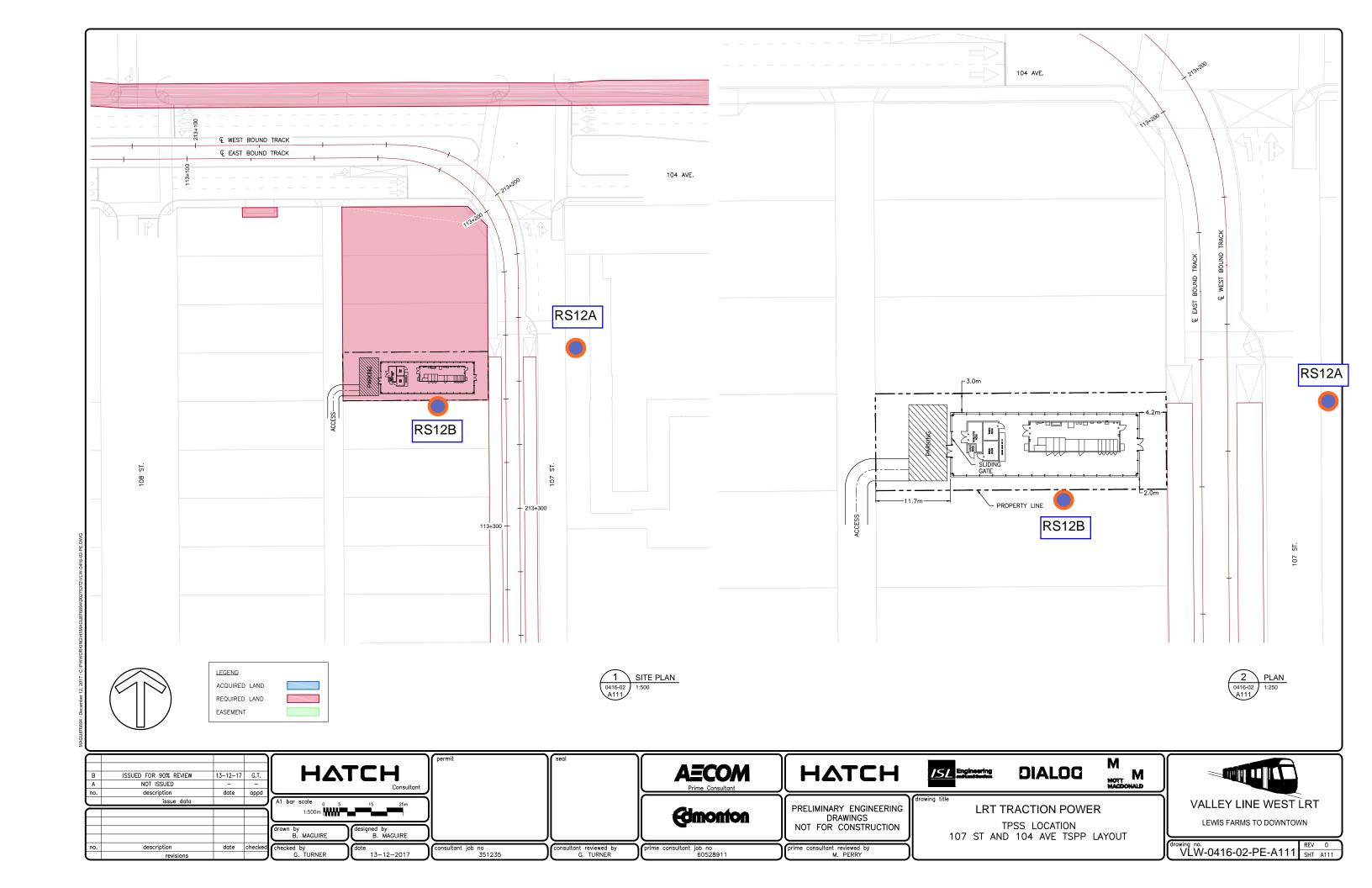






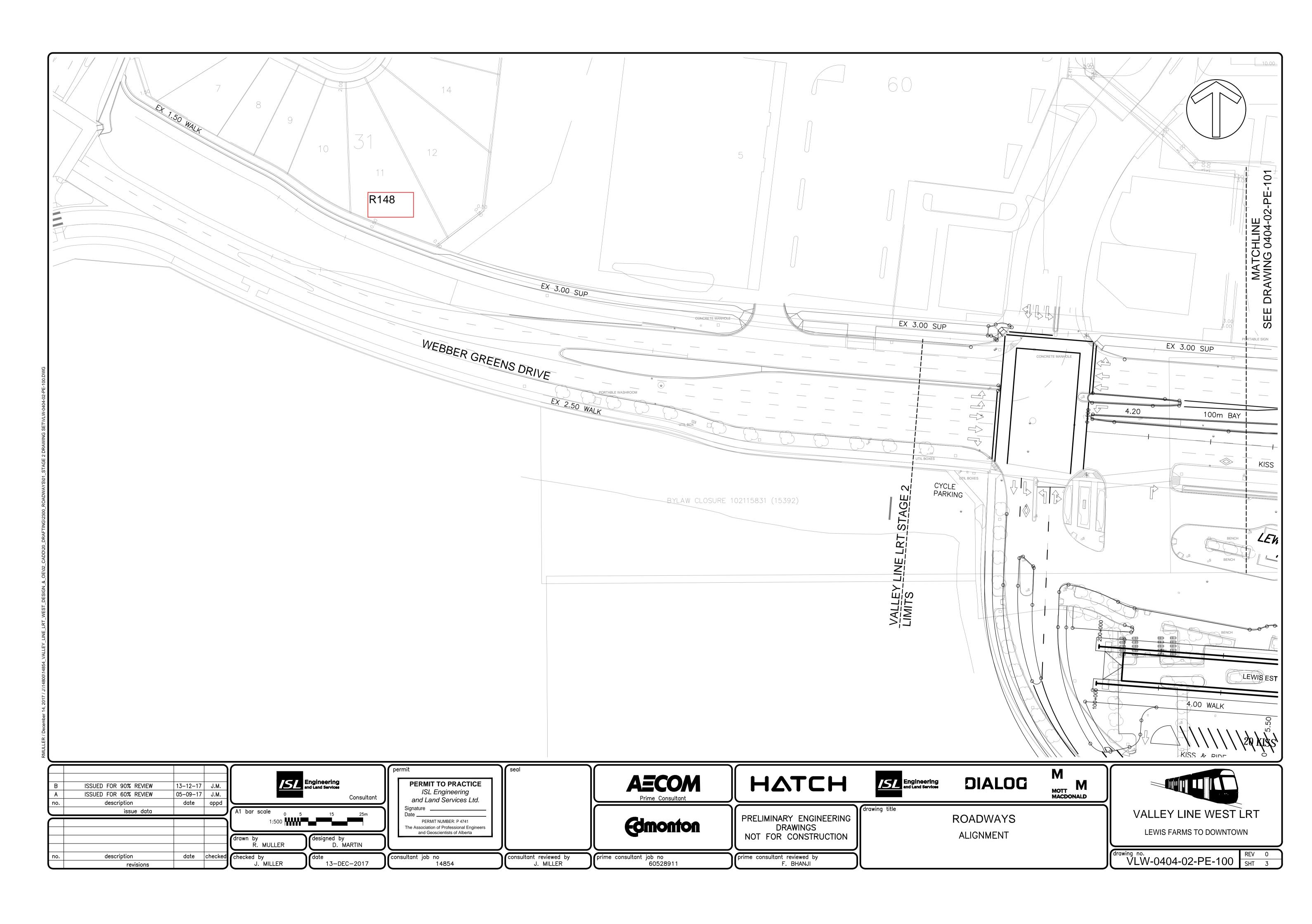


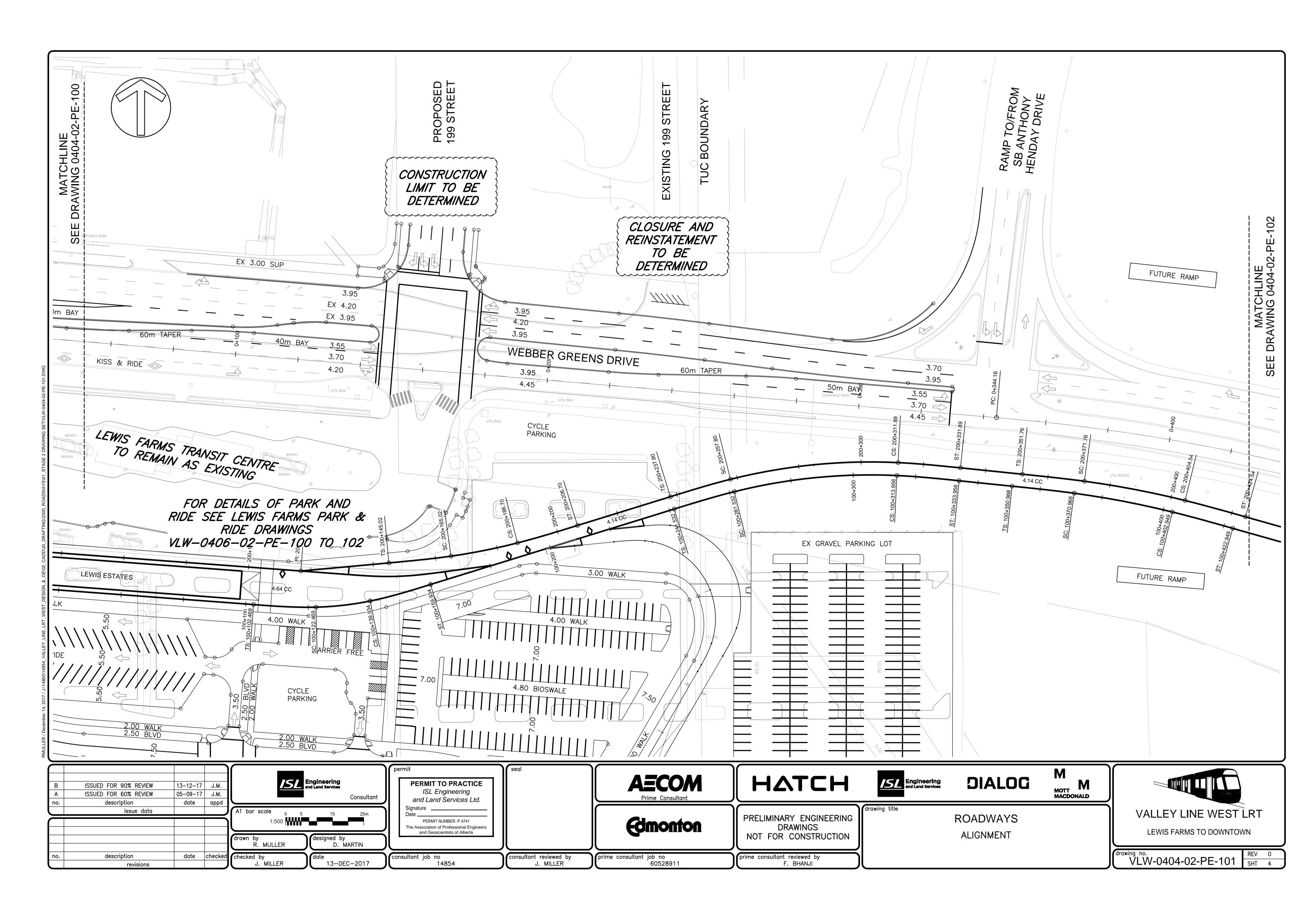


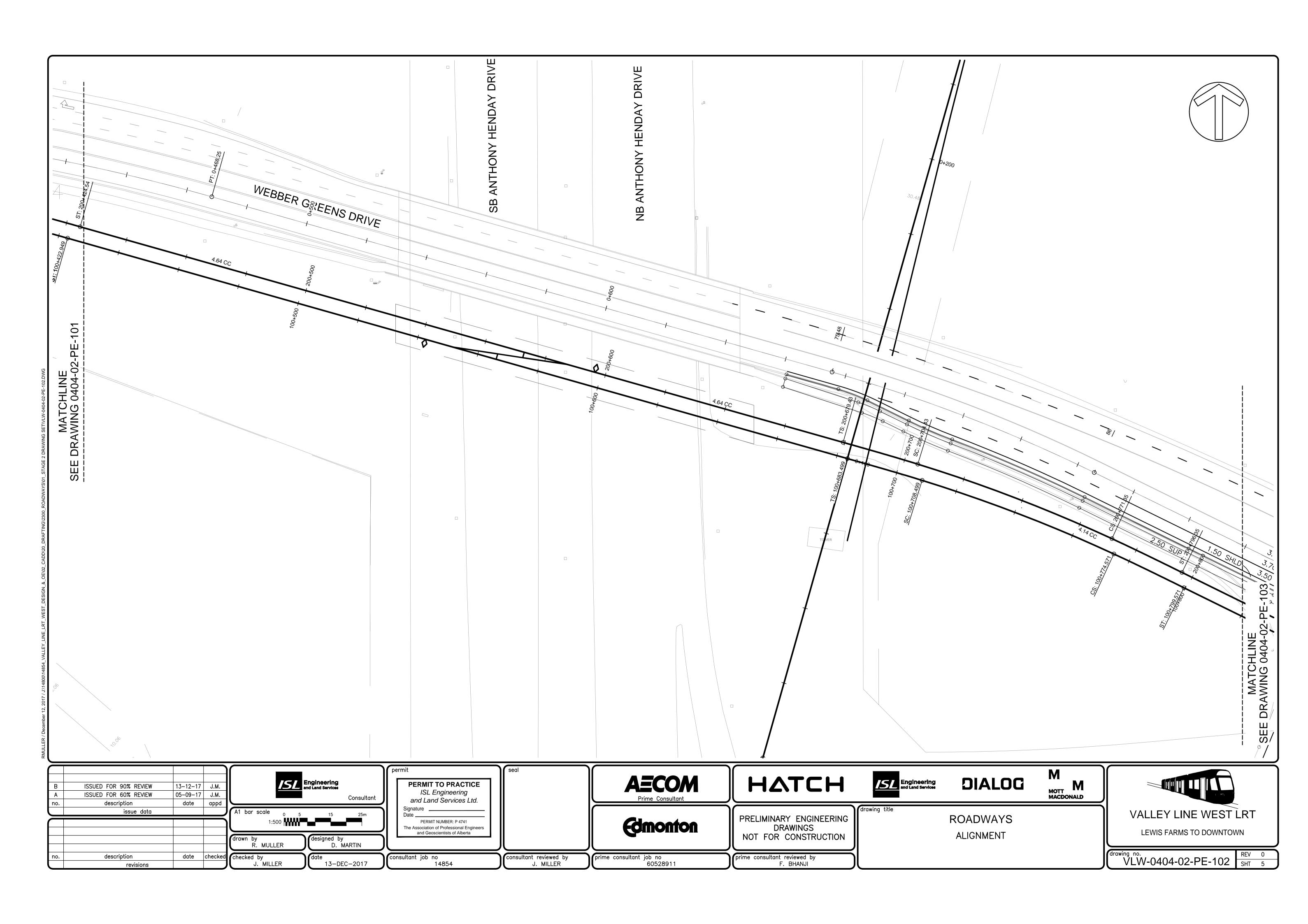


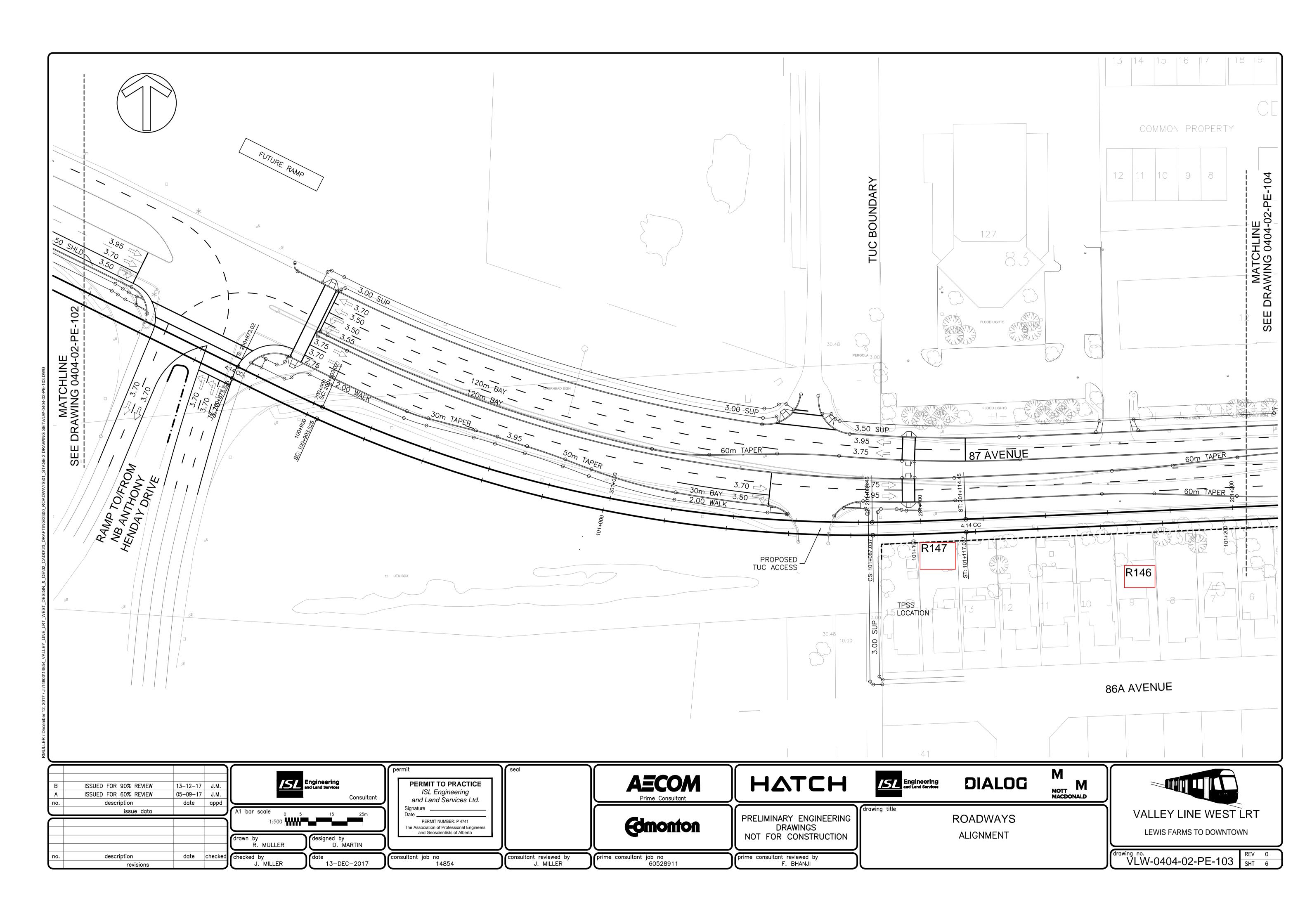


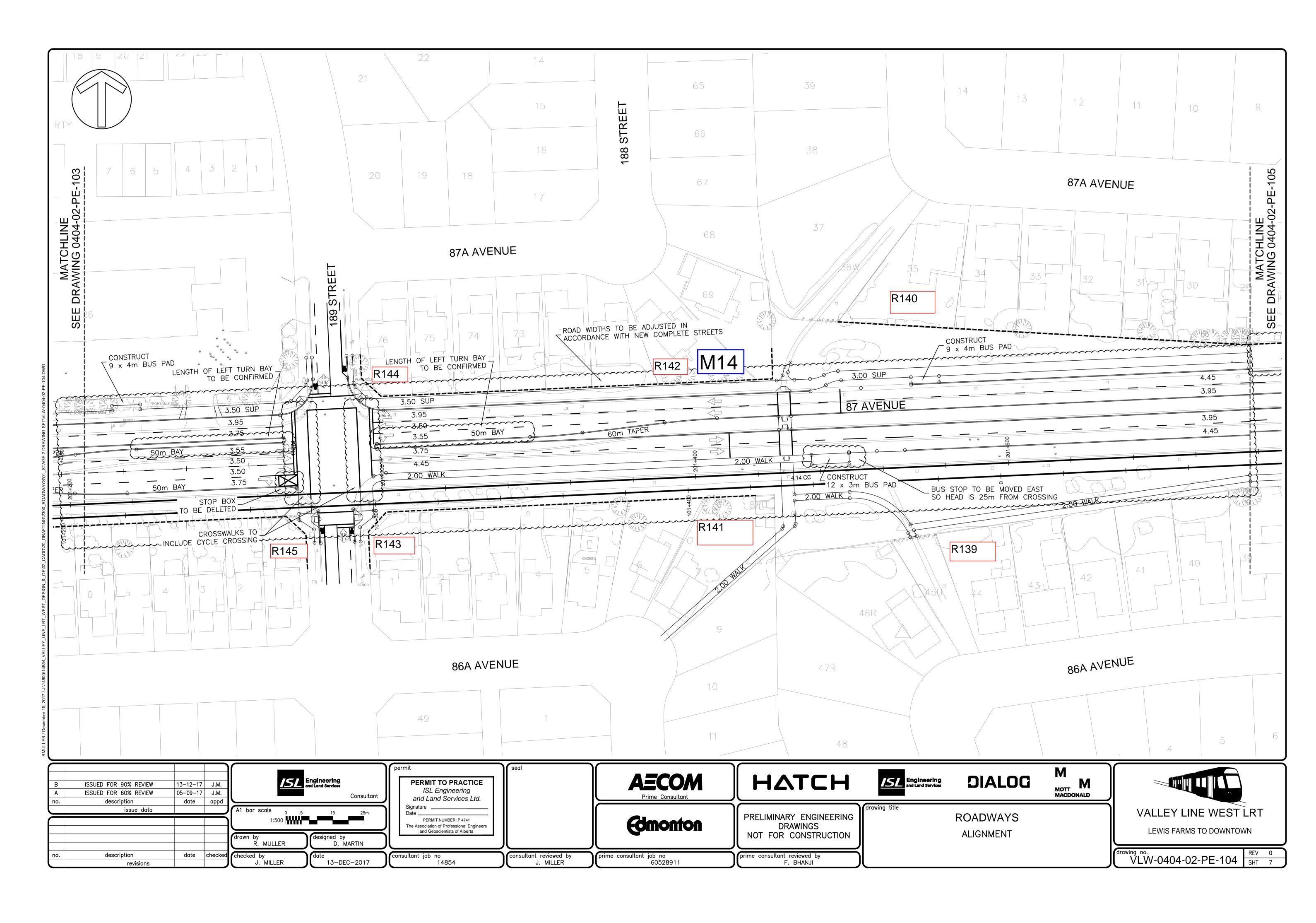
Appendix B1 Transportation Noise Receptor Map aecom.com

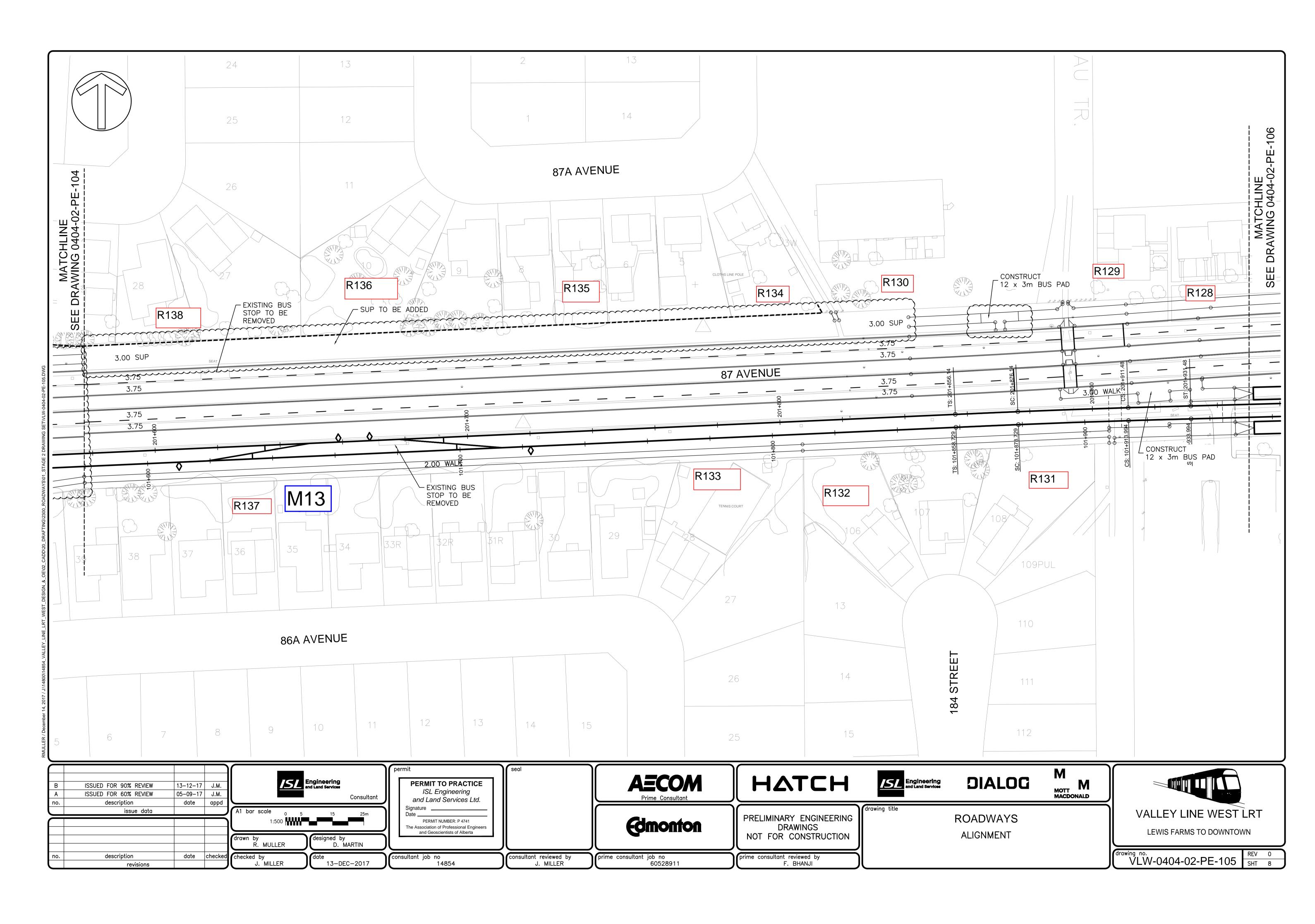


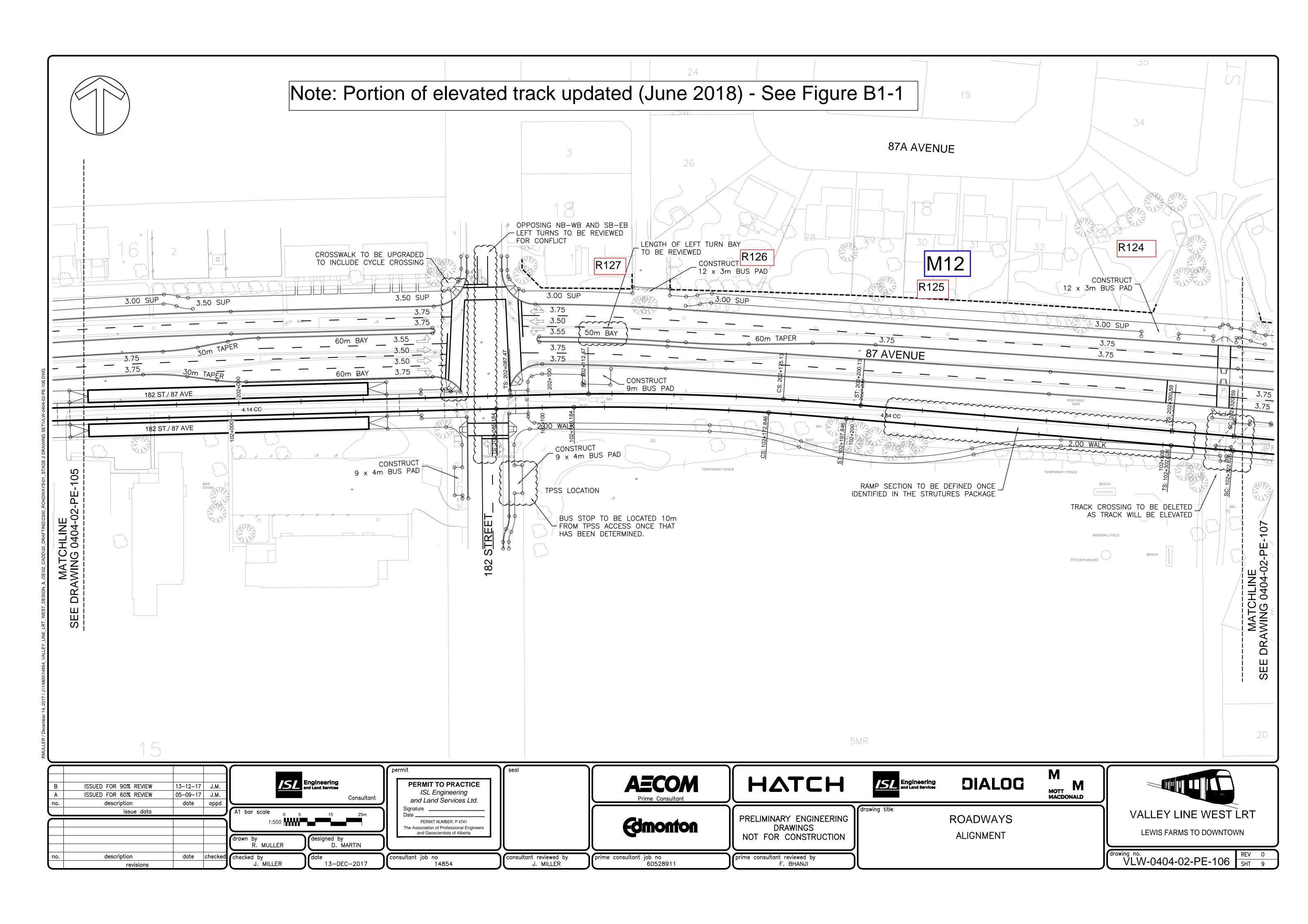


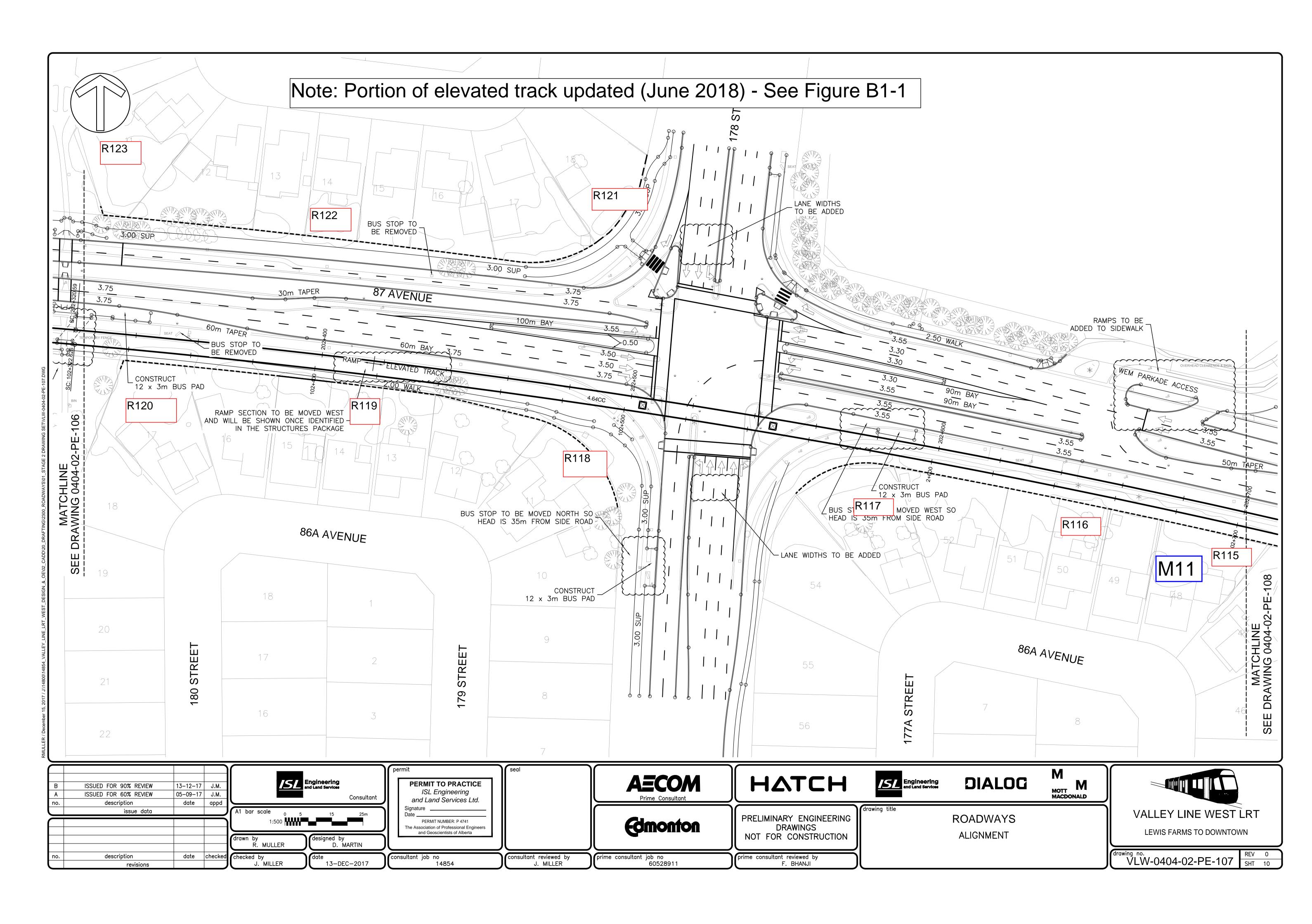


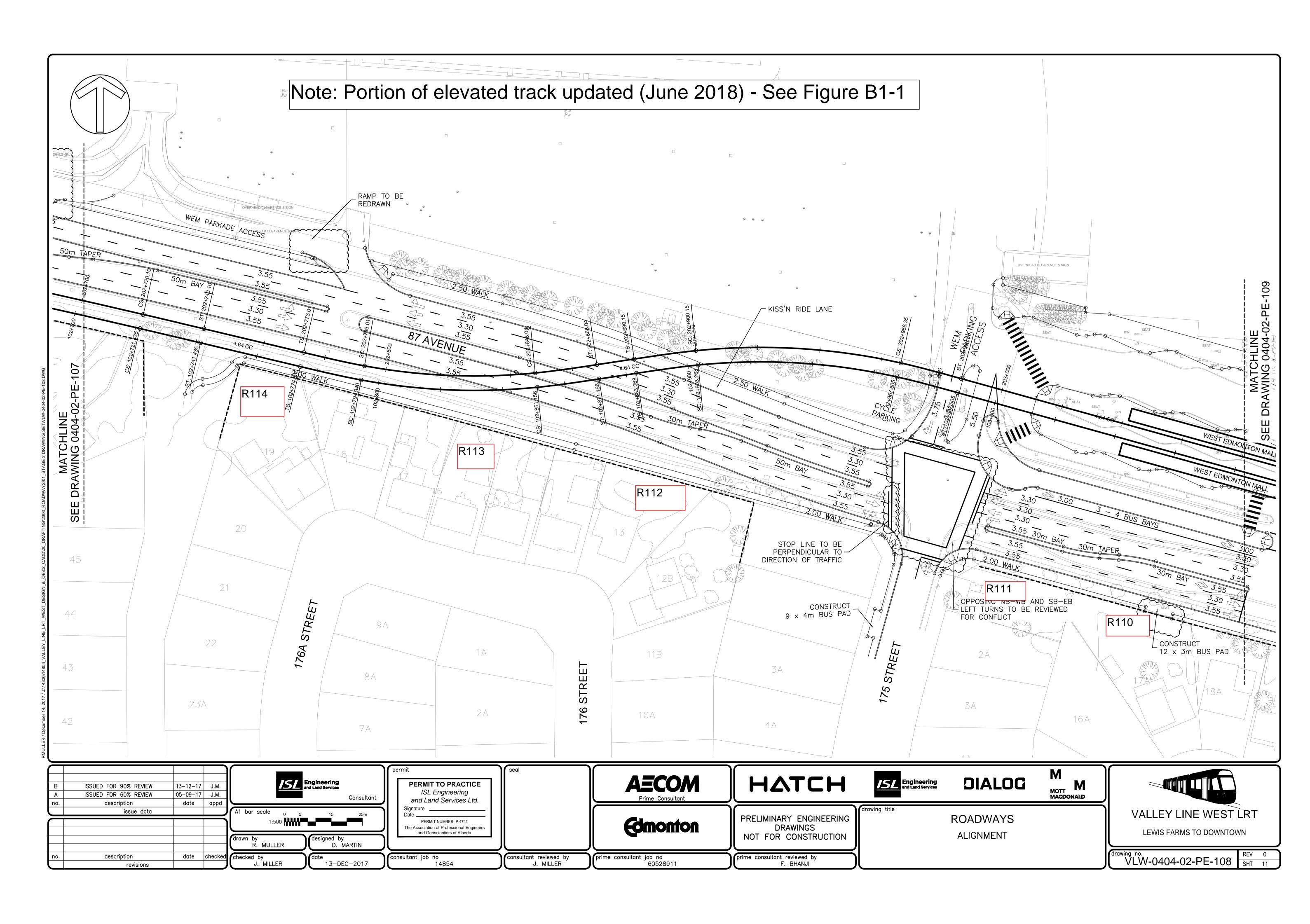


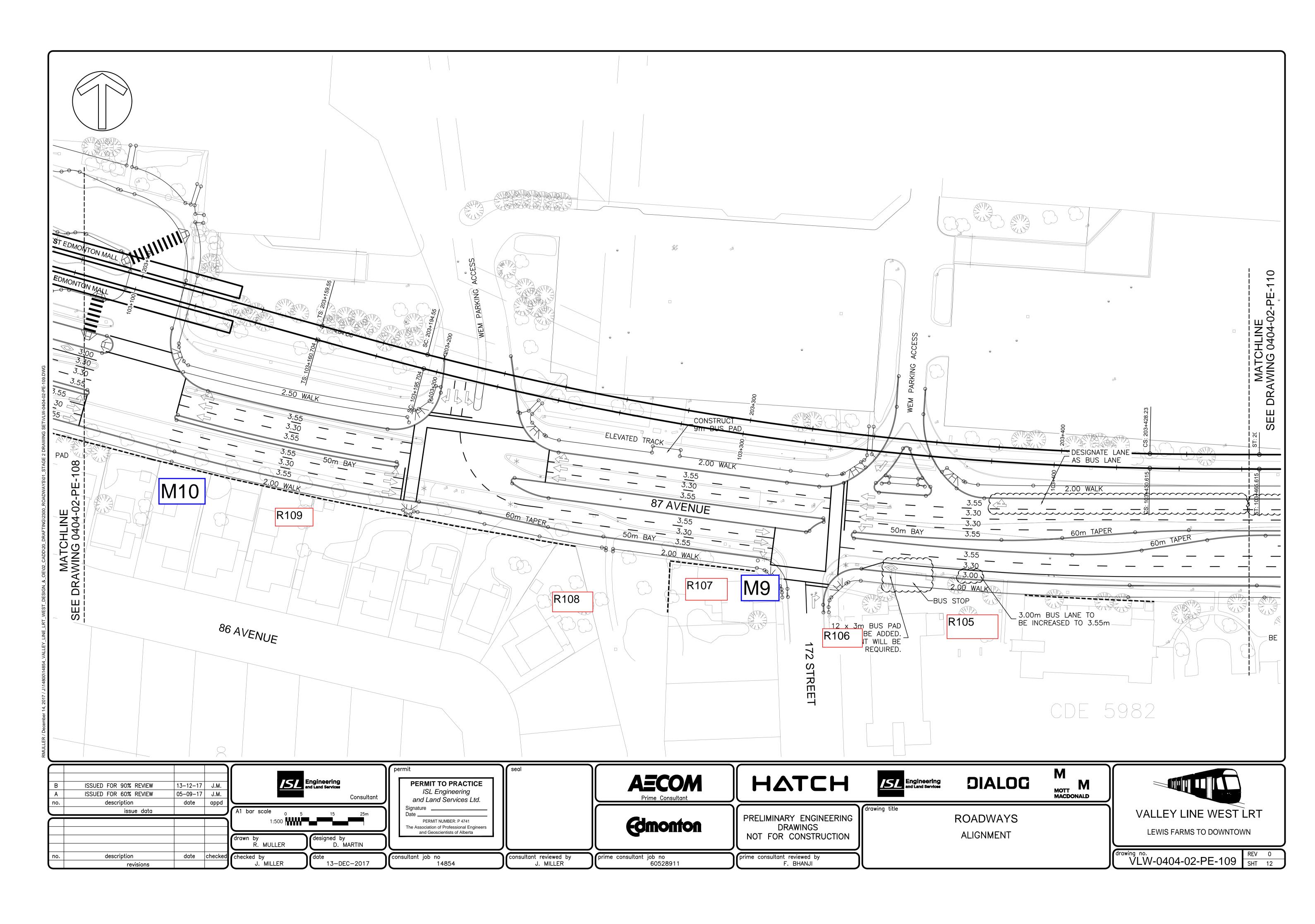


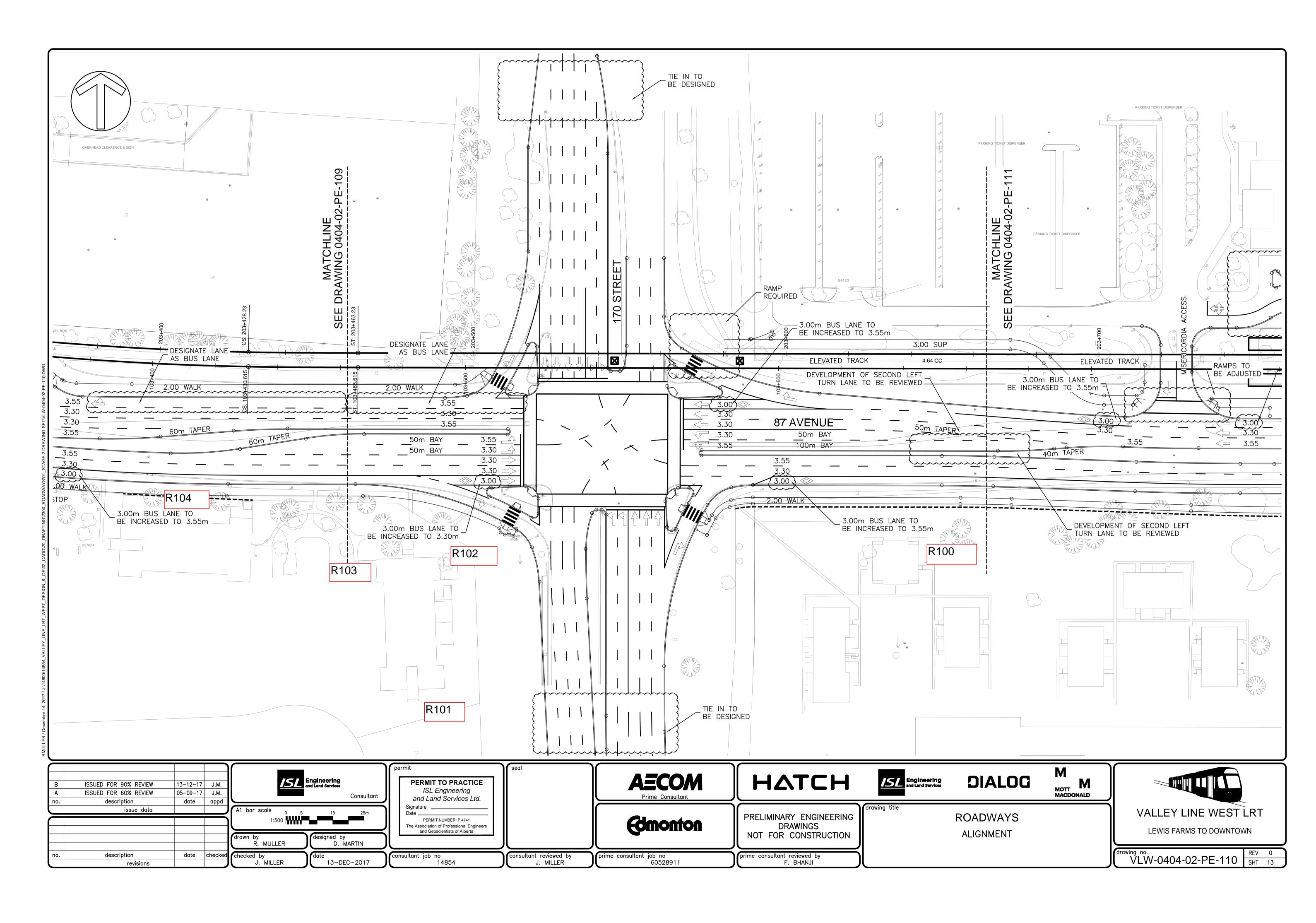


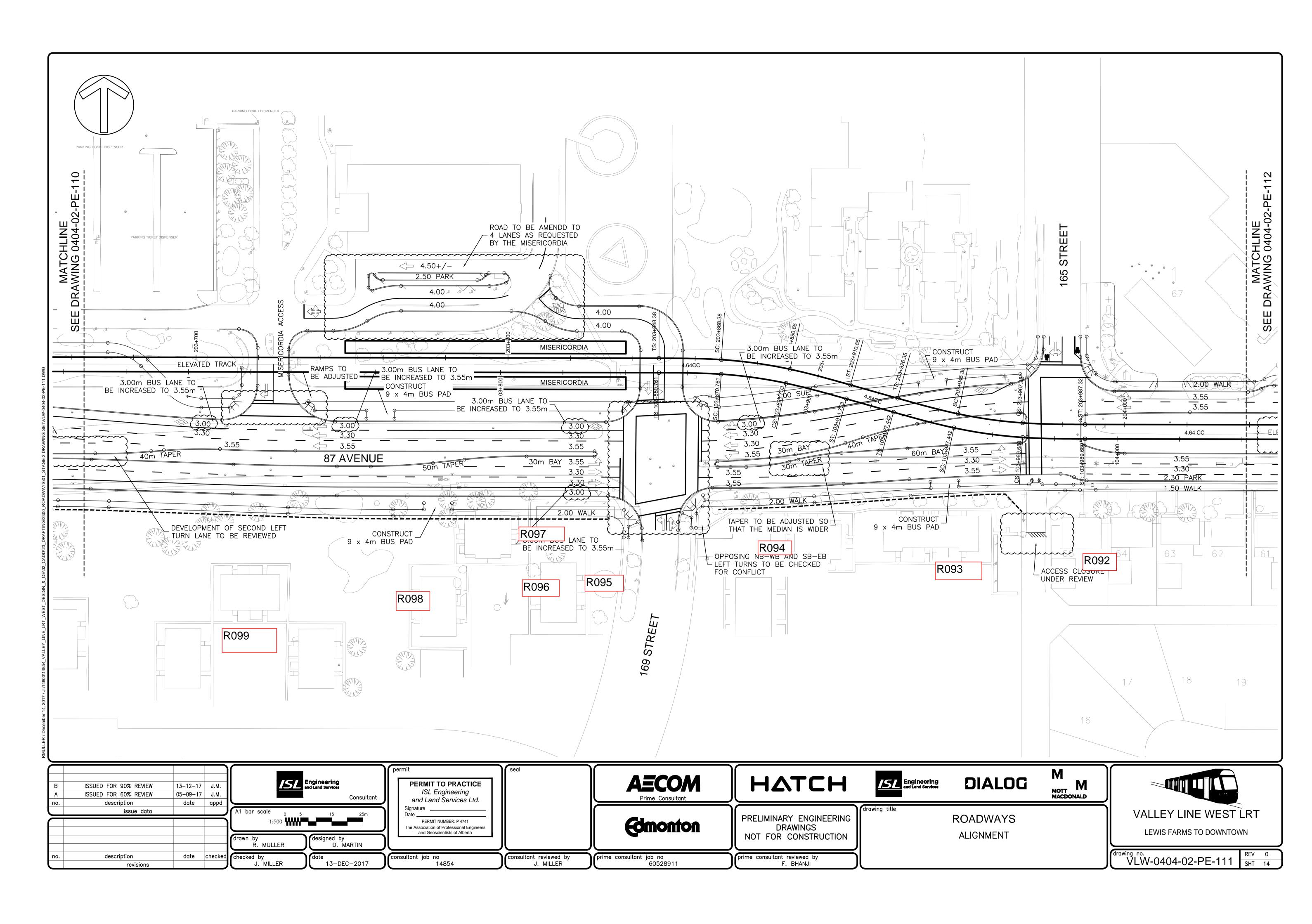


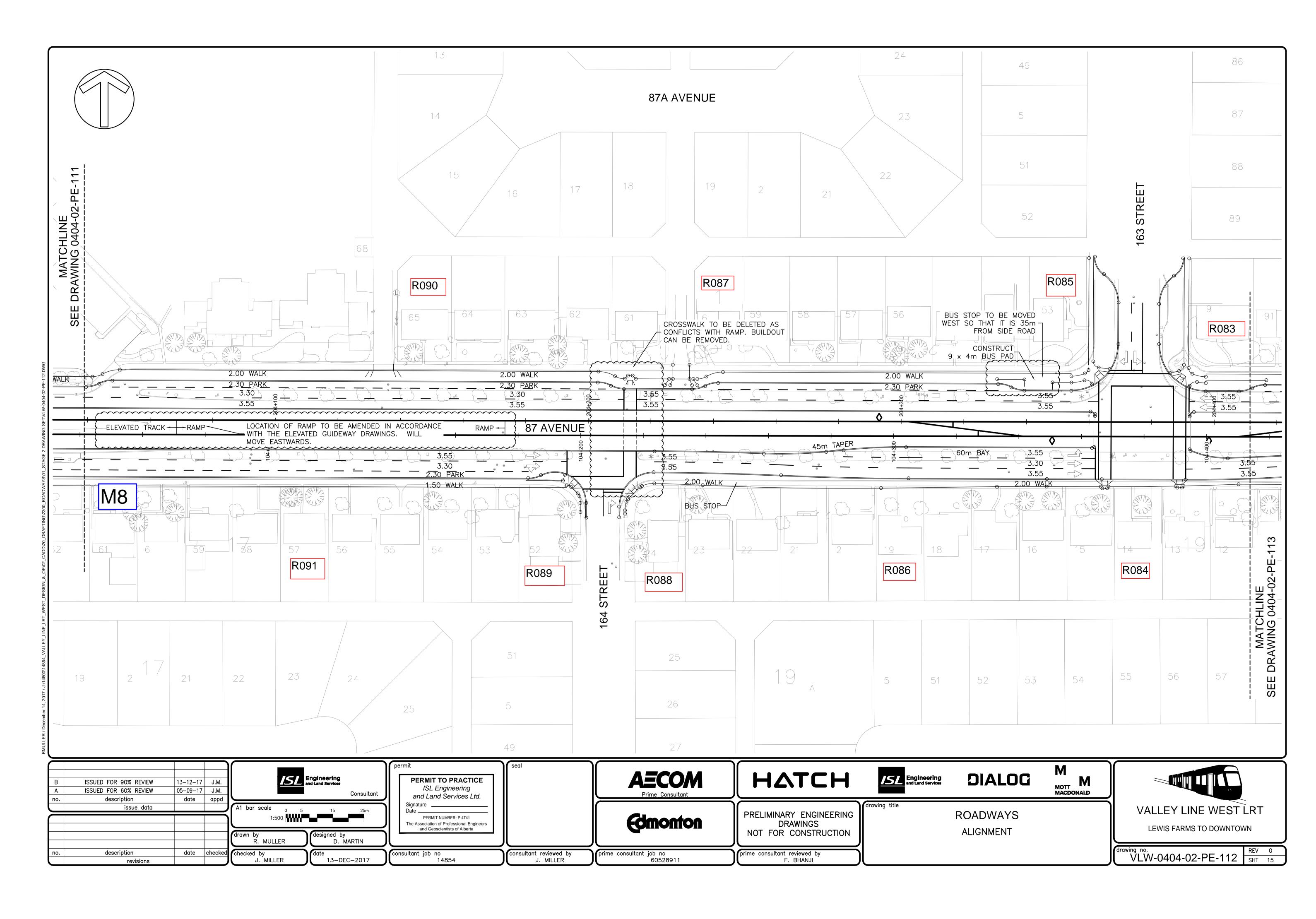


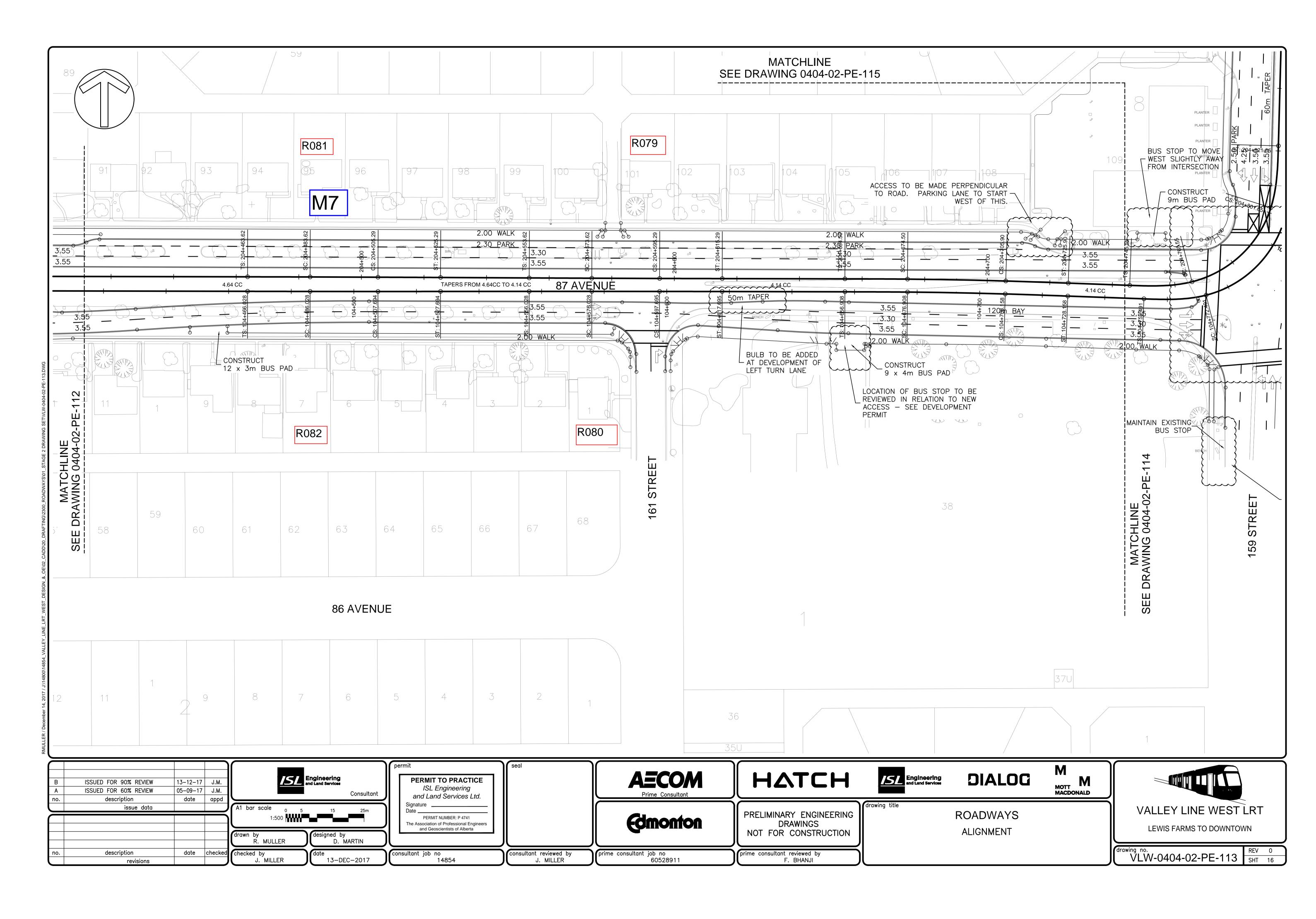


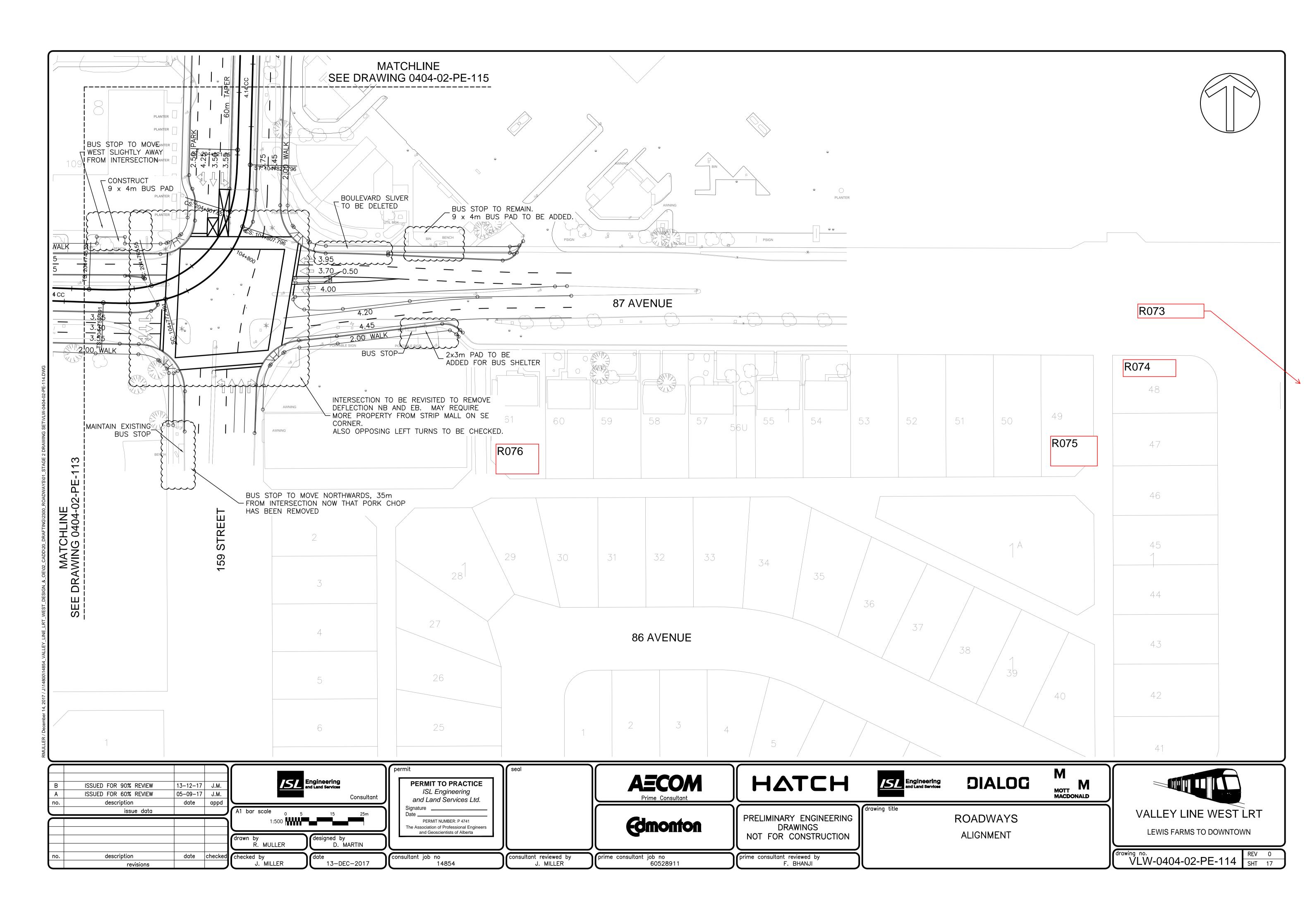


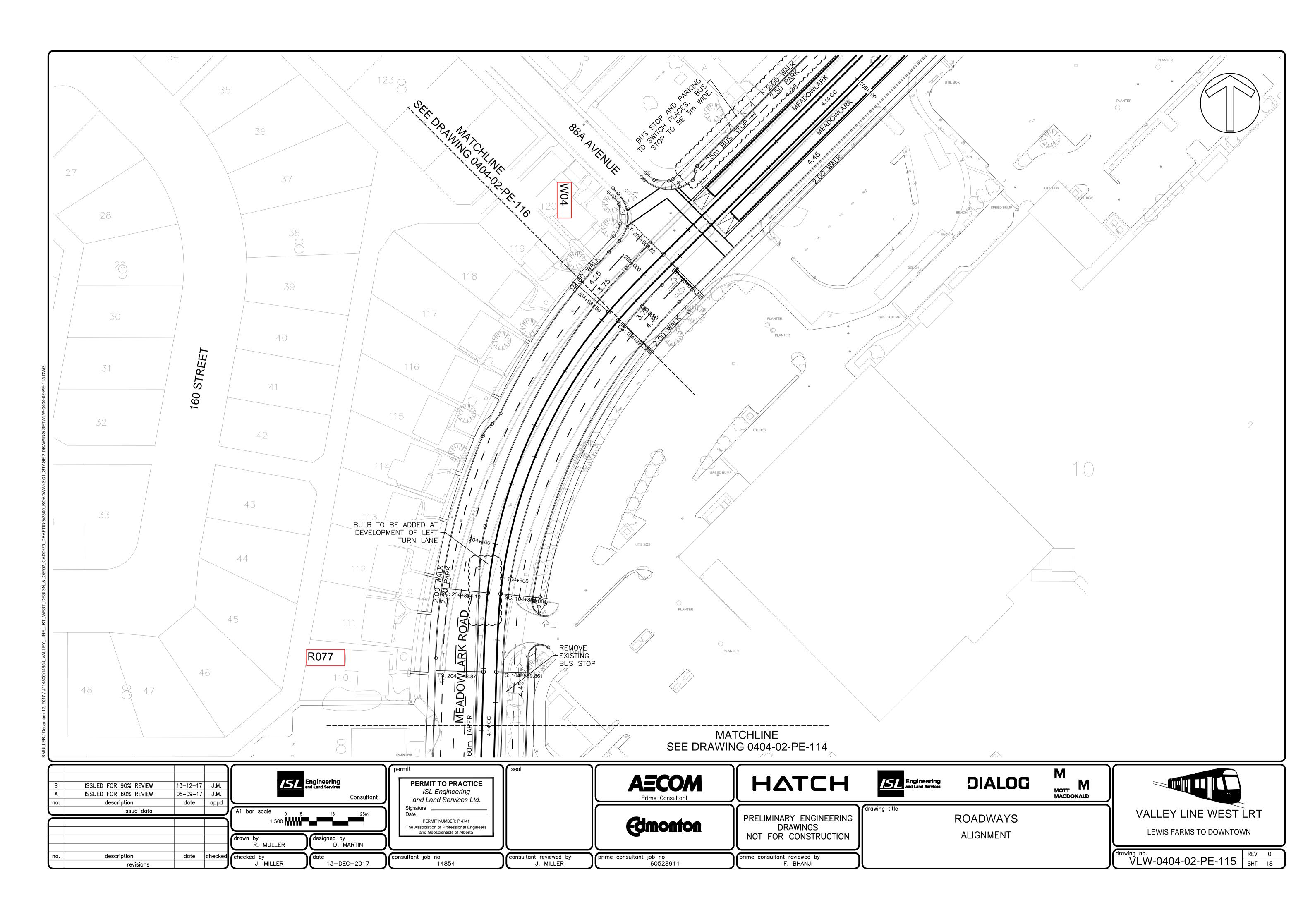


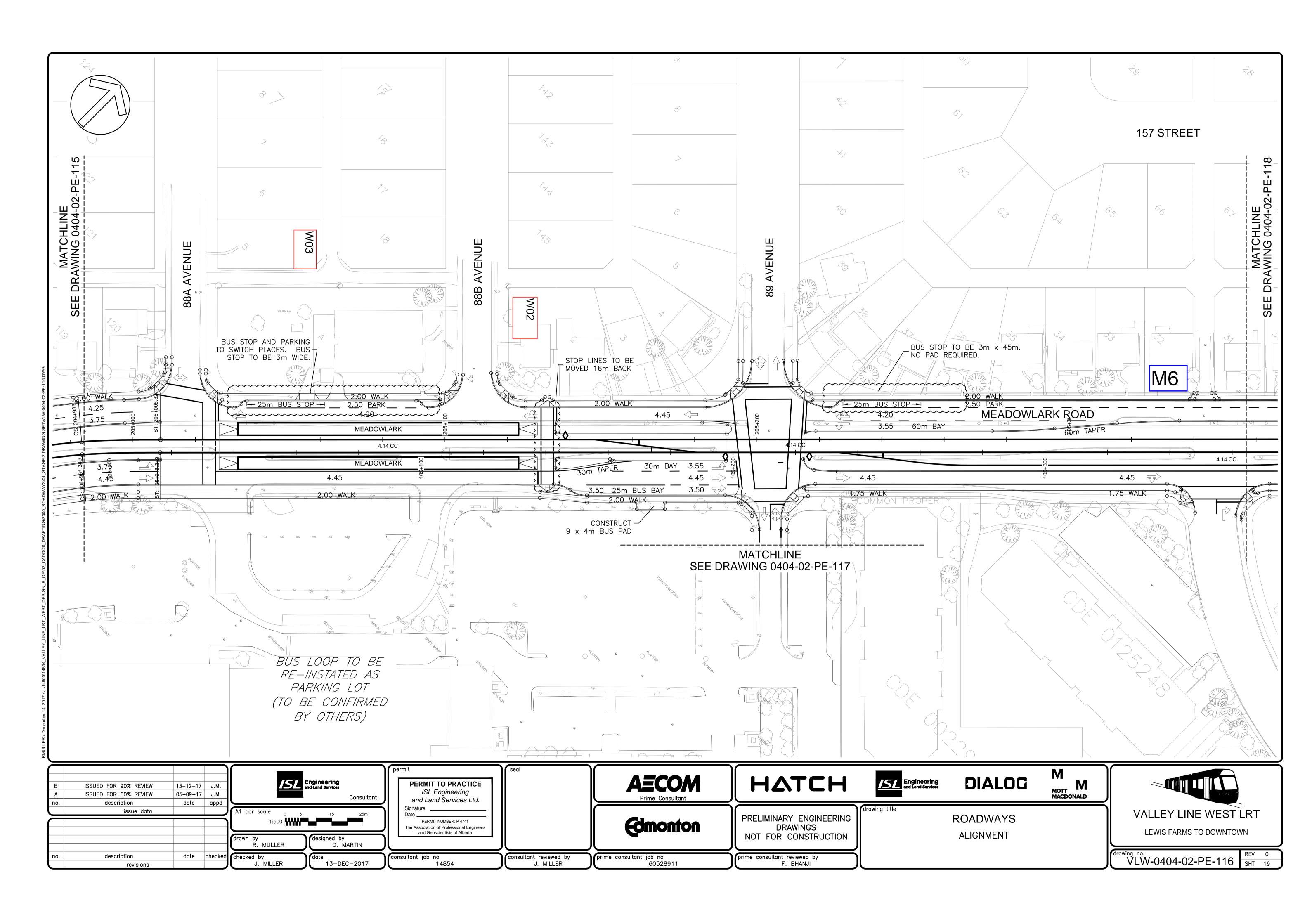


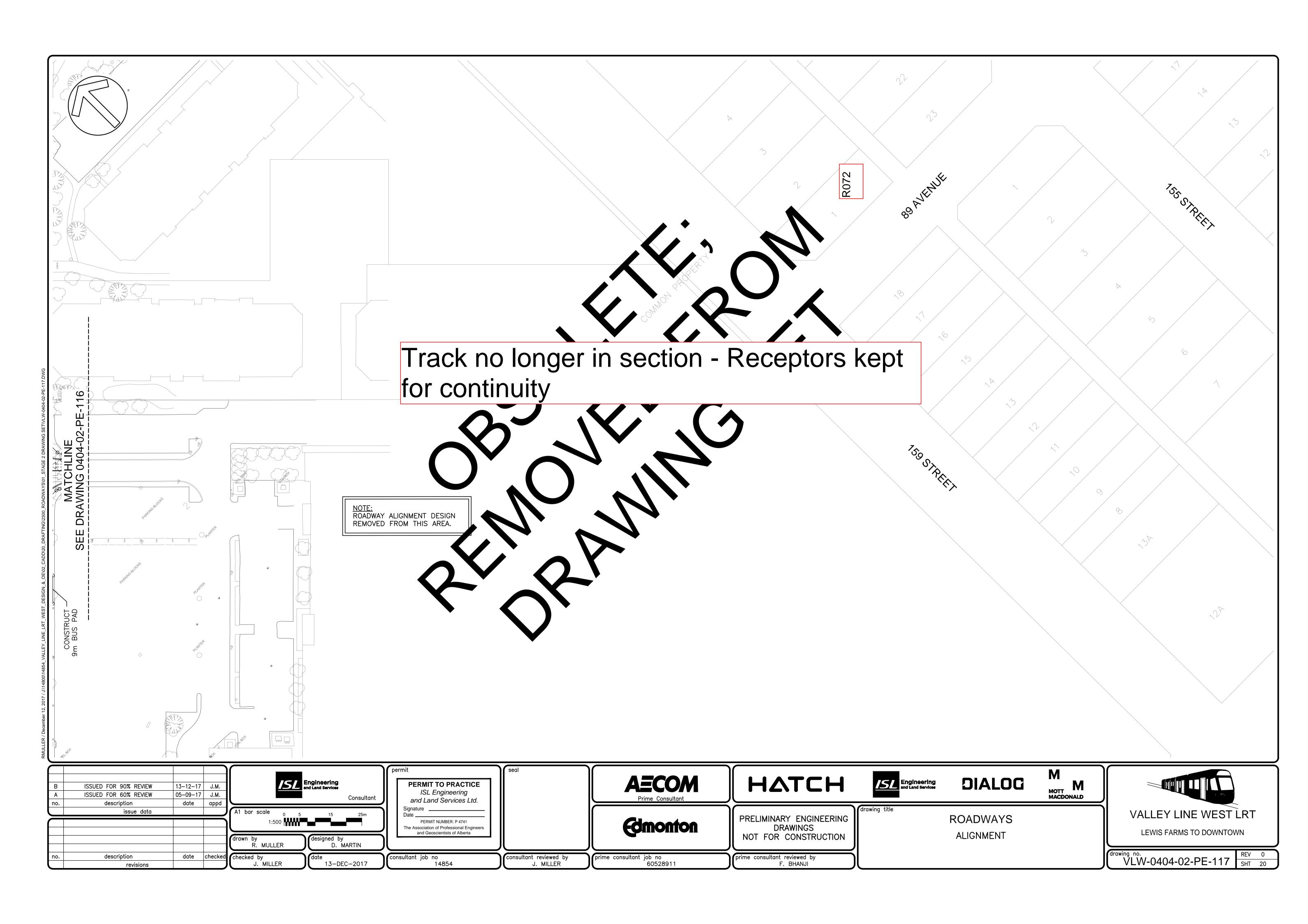


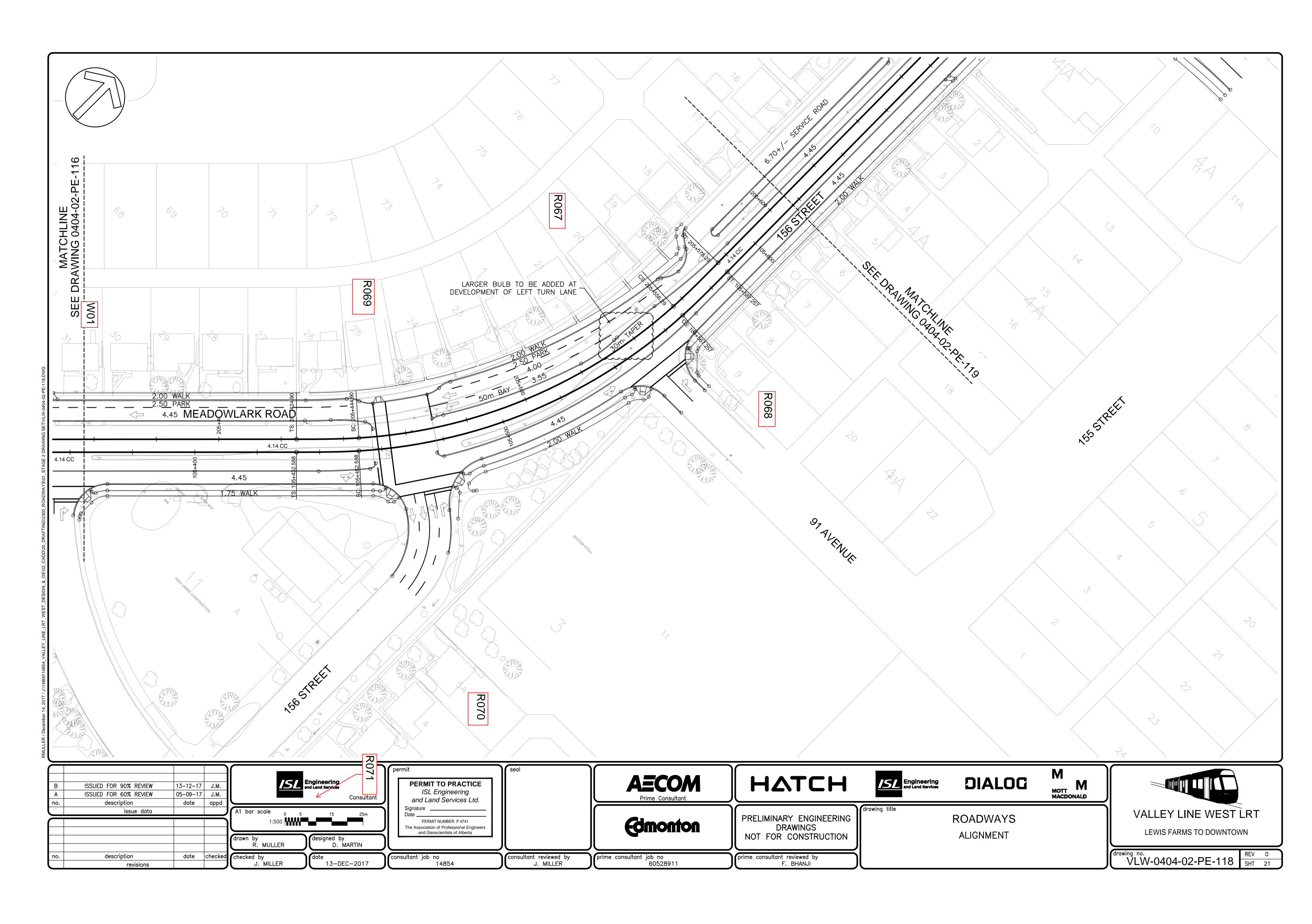


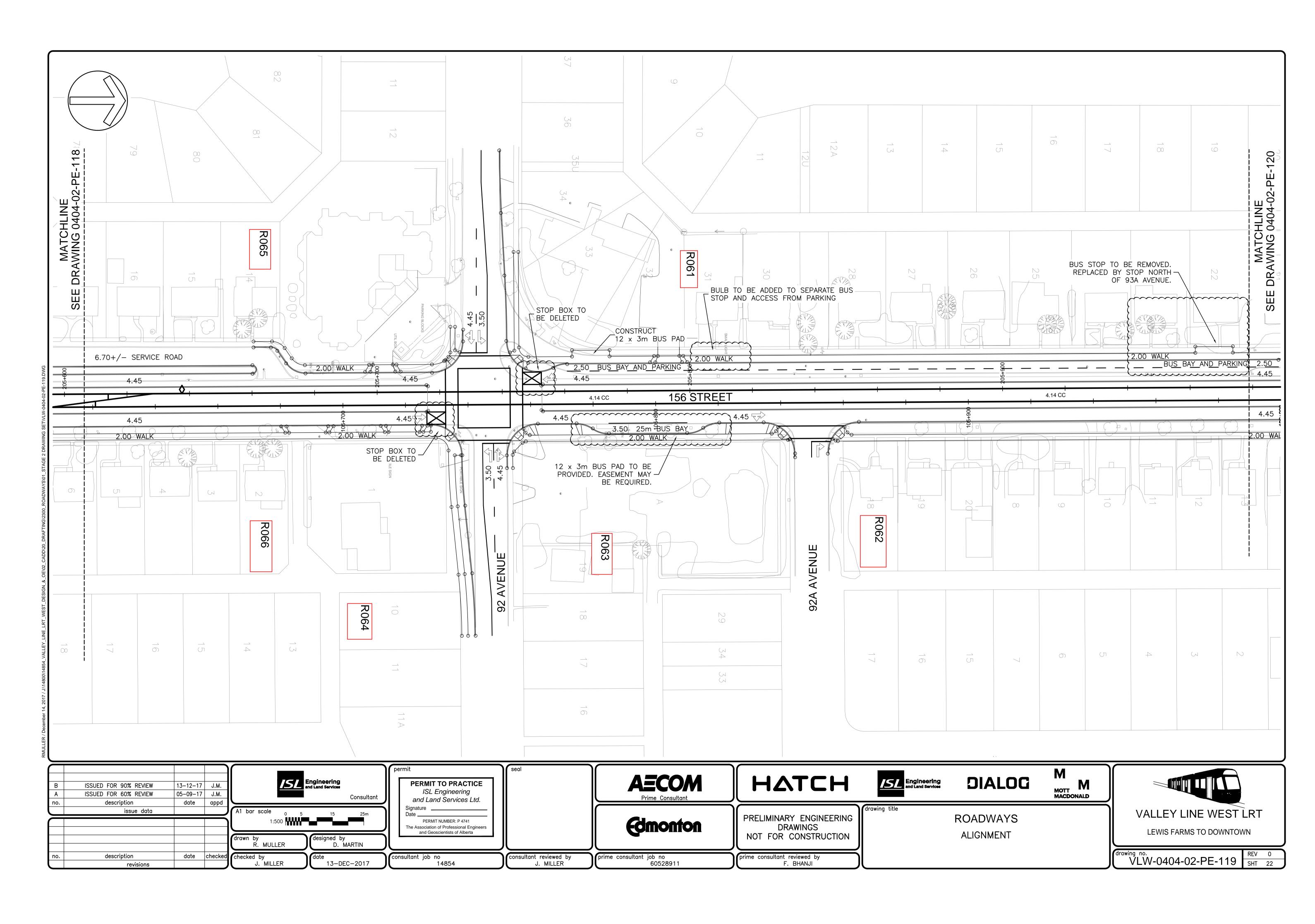


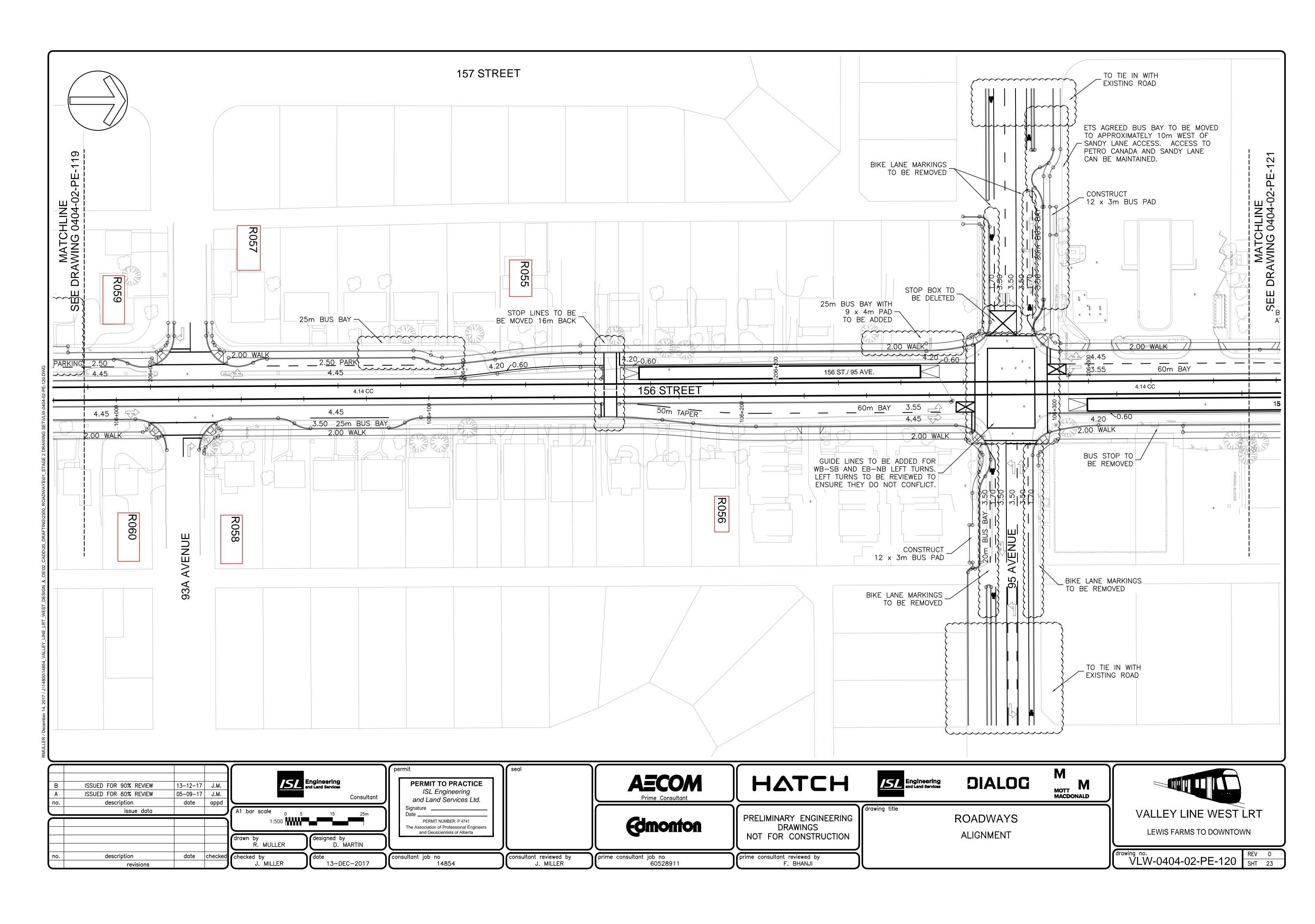


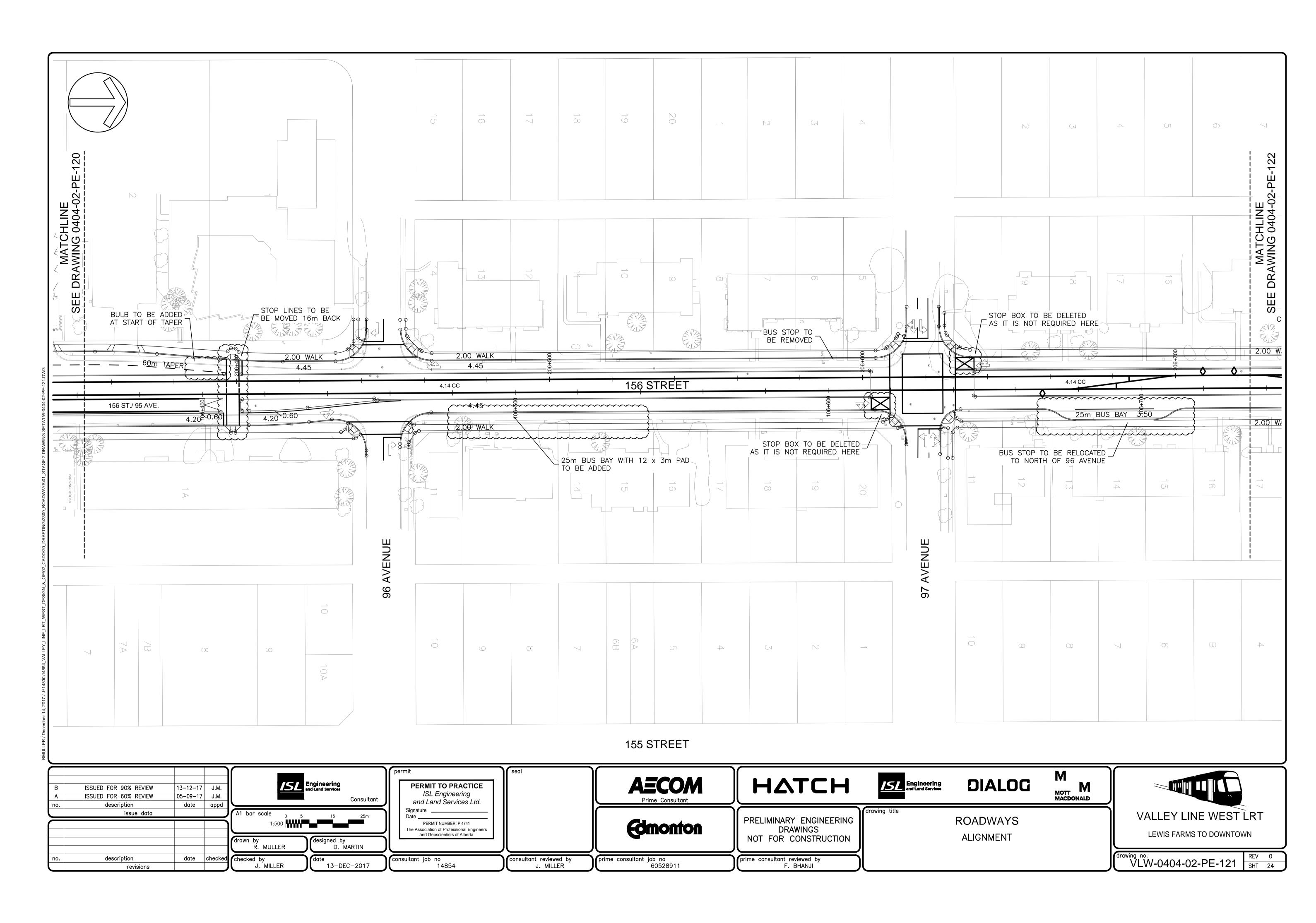


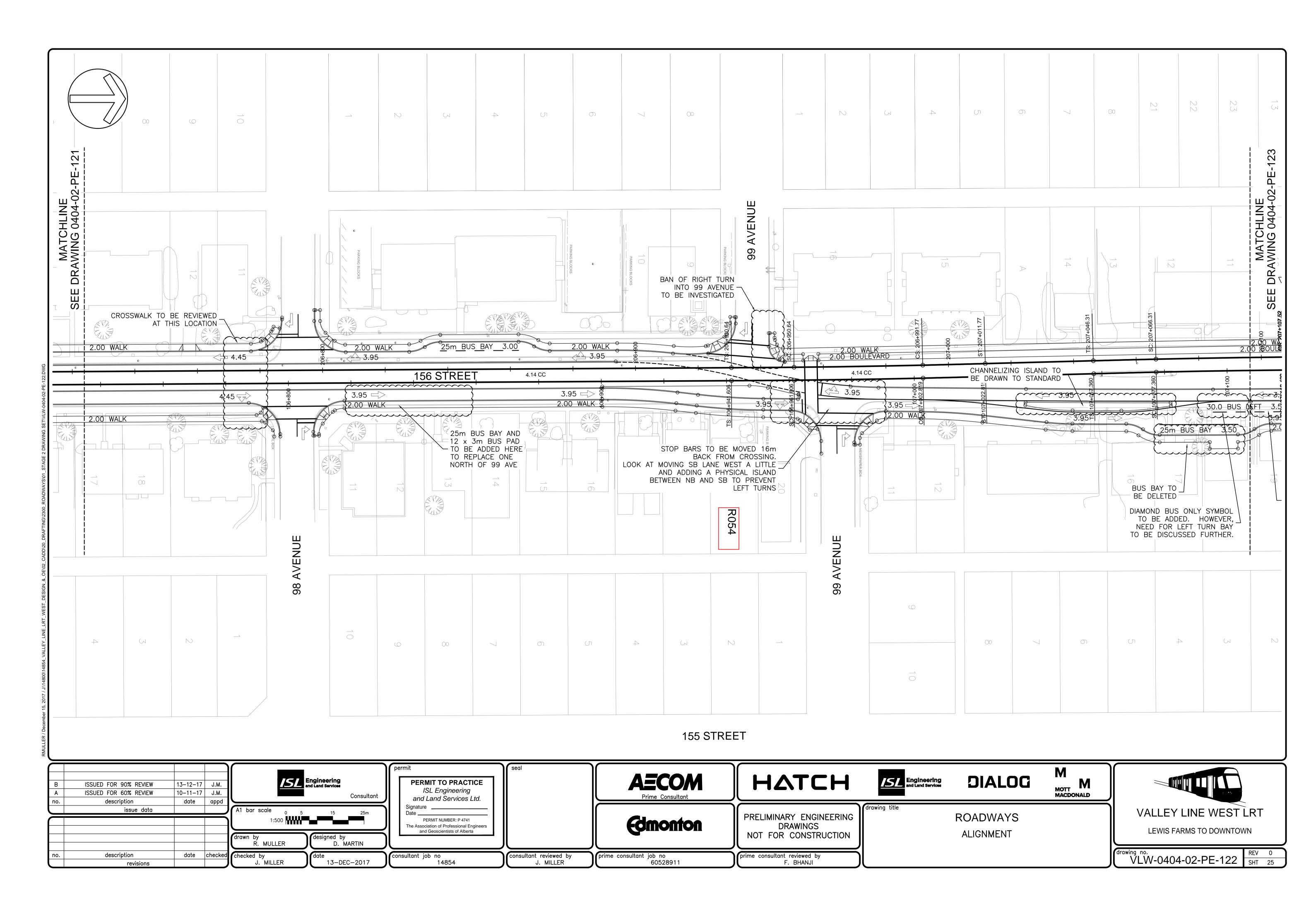


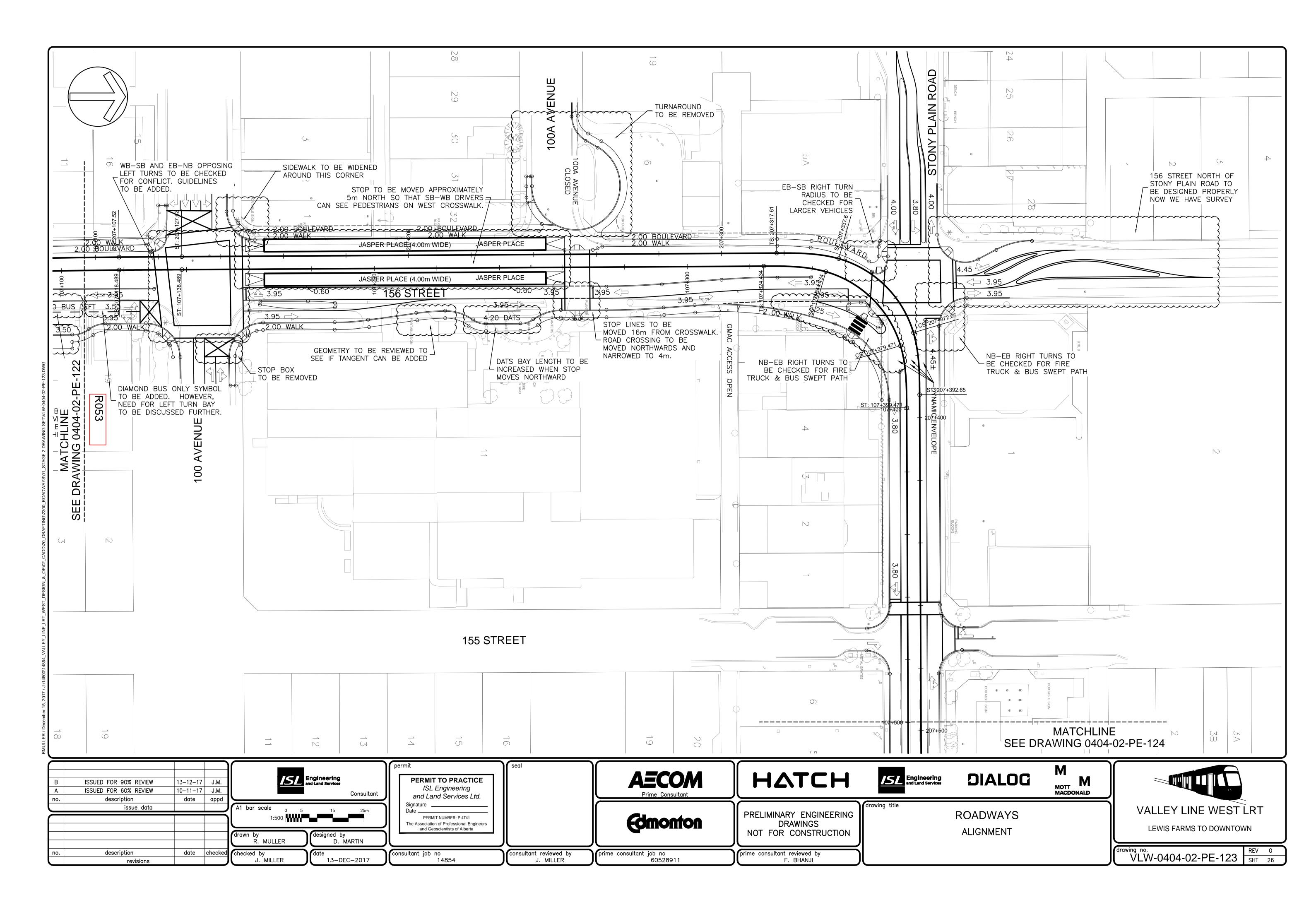


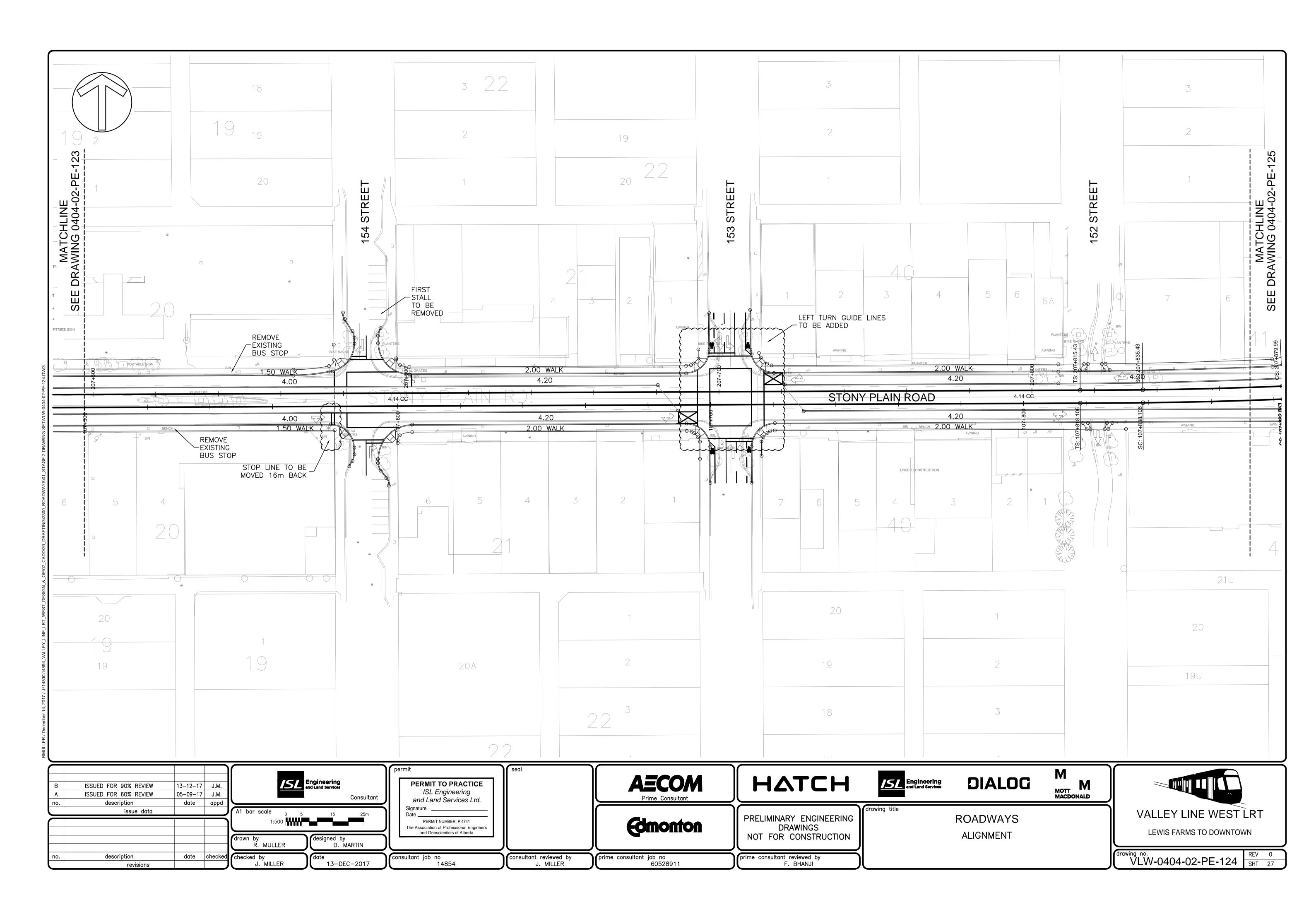


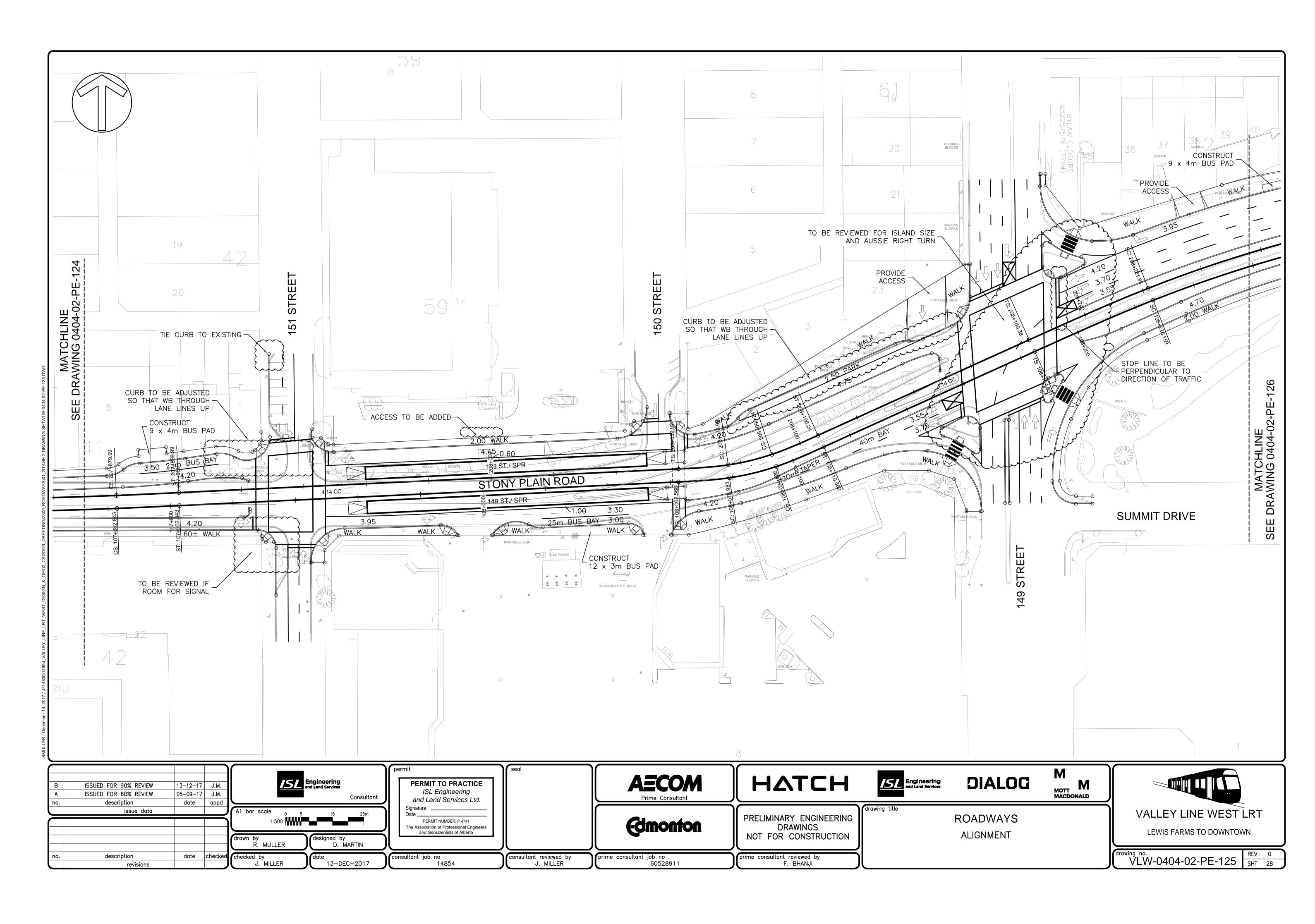


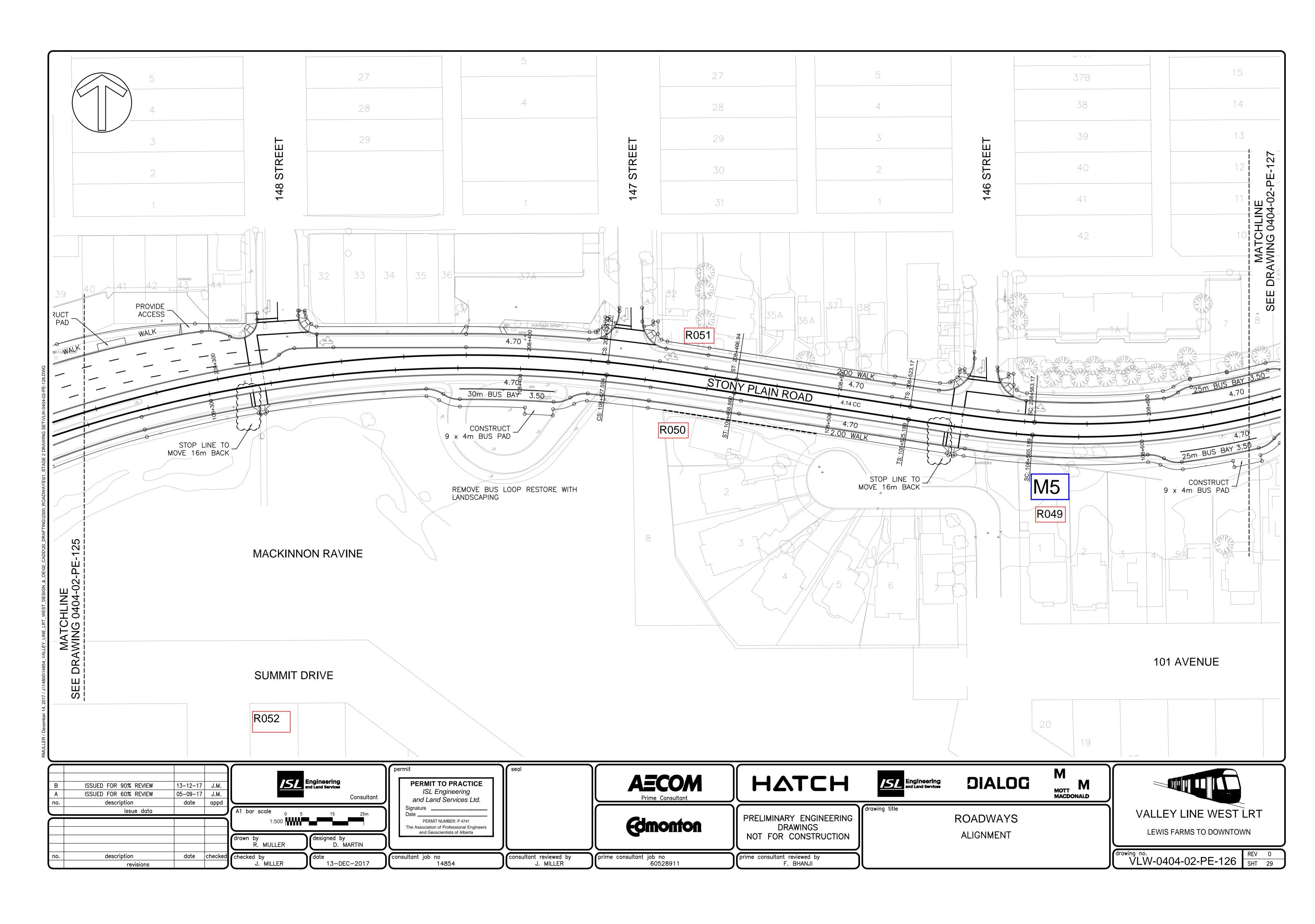


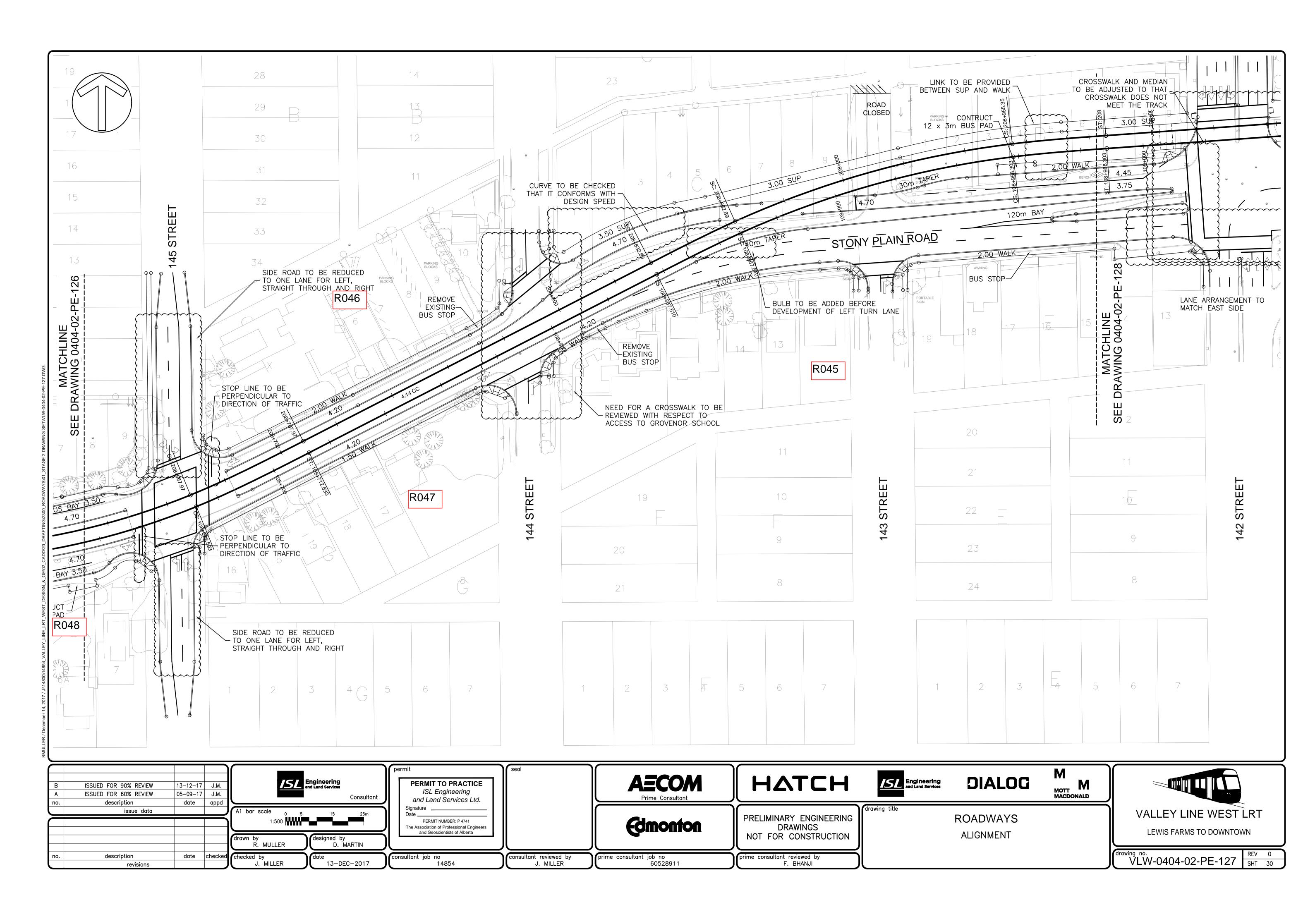


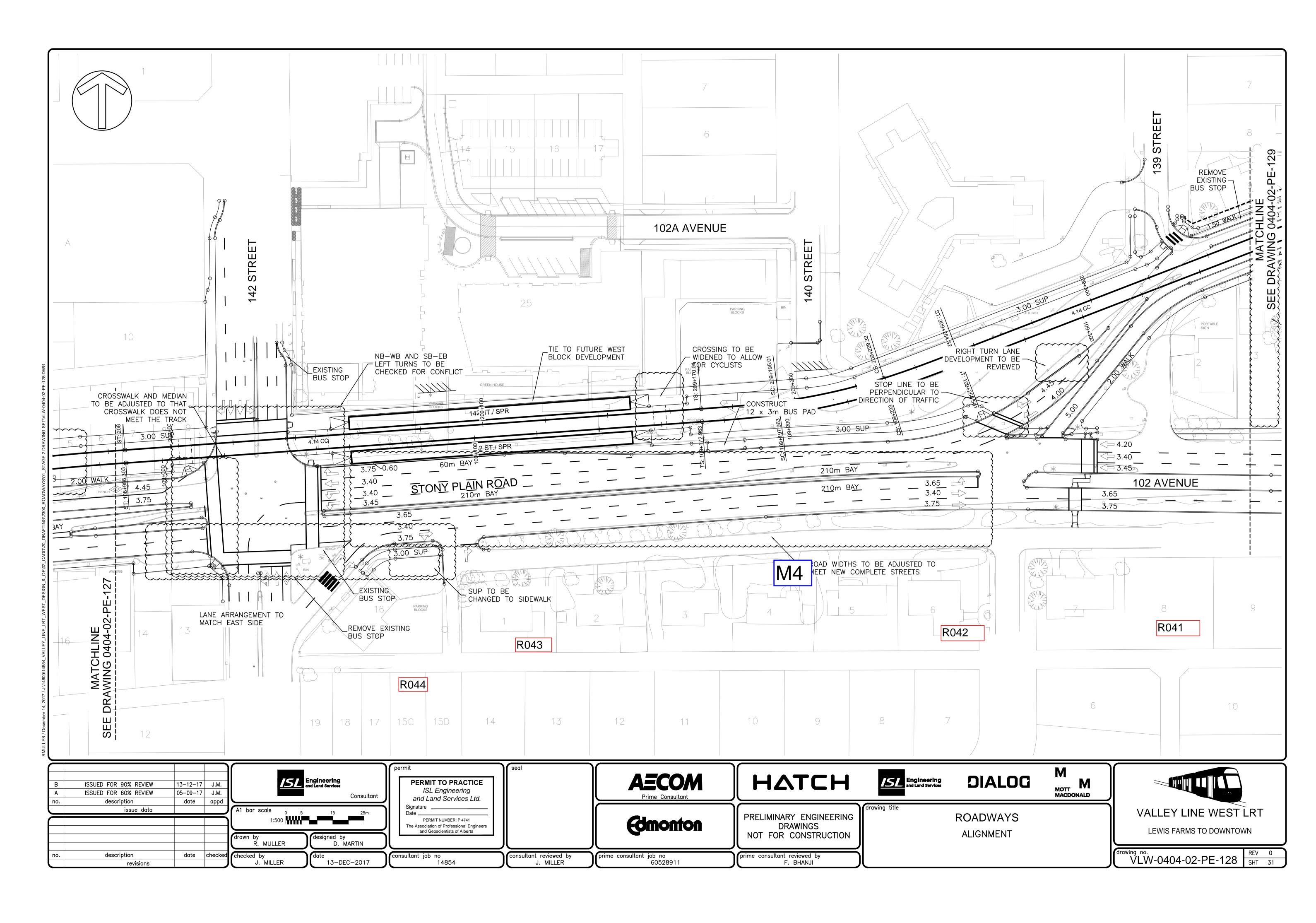


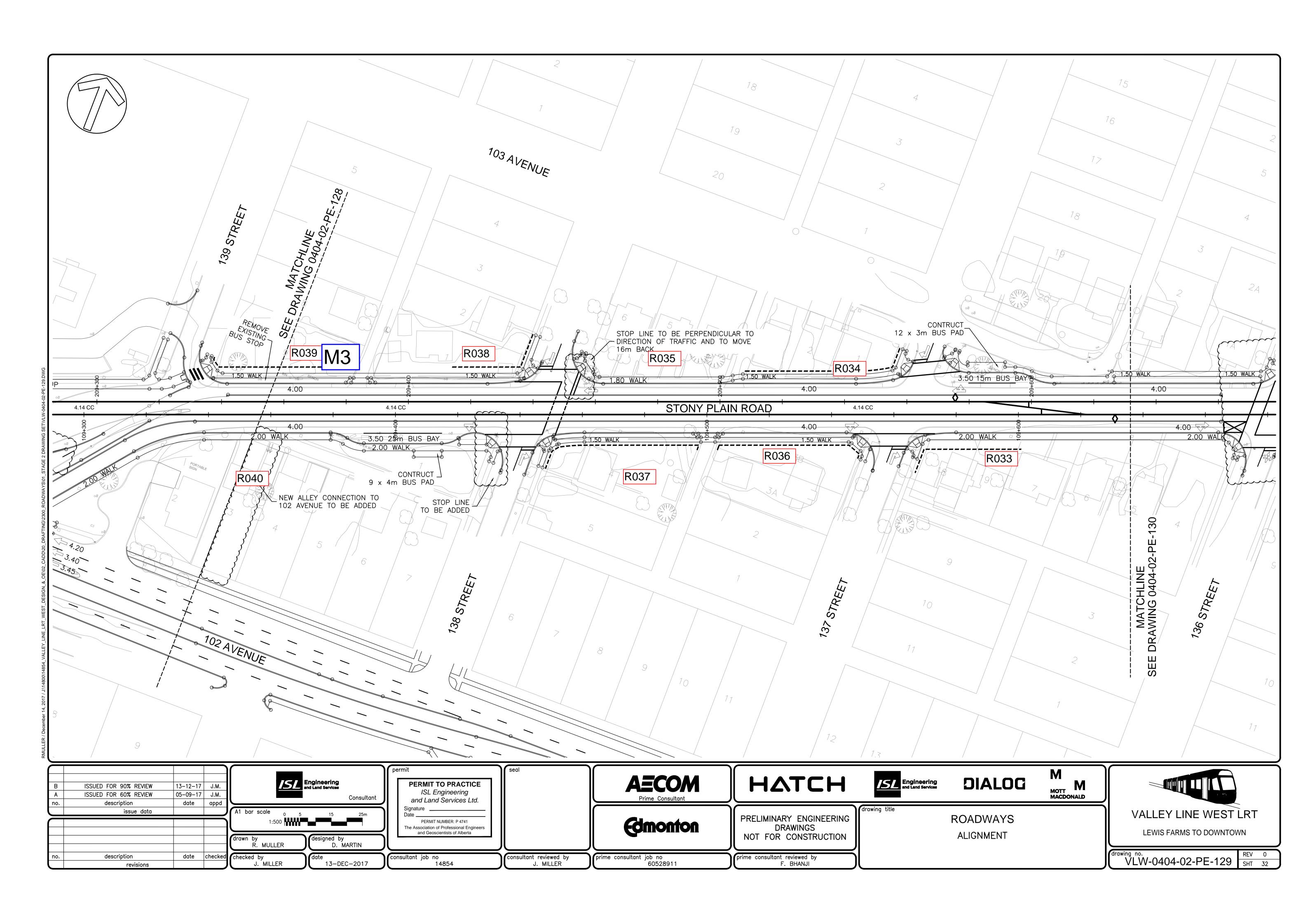


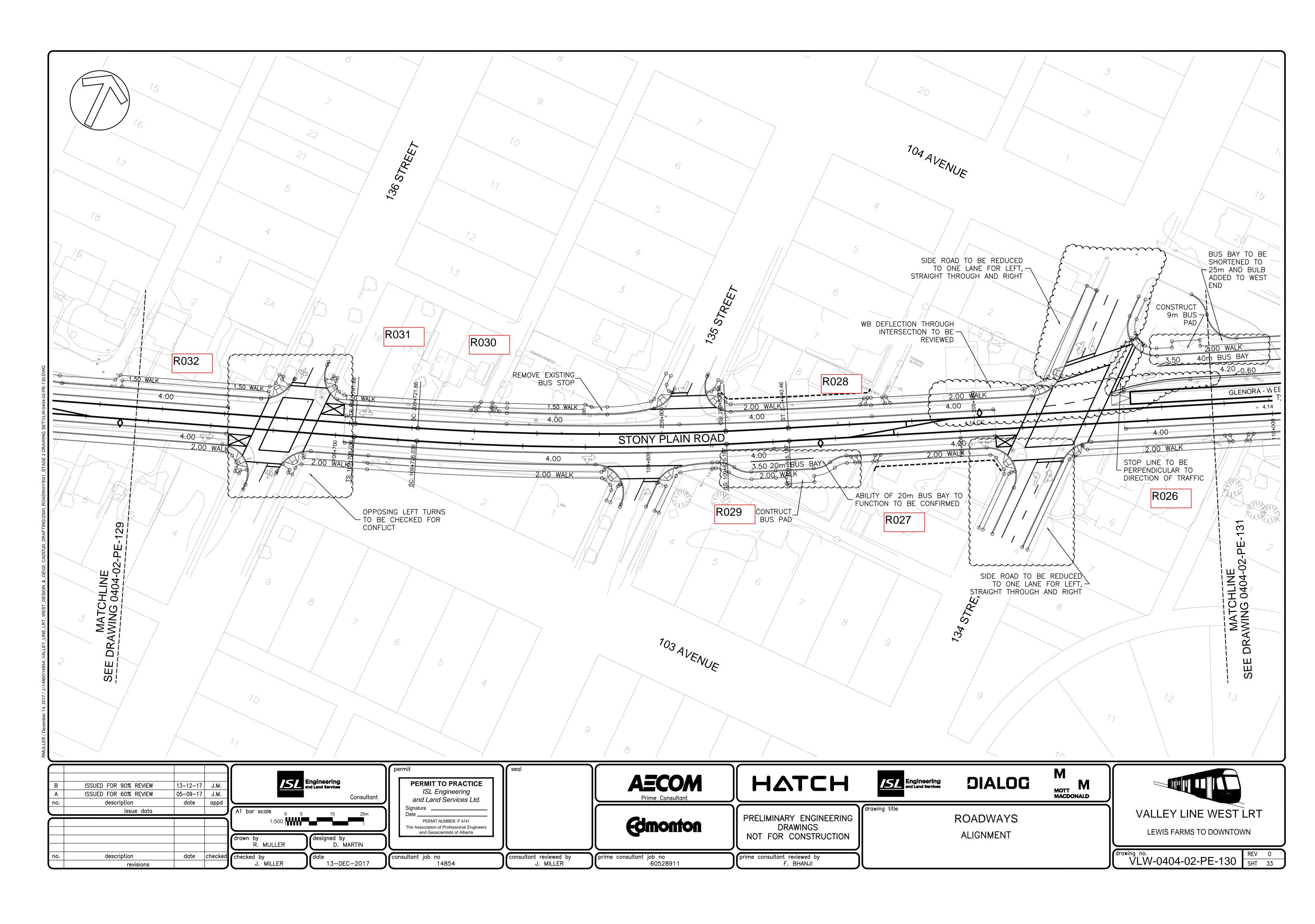


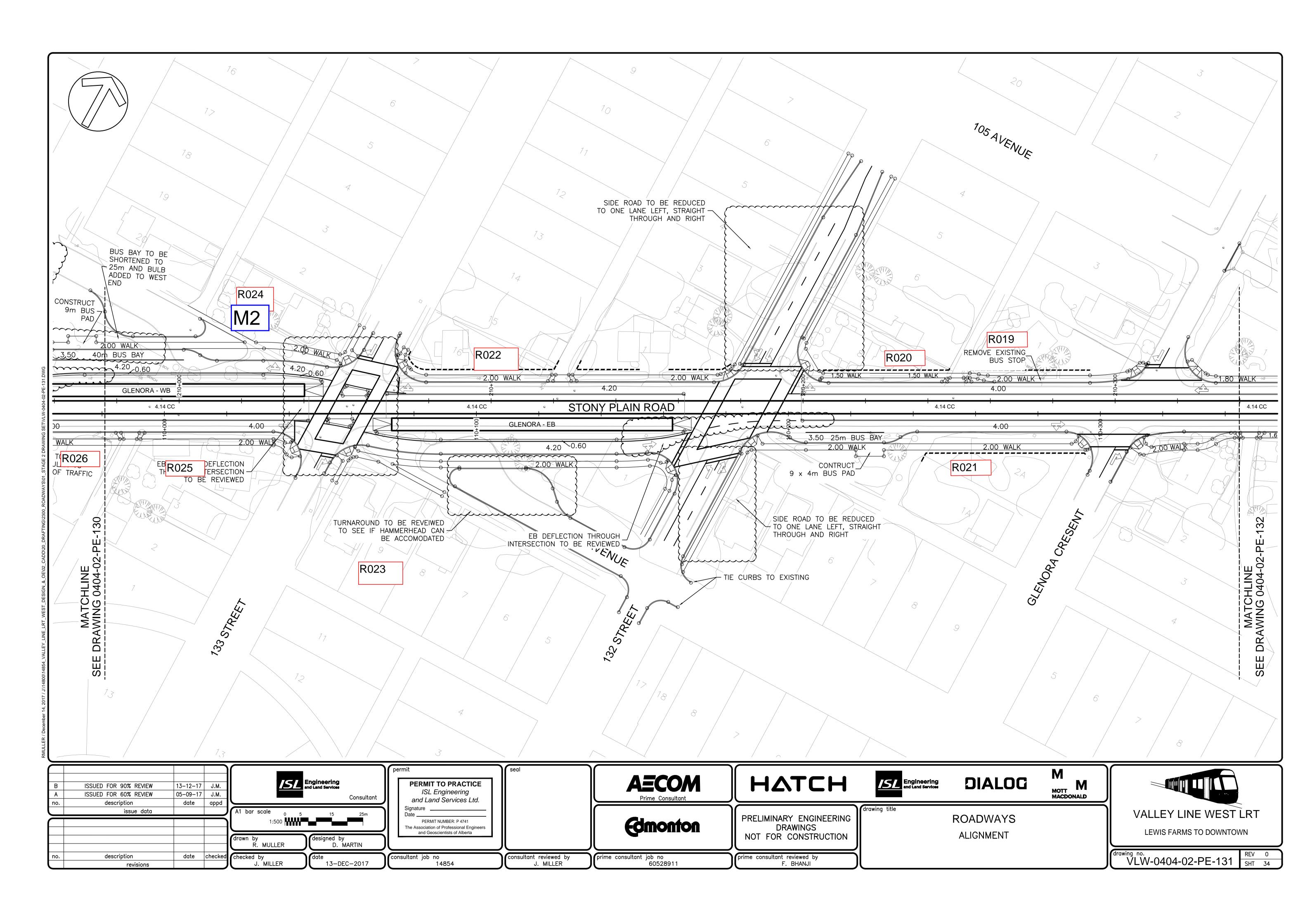


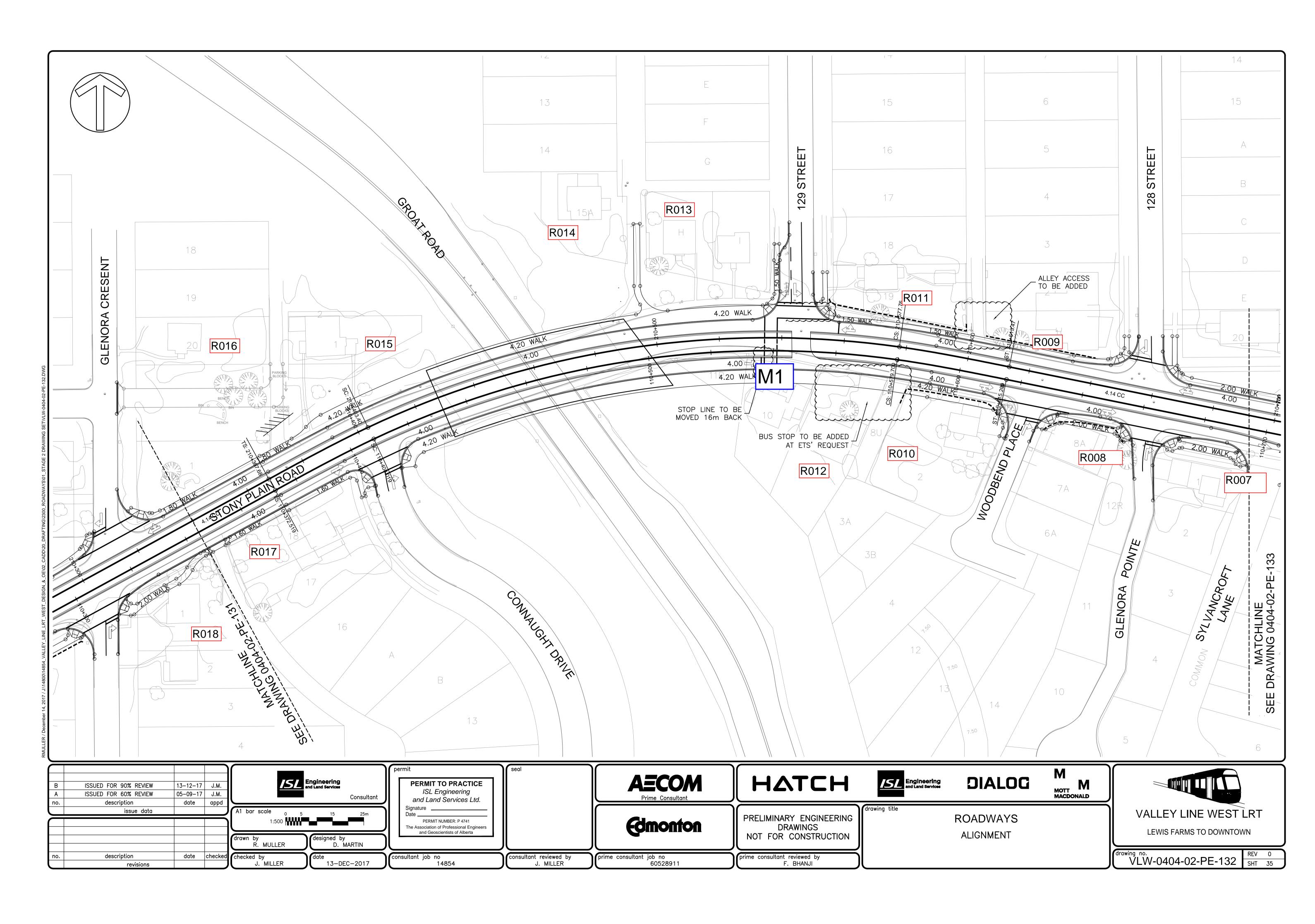


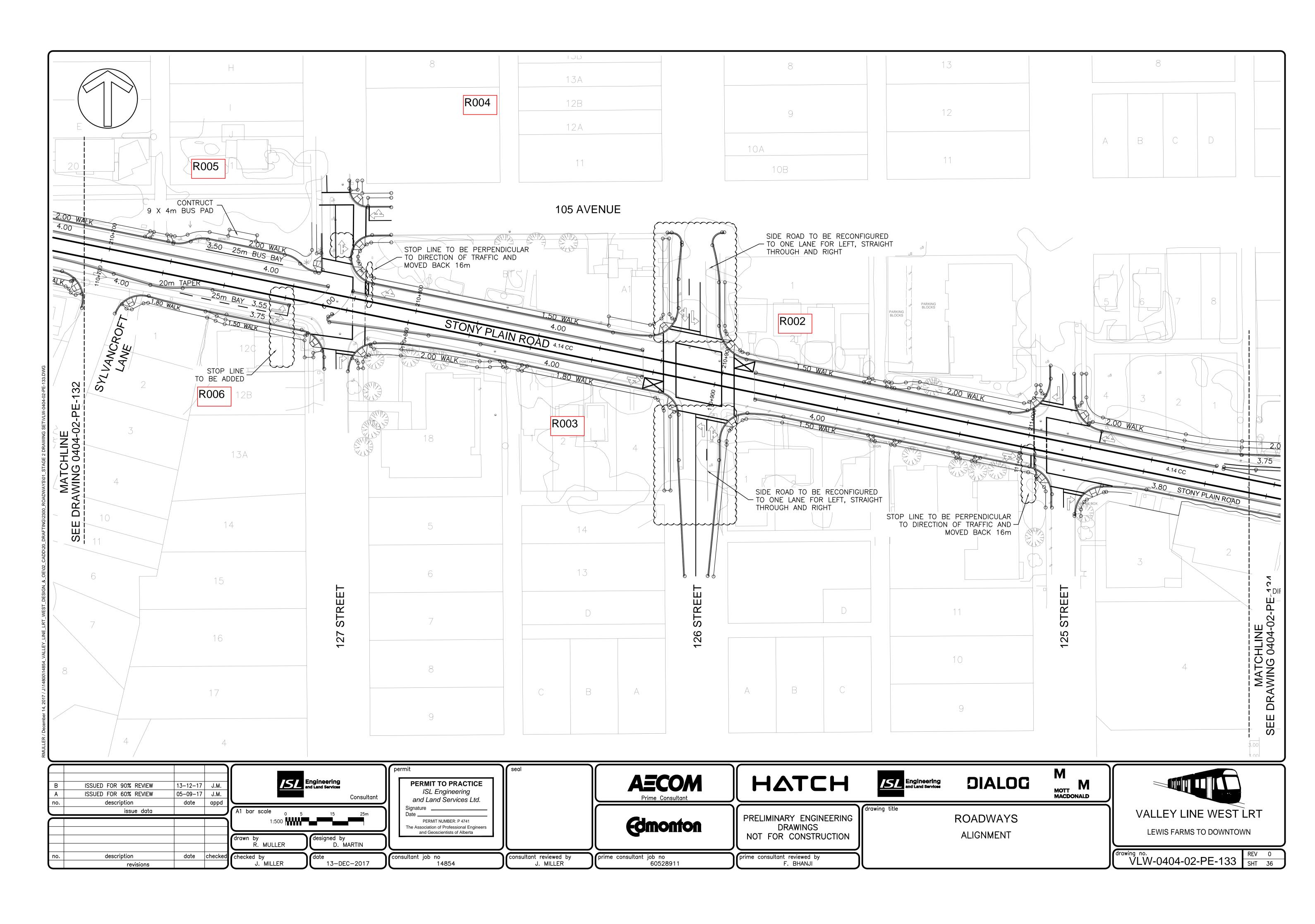


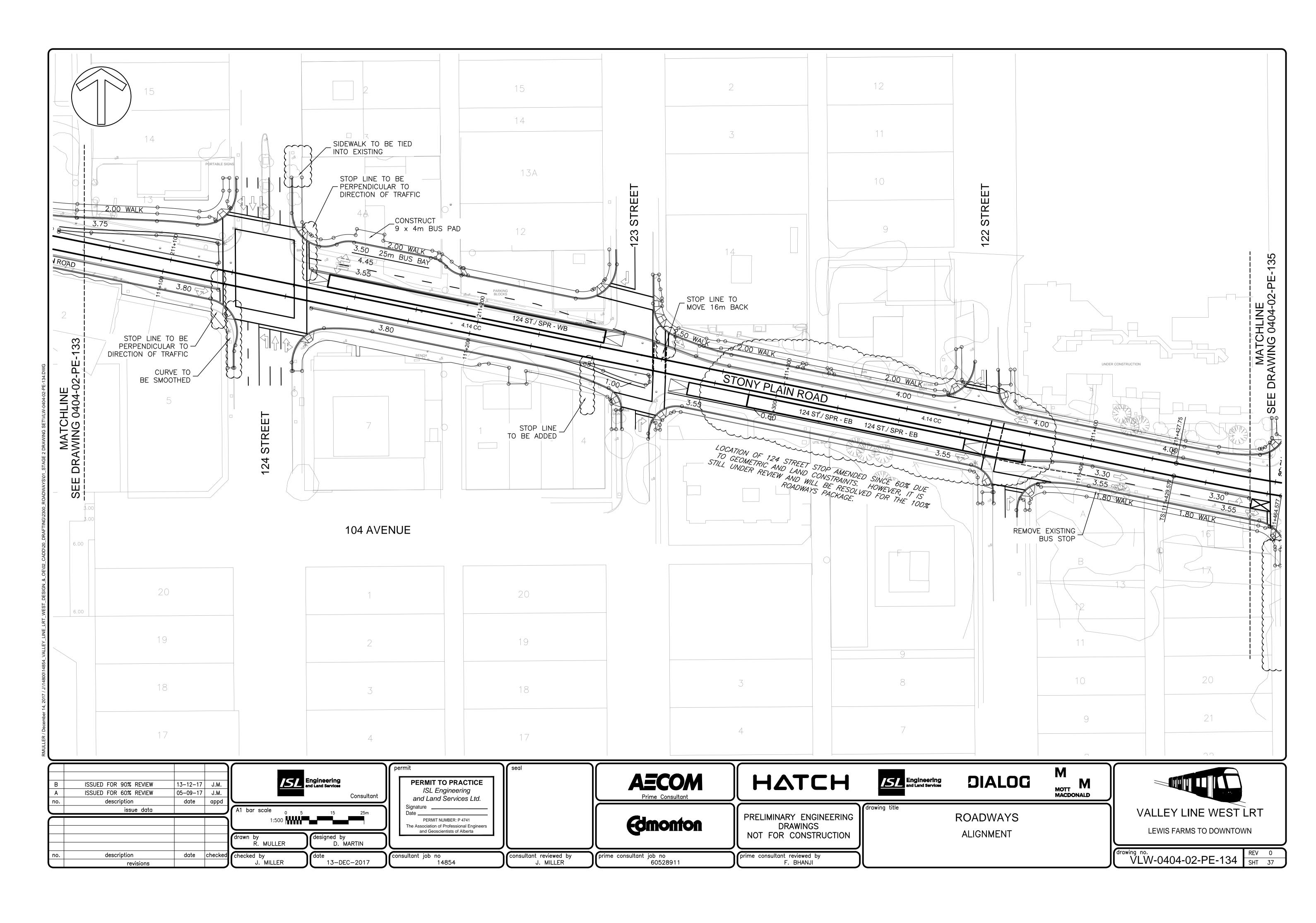


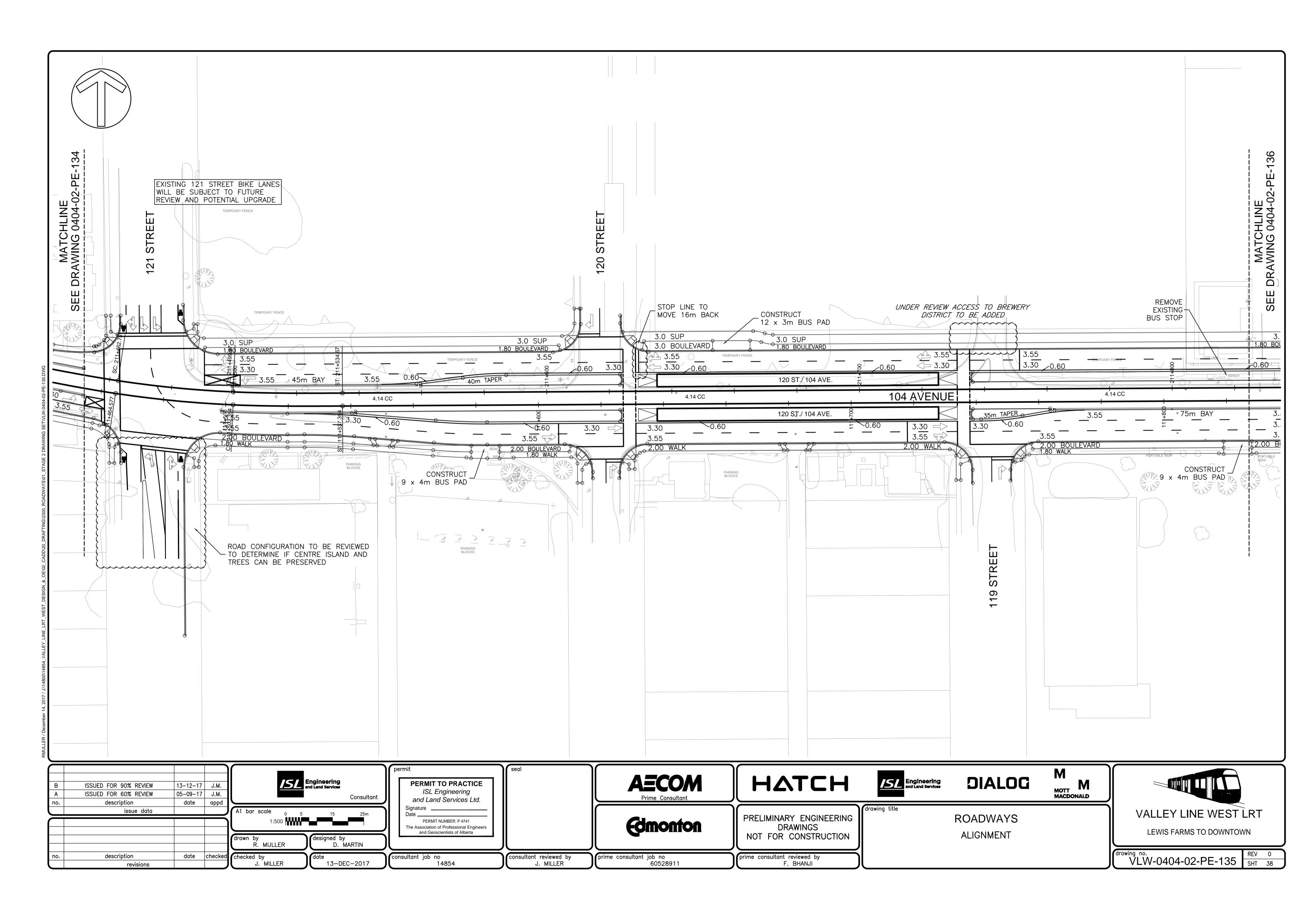


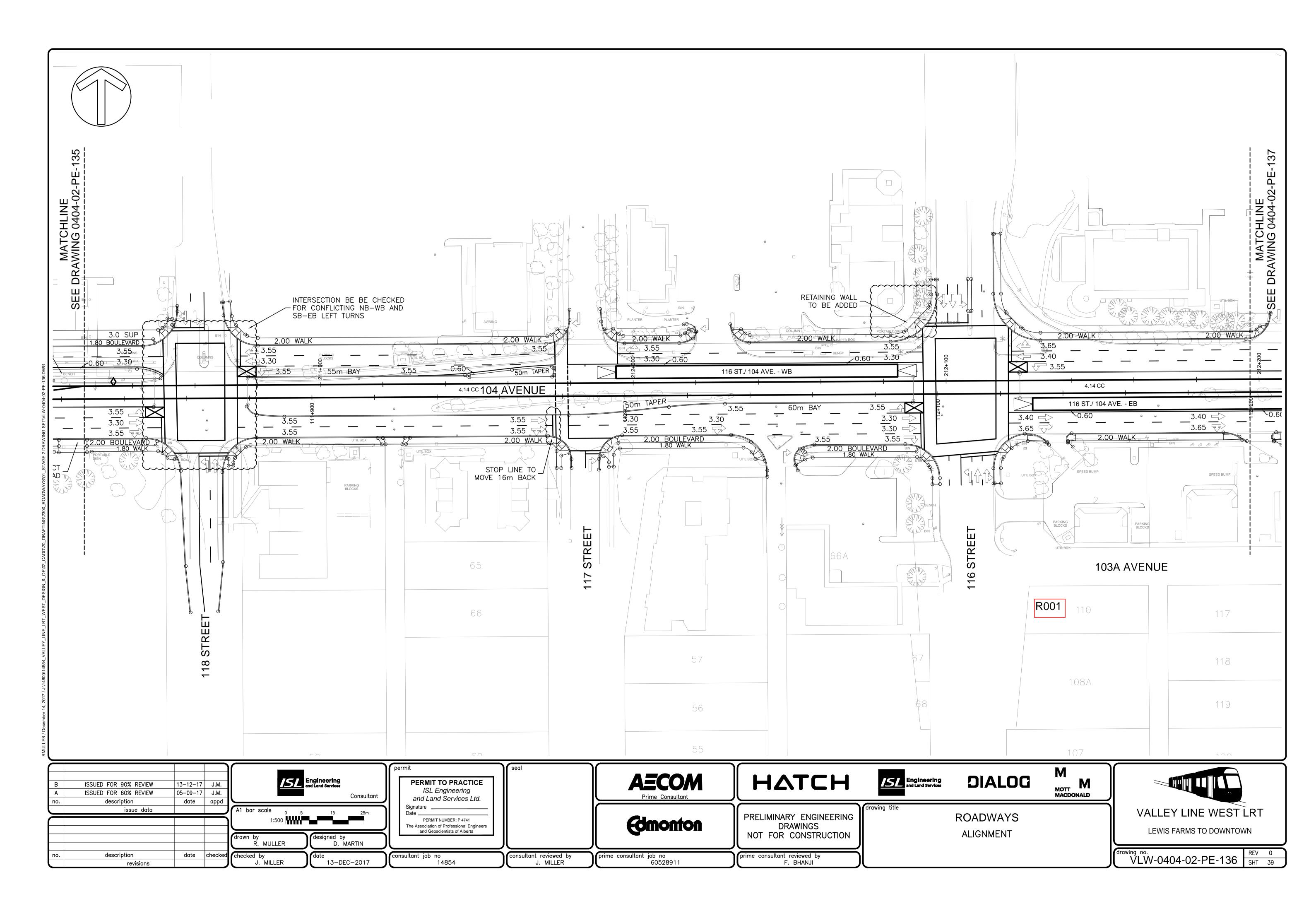


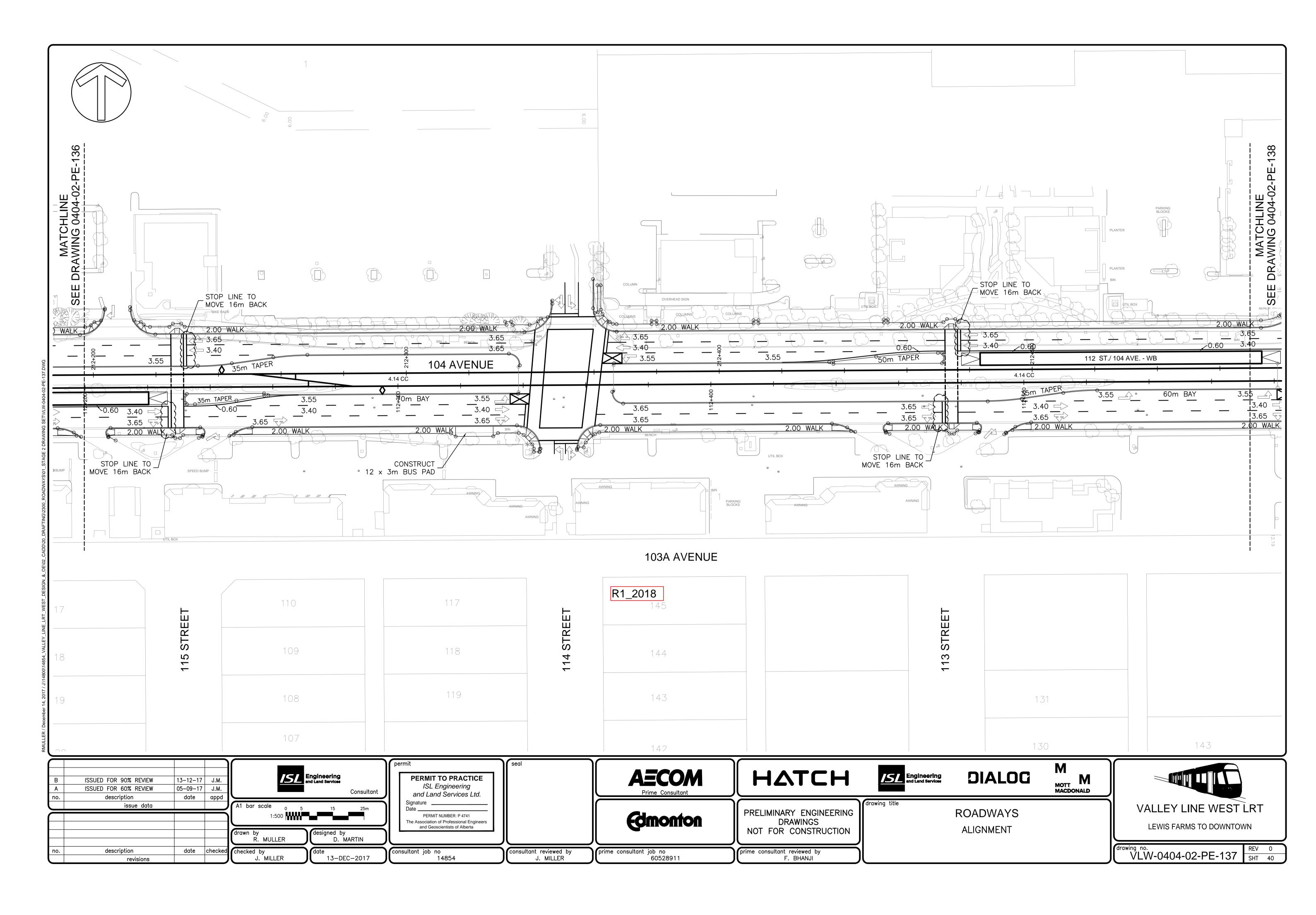


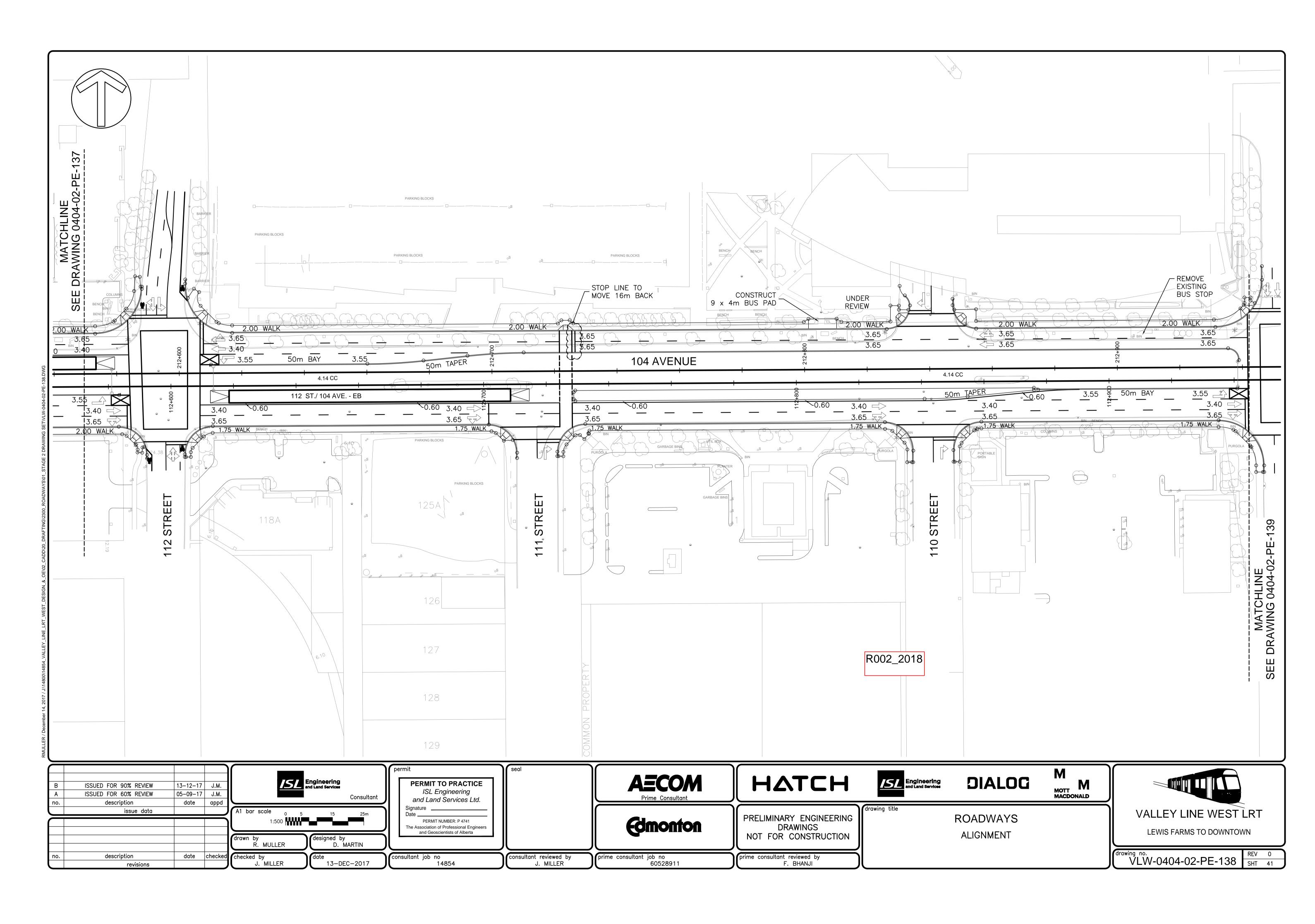


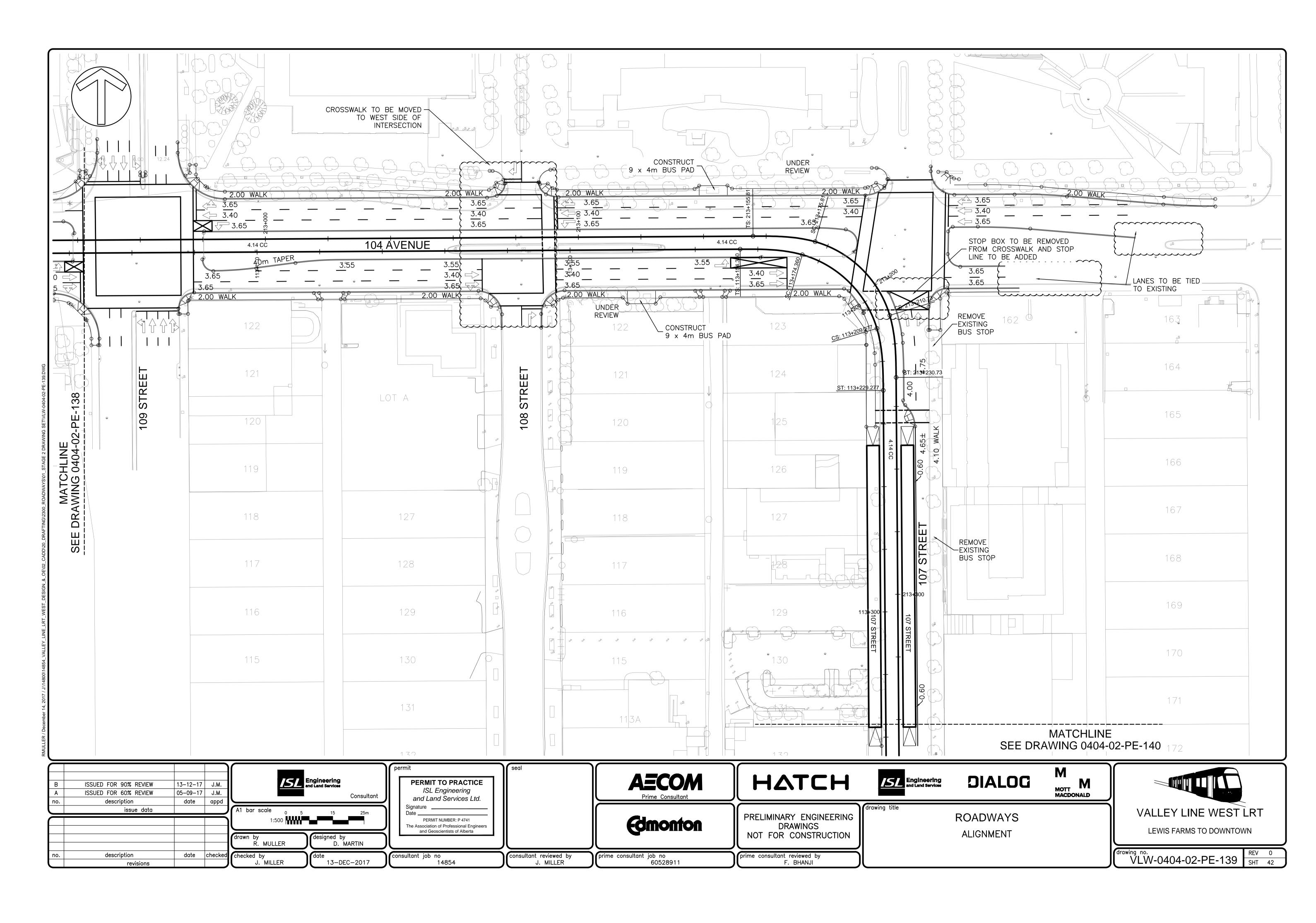


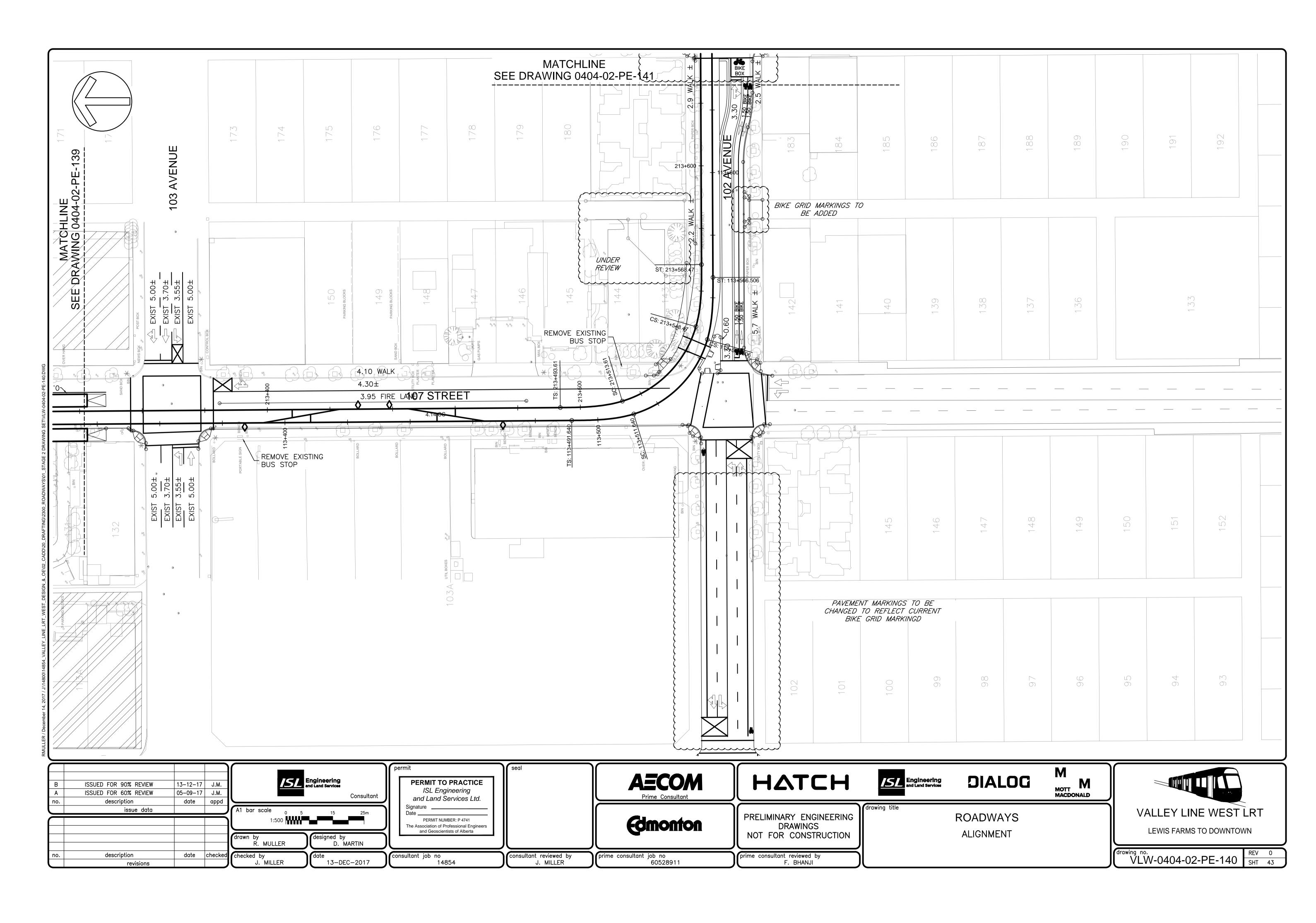


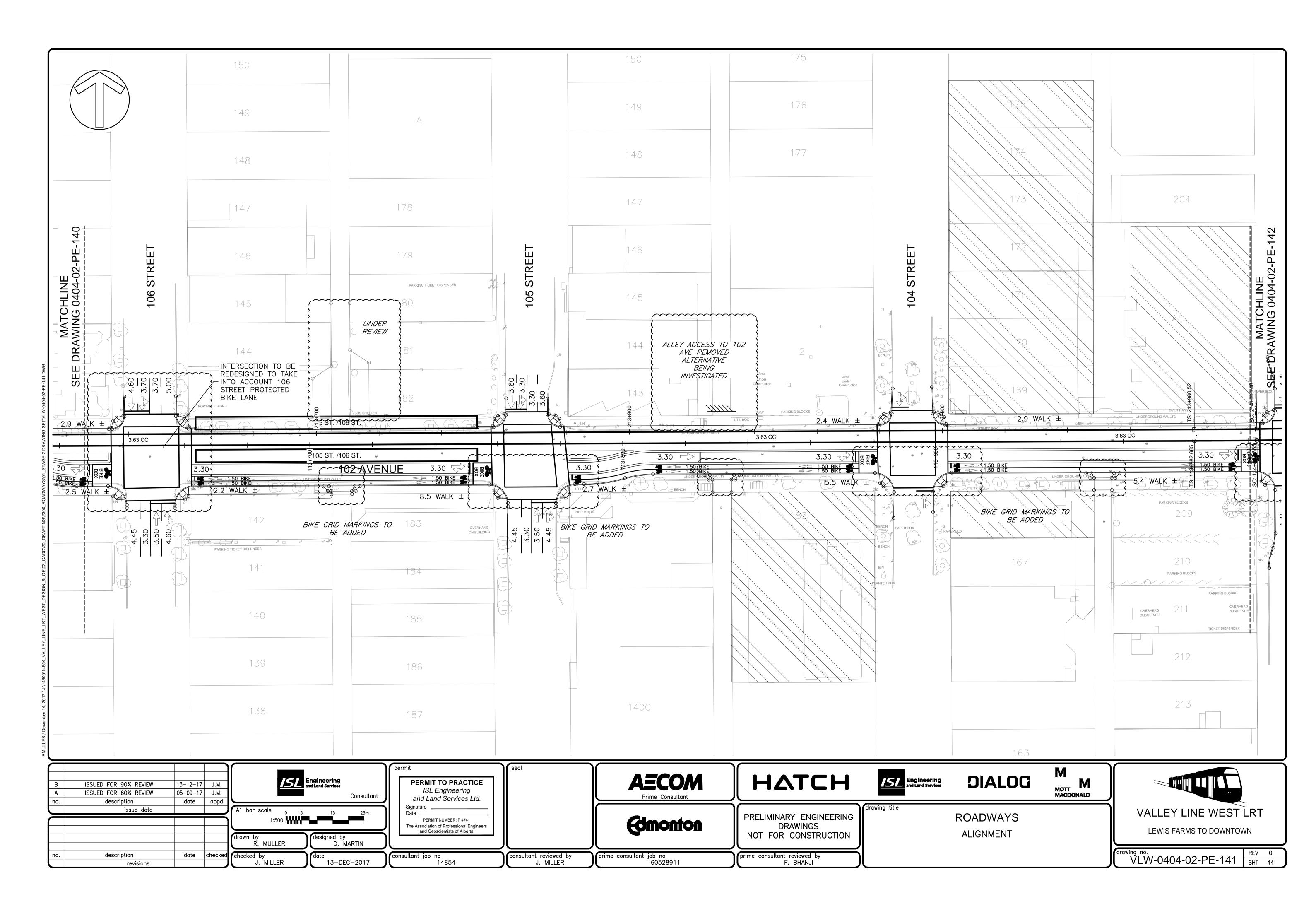












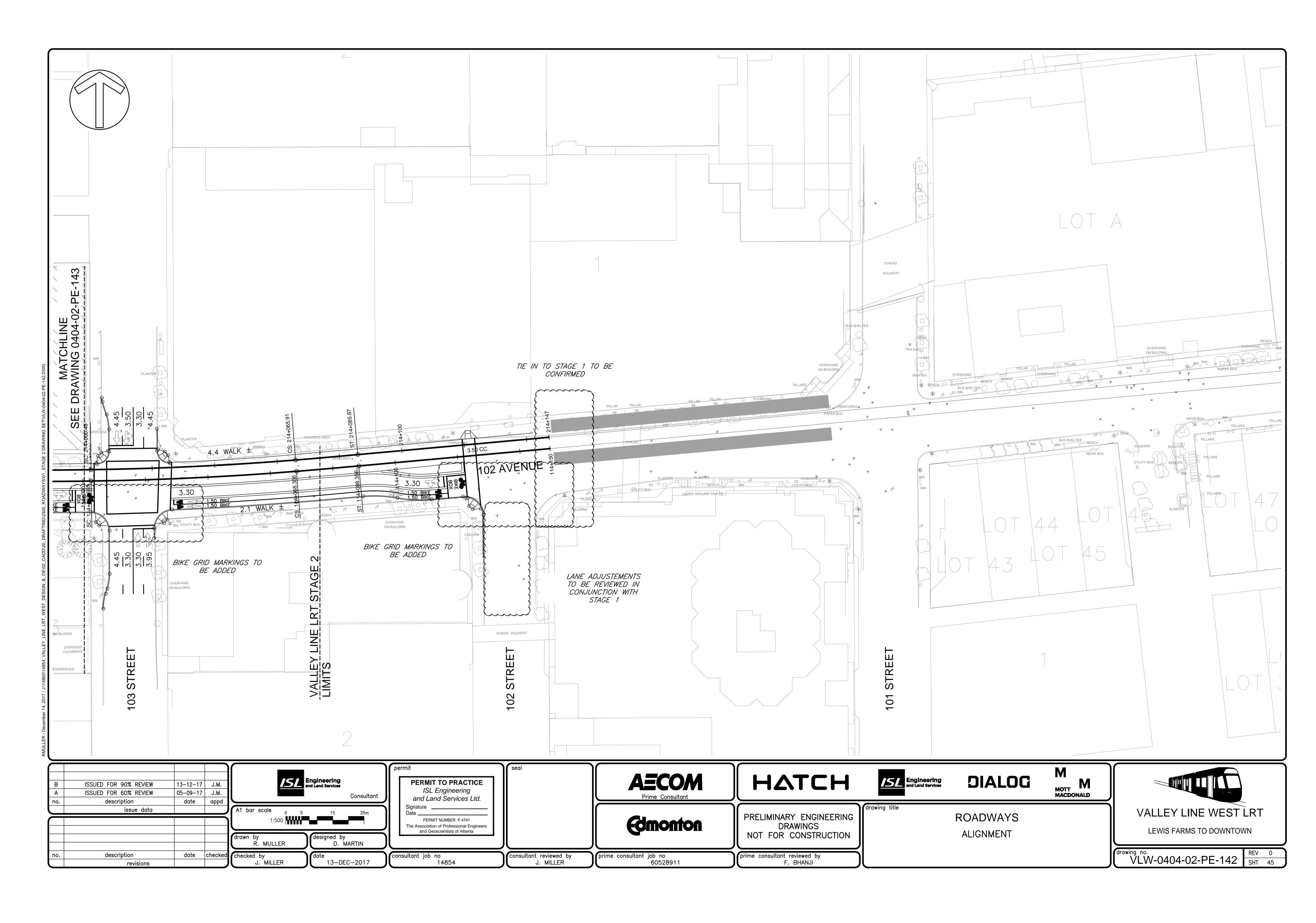
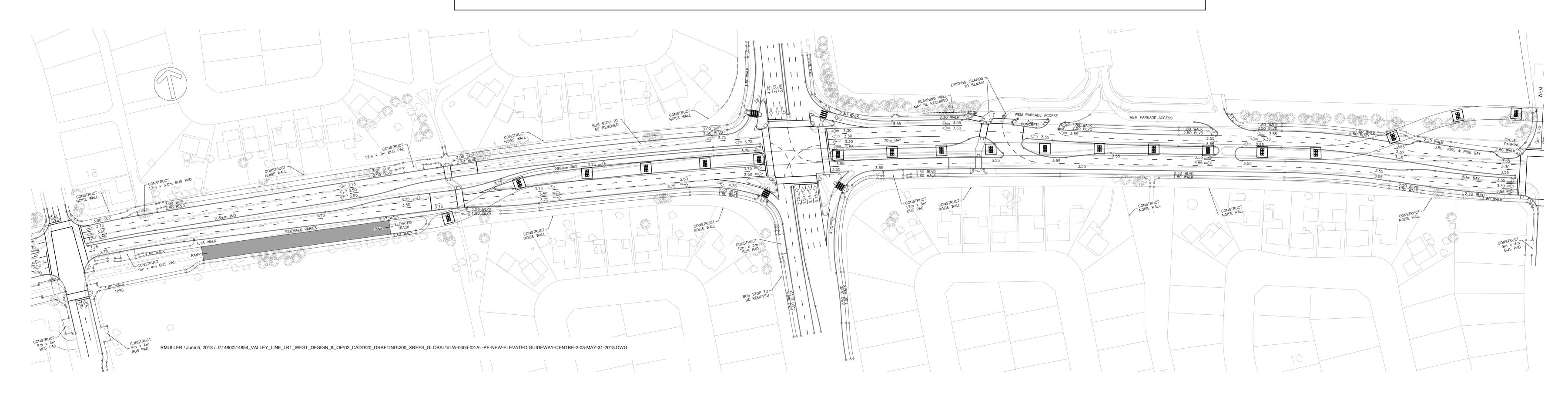
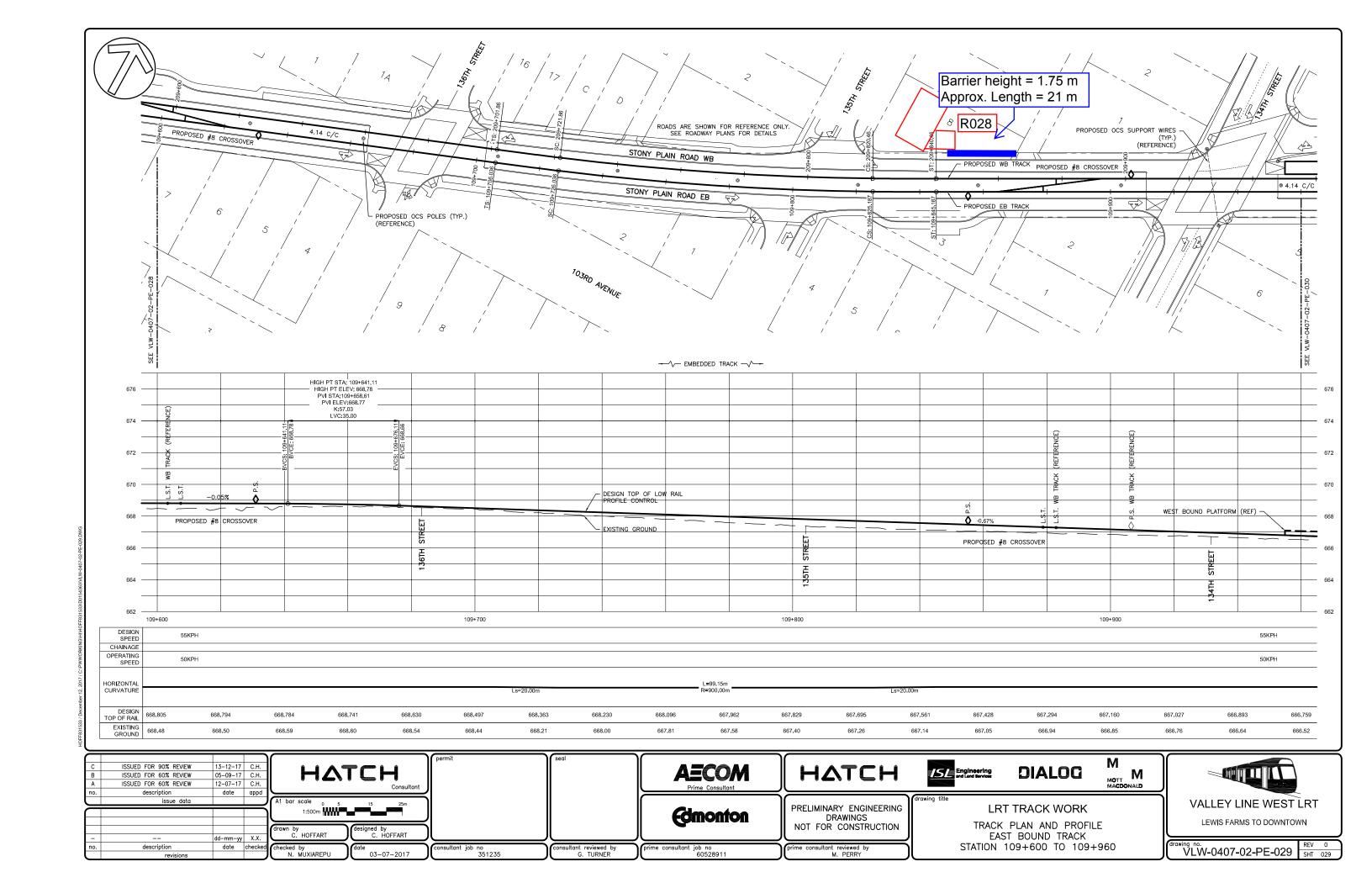


Figure B1-1 - Updated Elevated Track Section (June 2018)

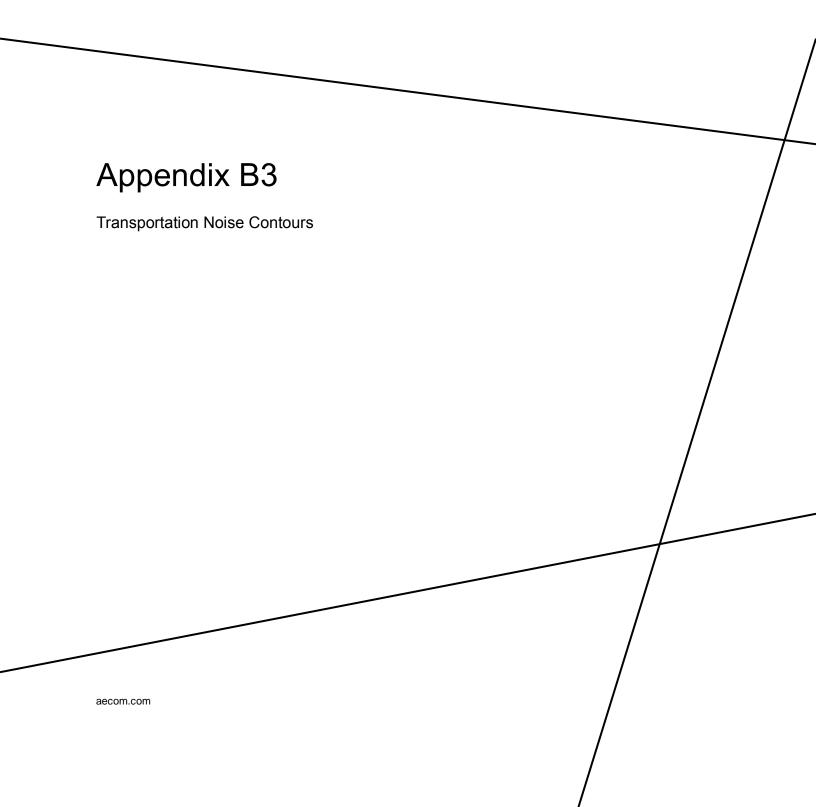


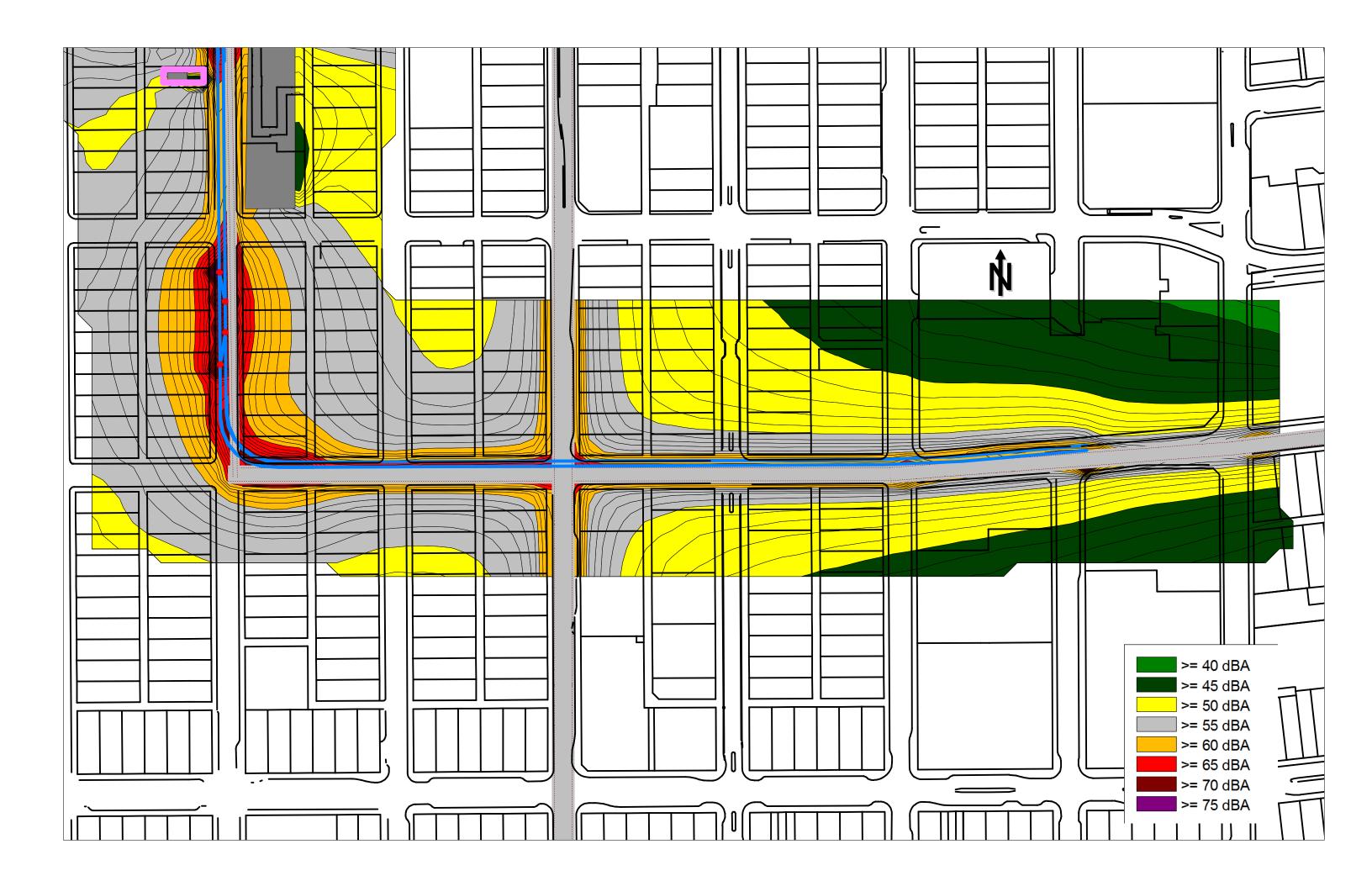


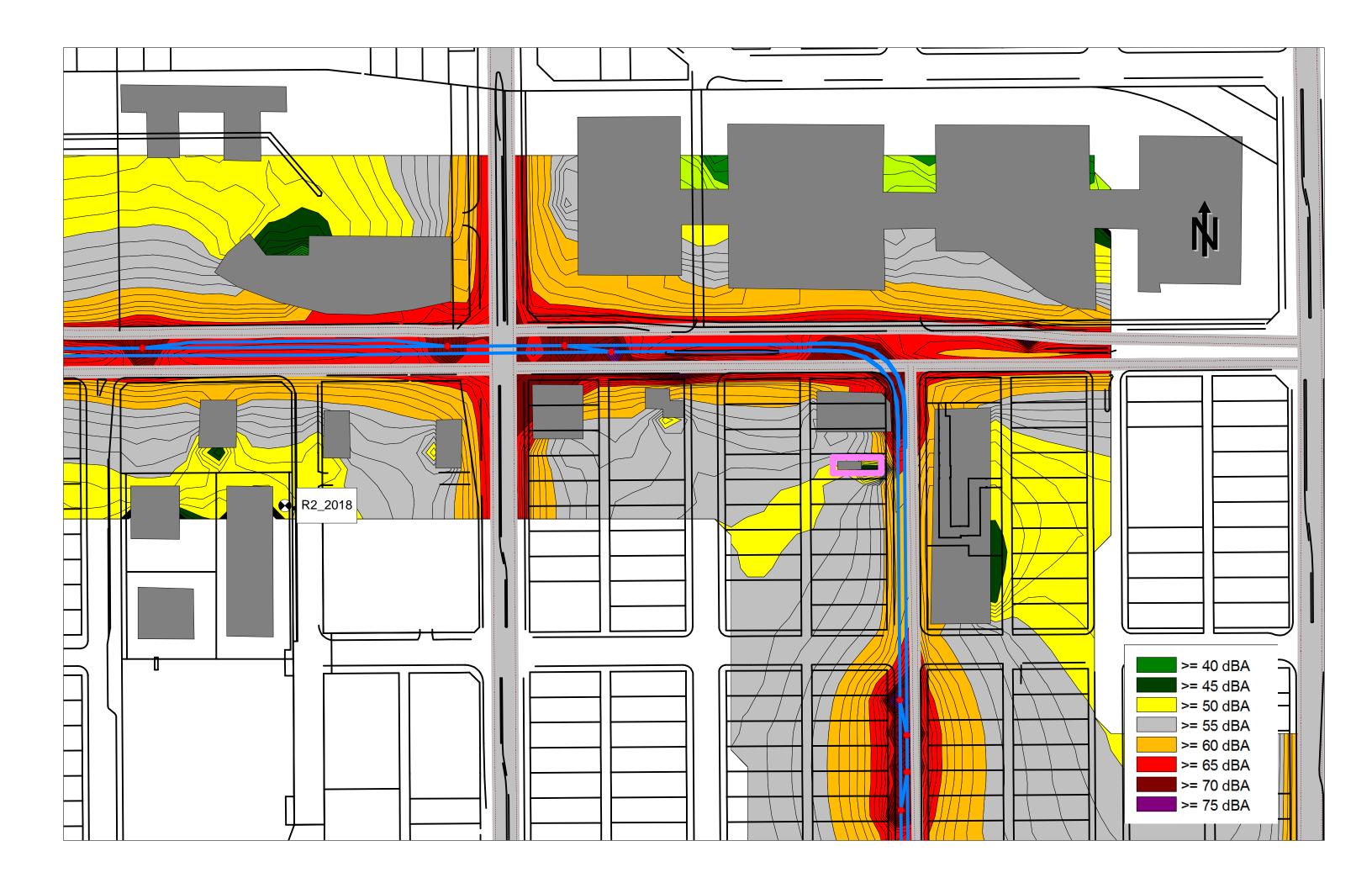
Appendix B2 Transportation Noise Mitigation – Barrier Locations aecom.com

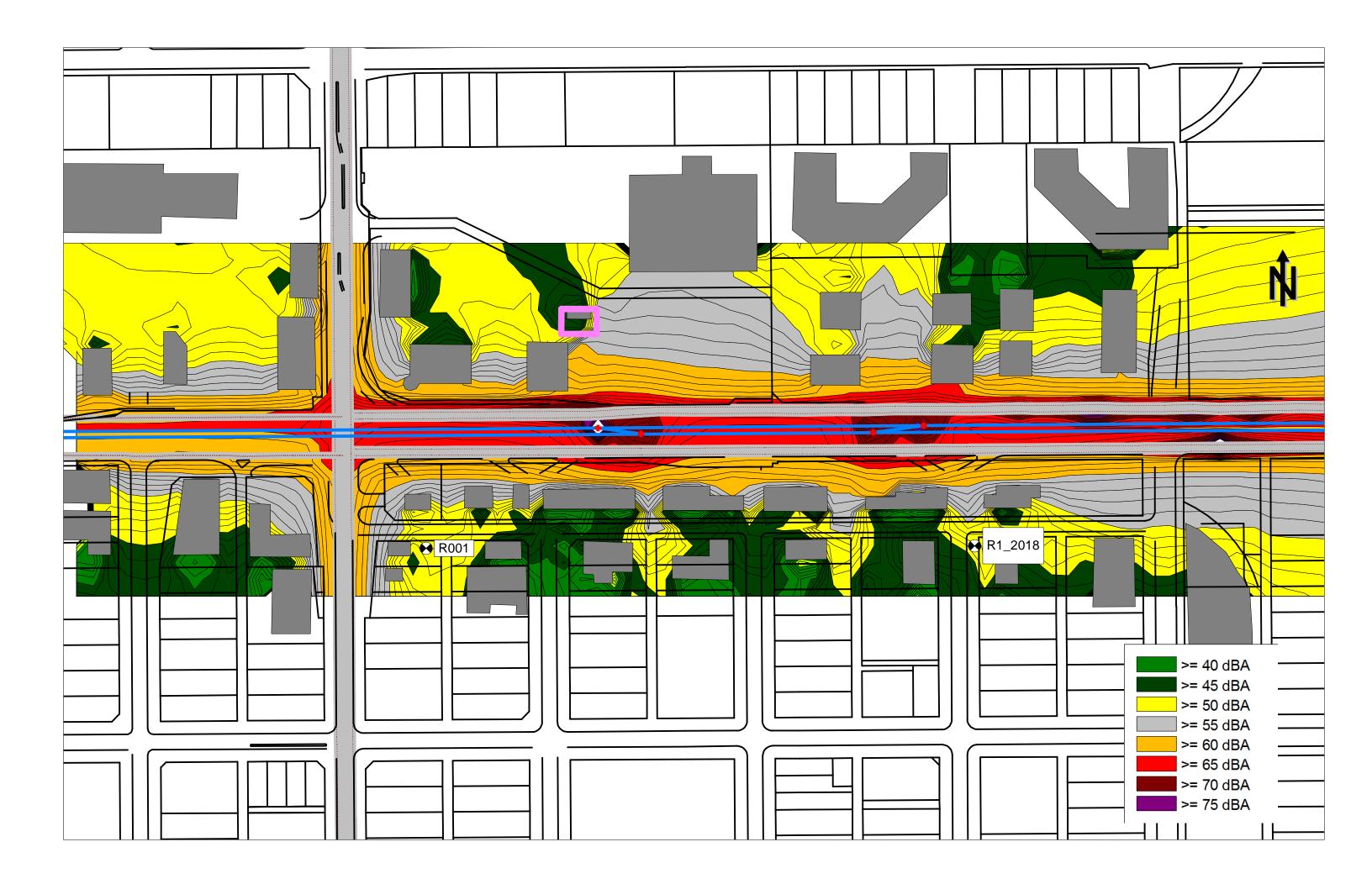


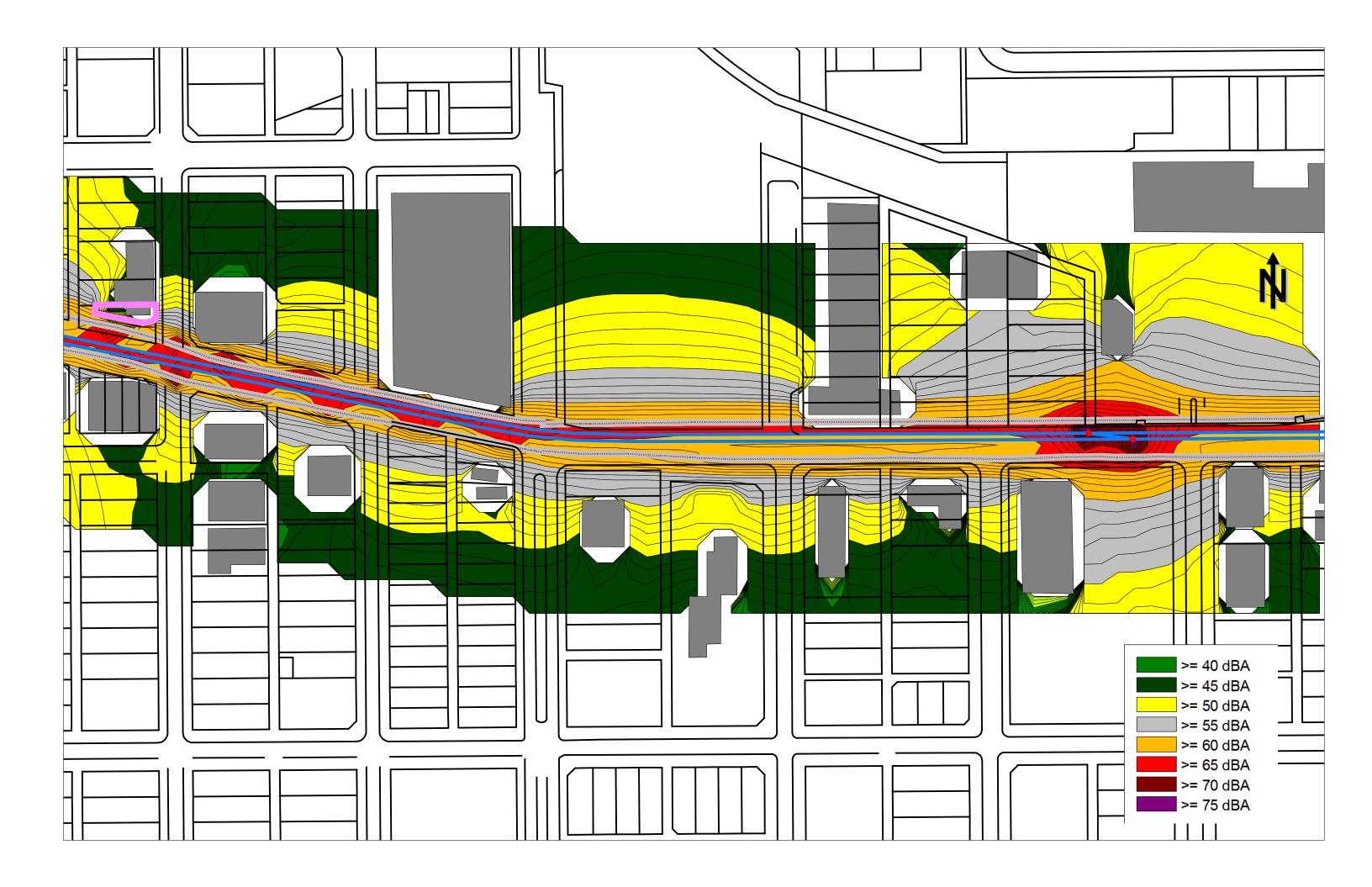




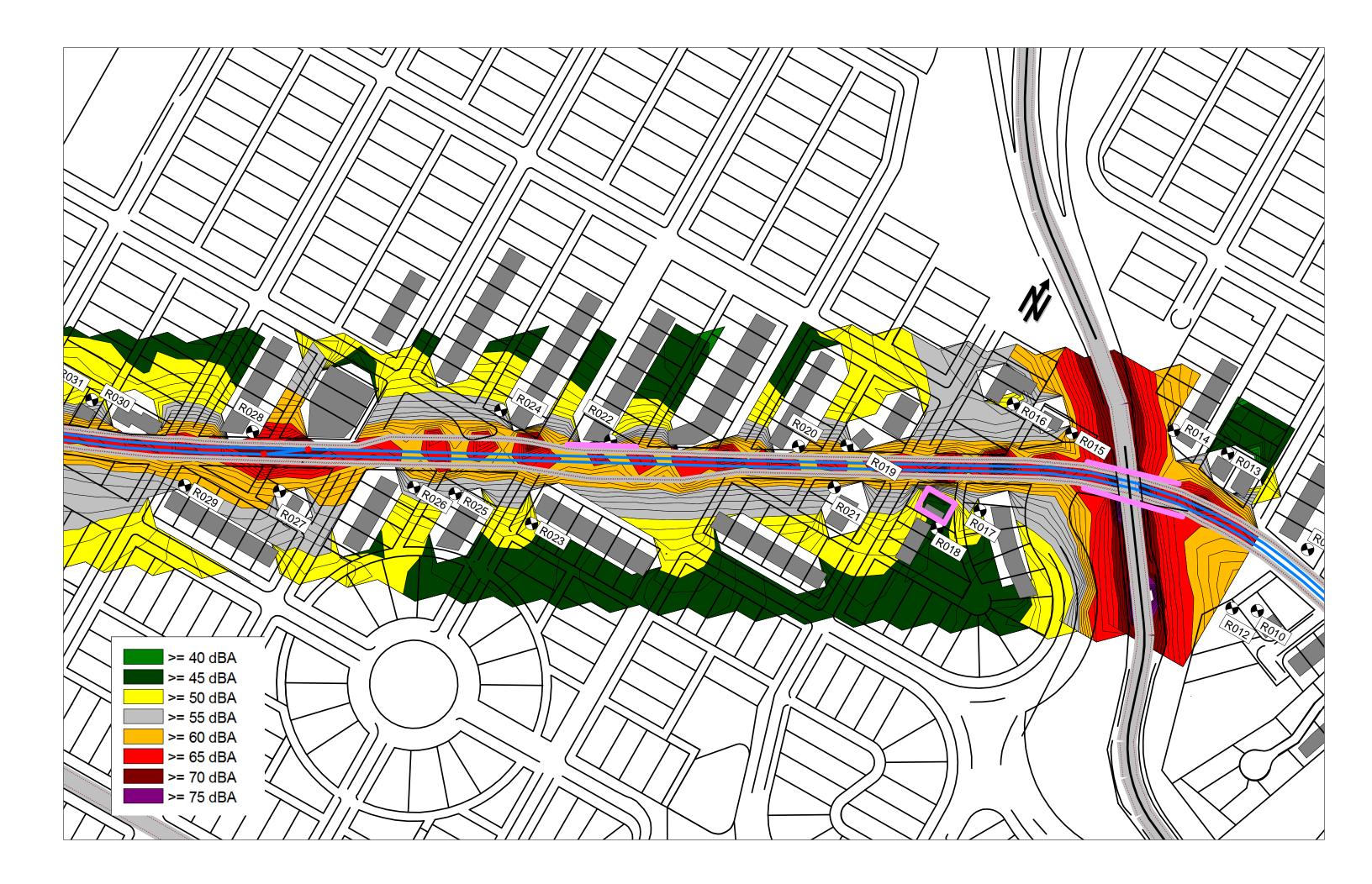




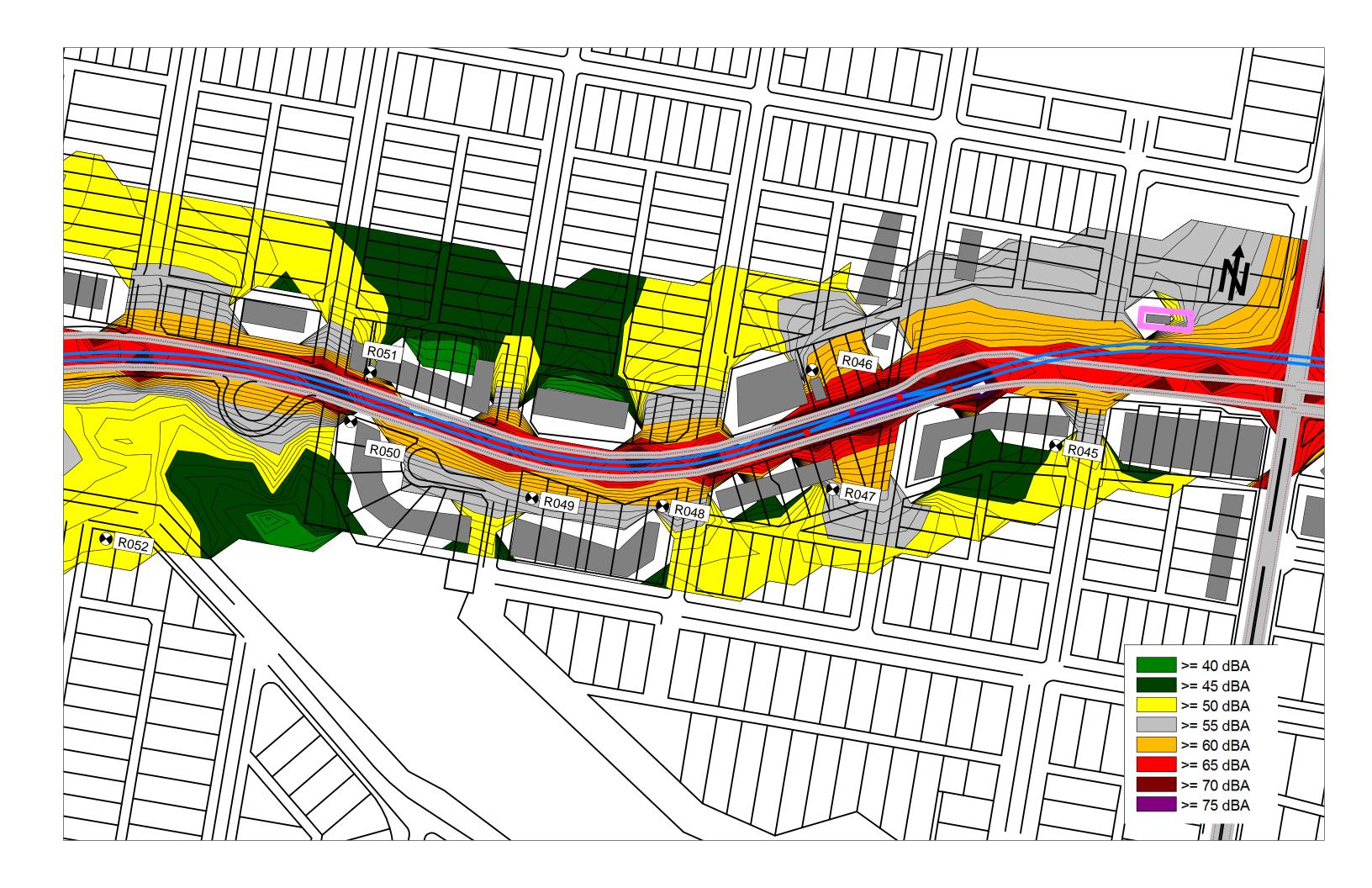


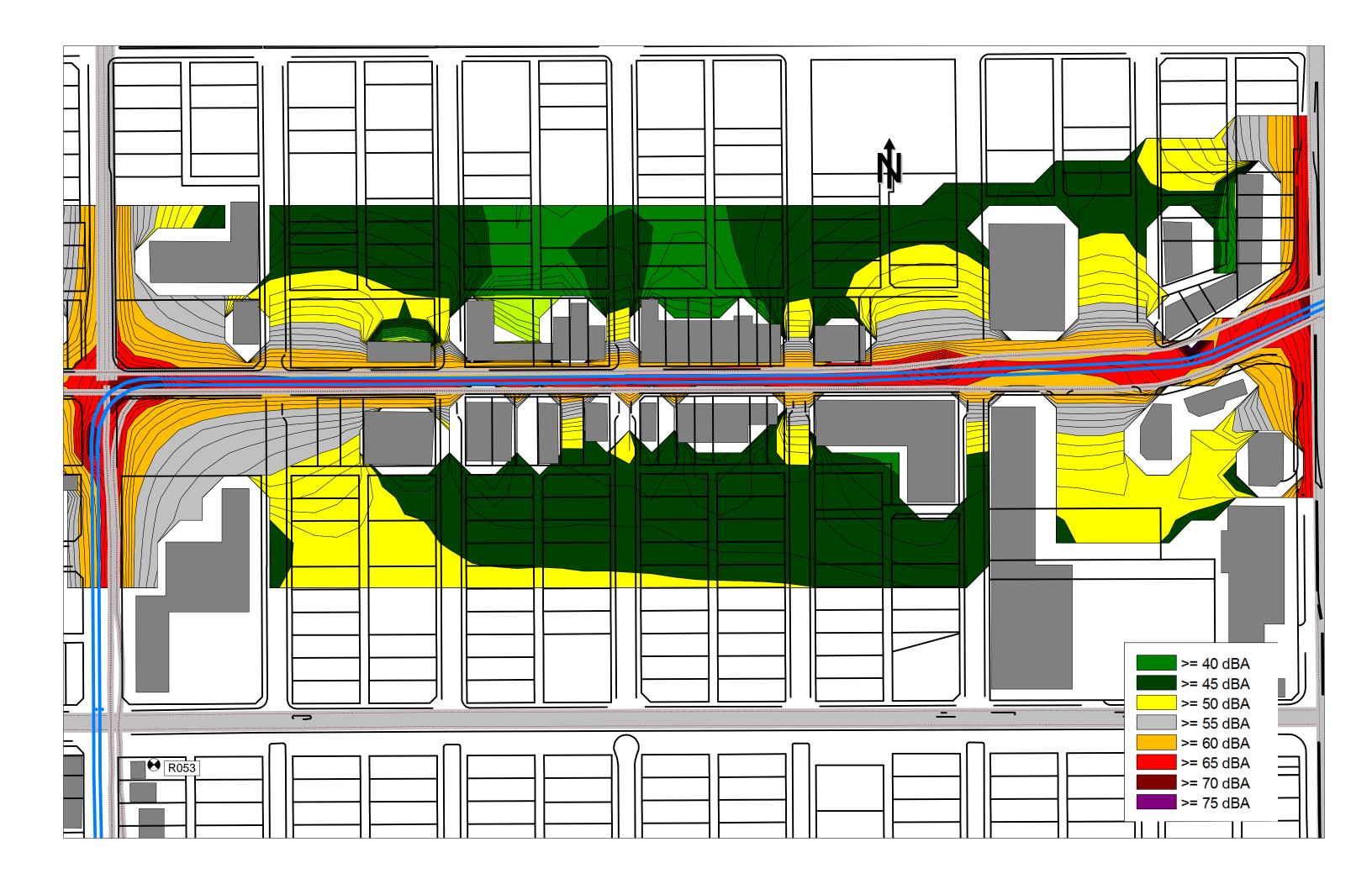


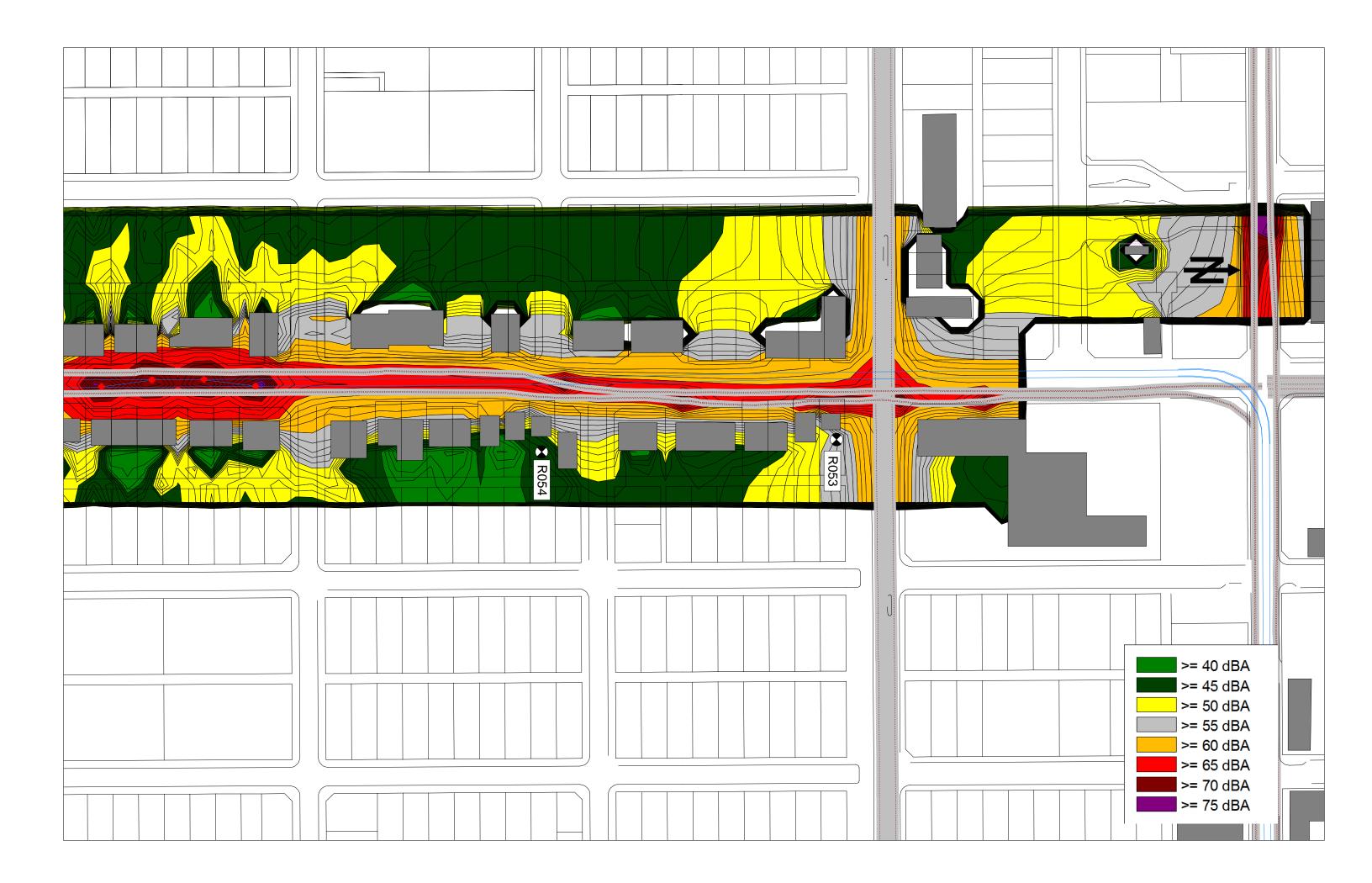


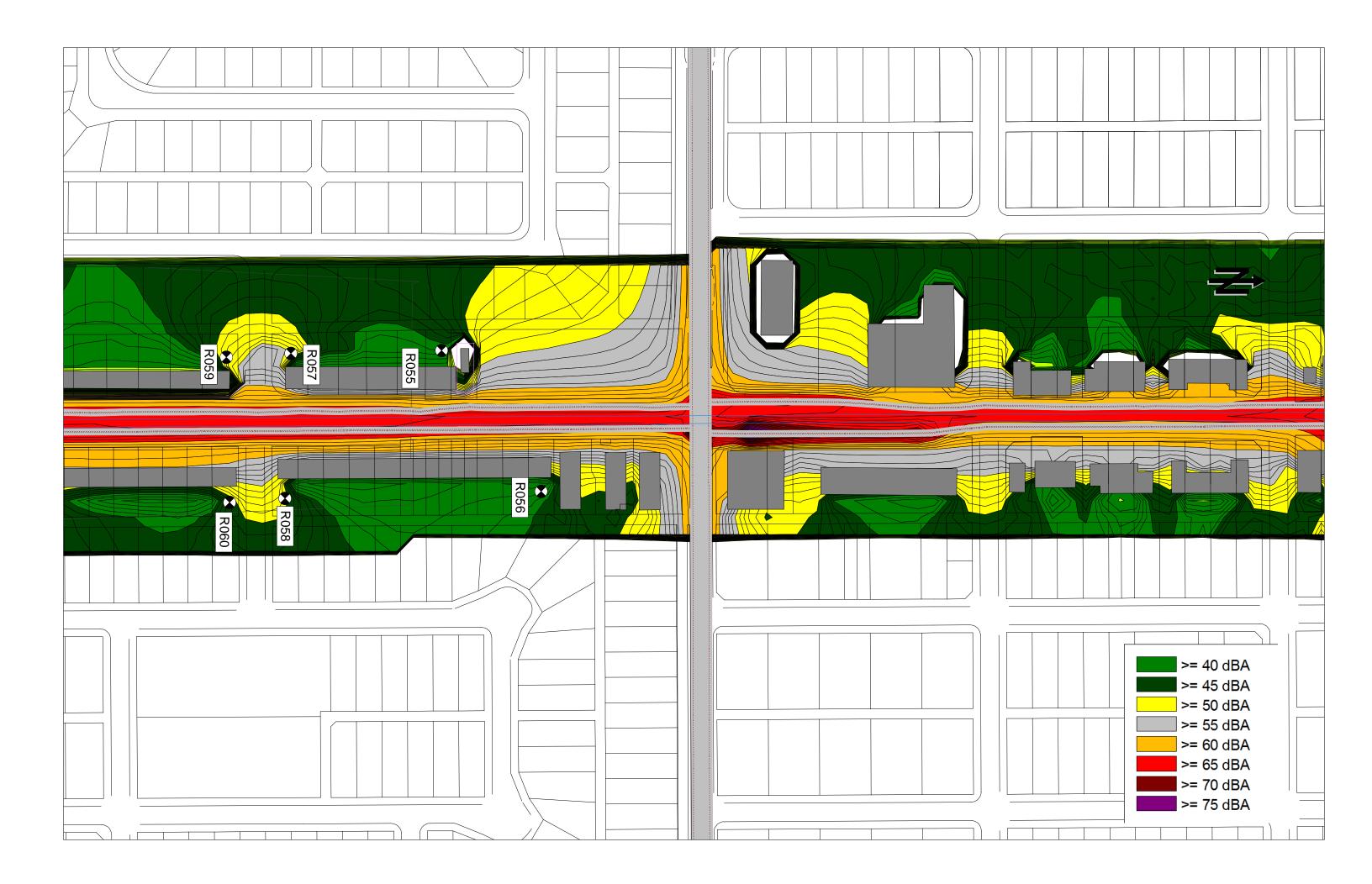




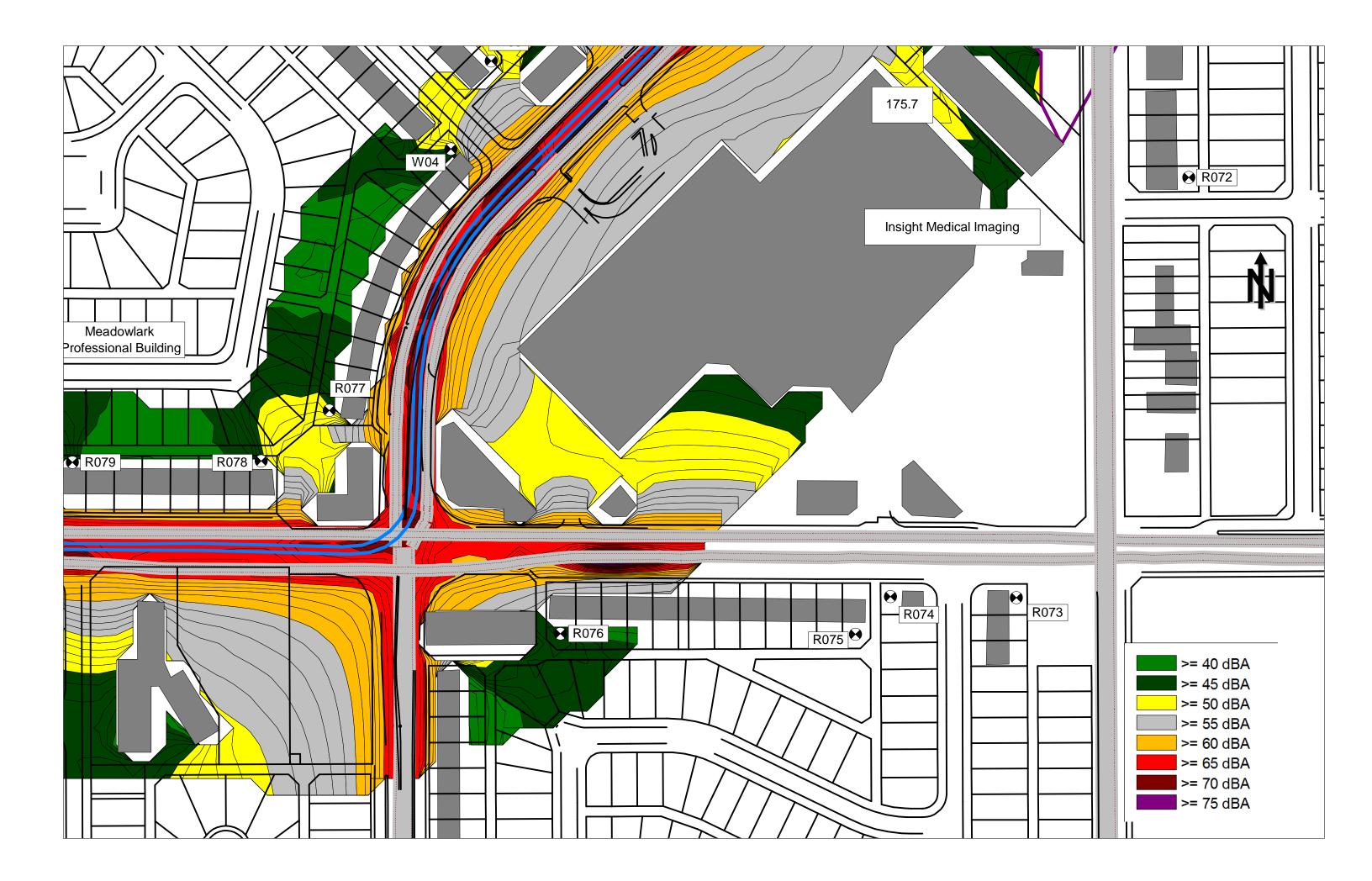


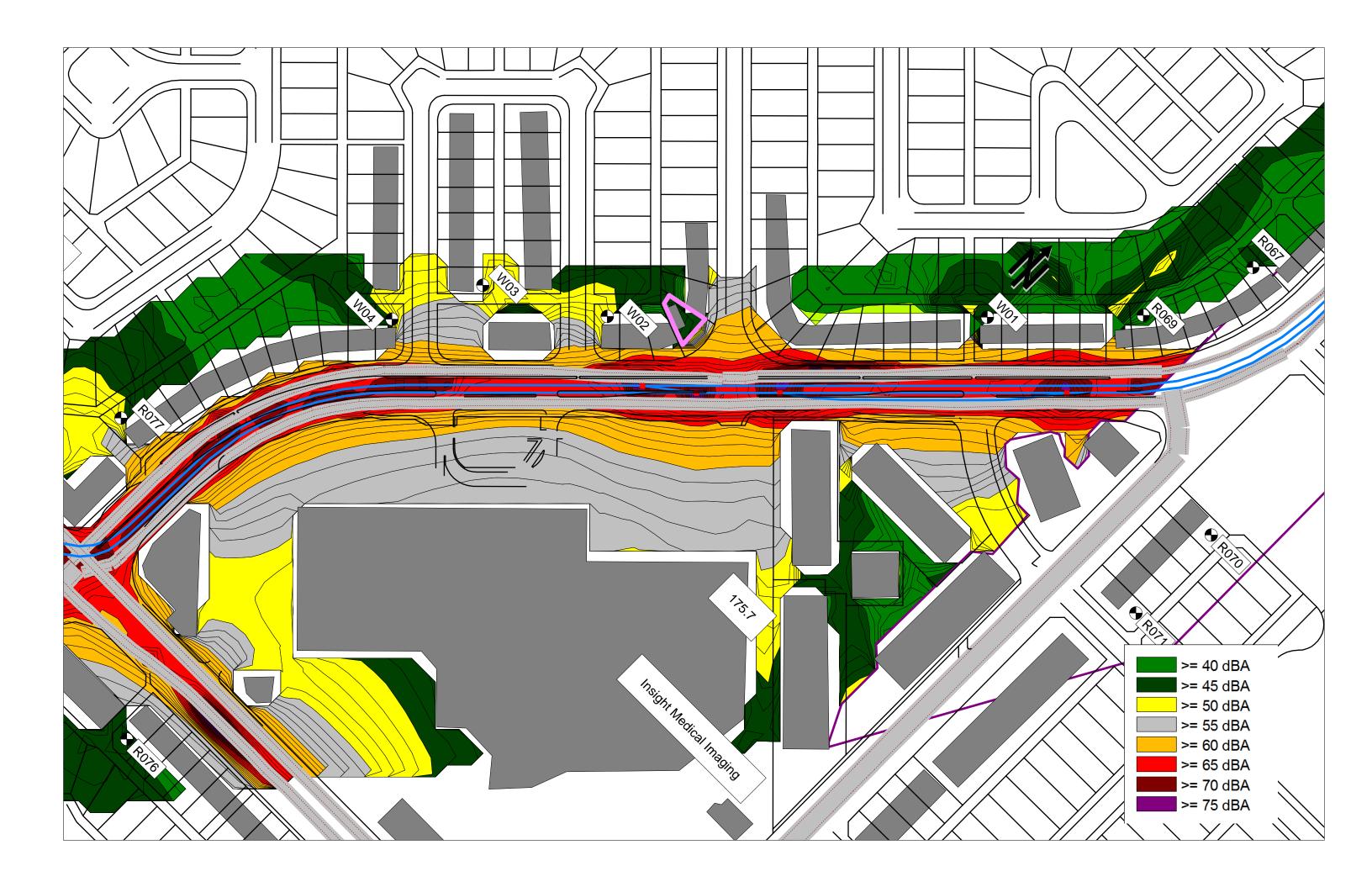


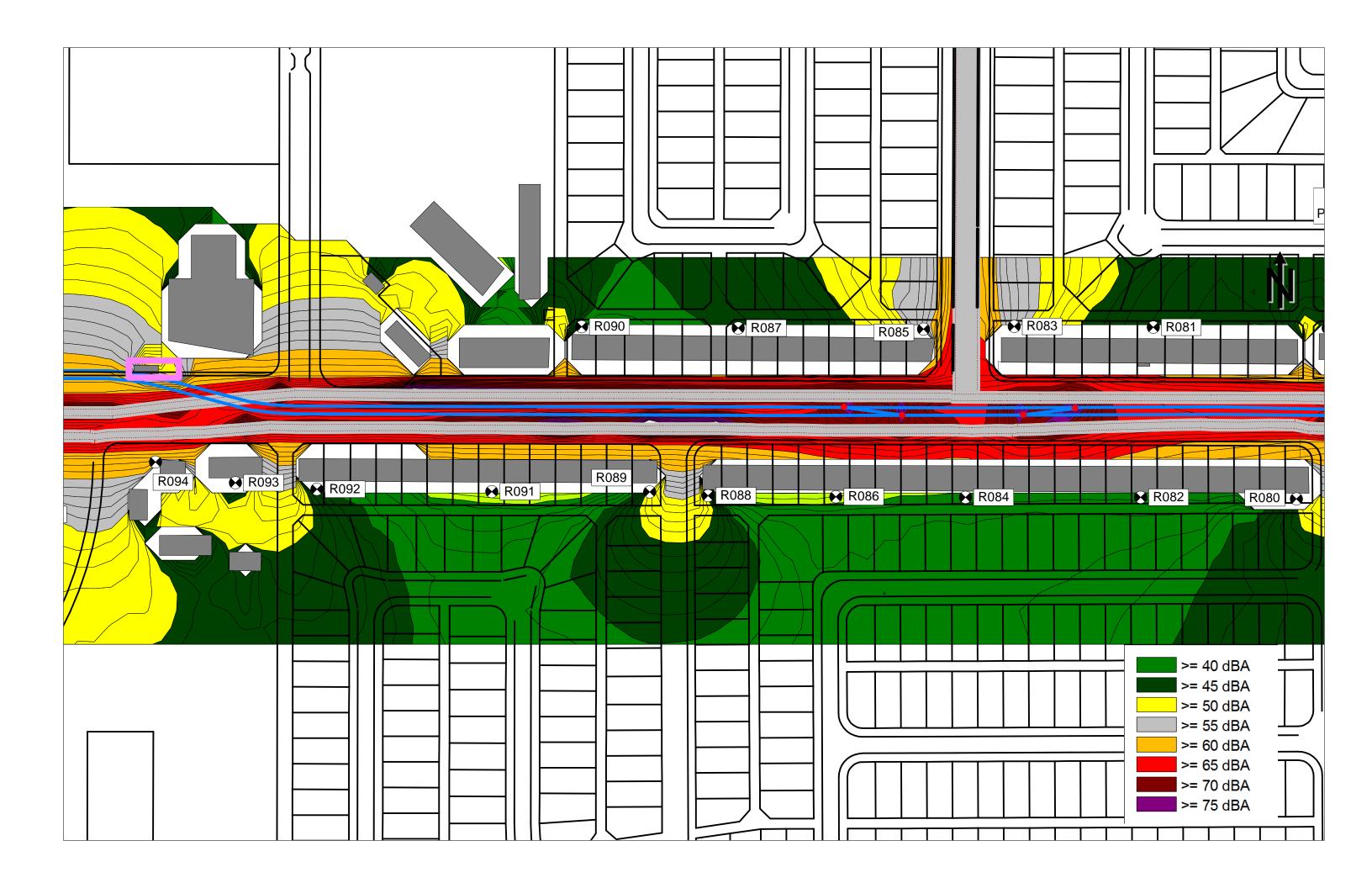


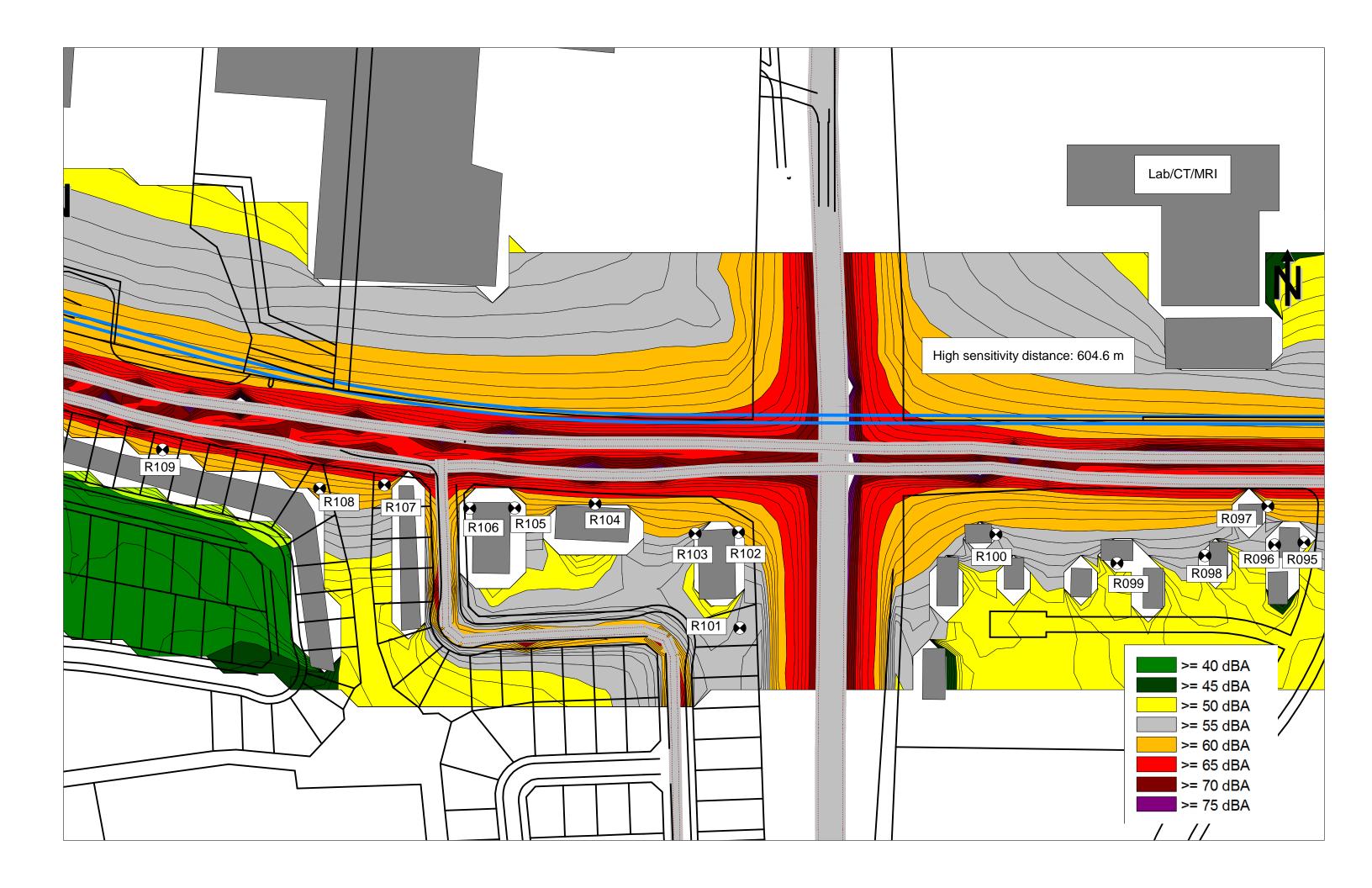






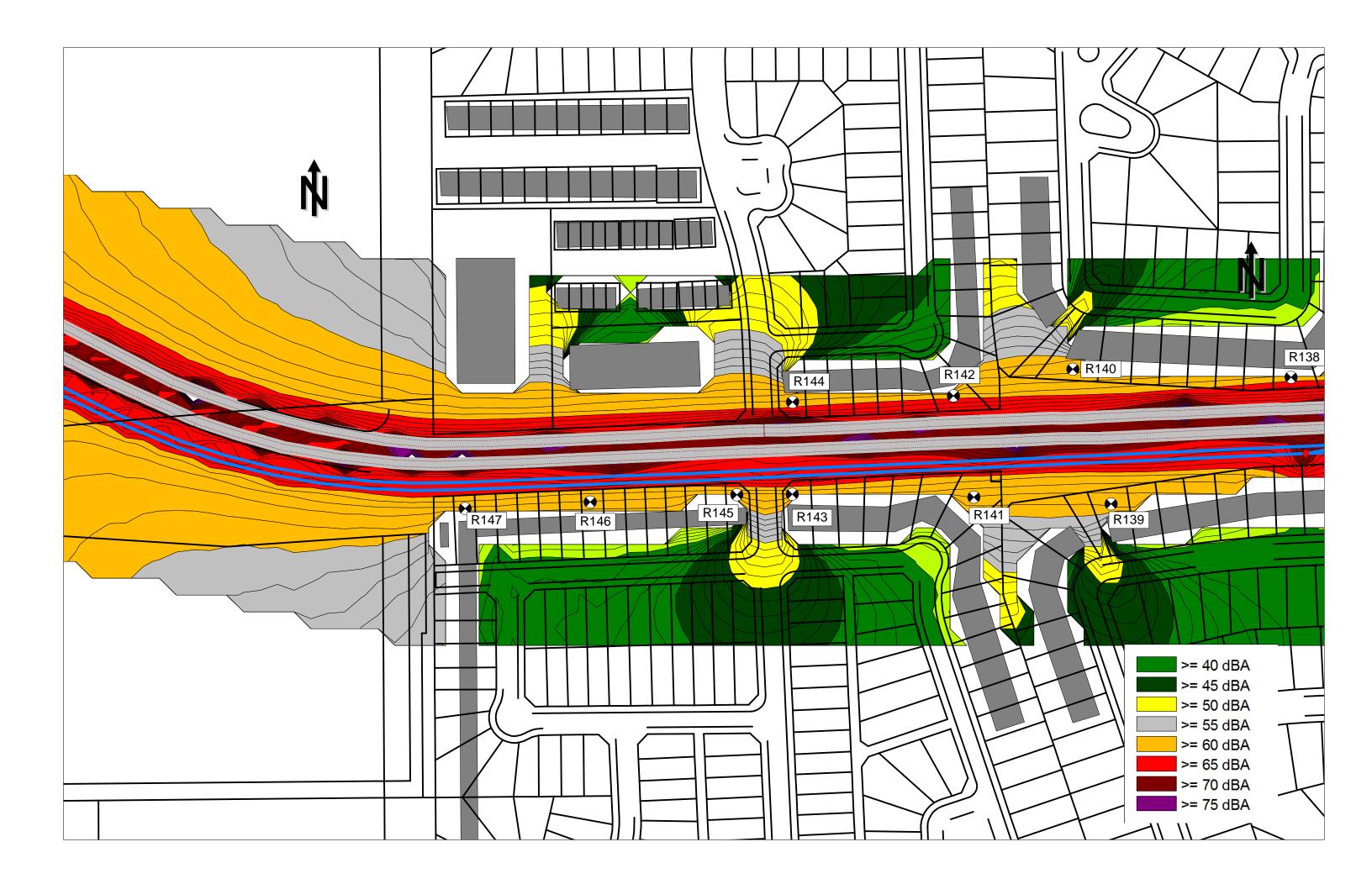


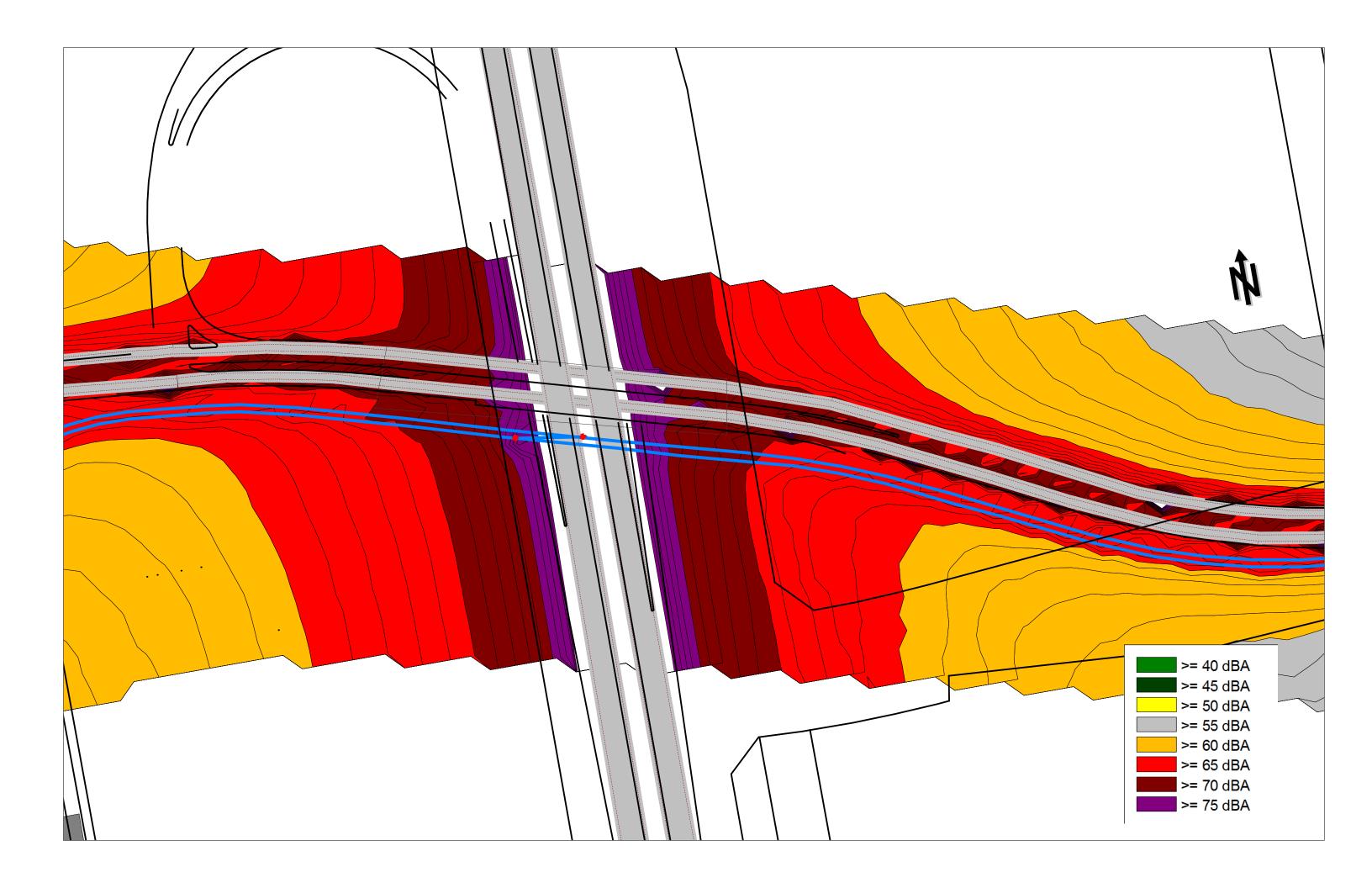


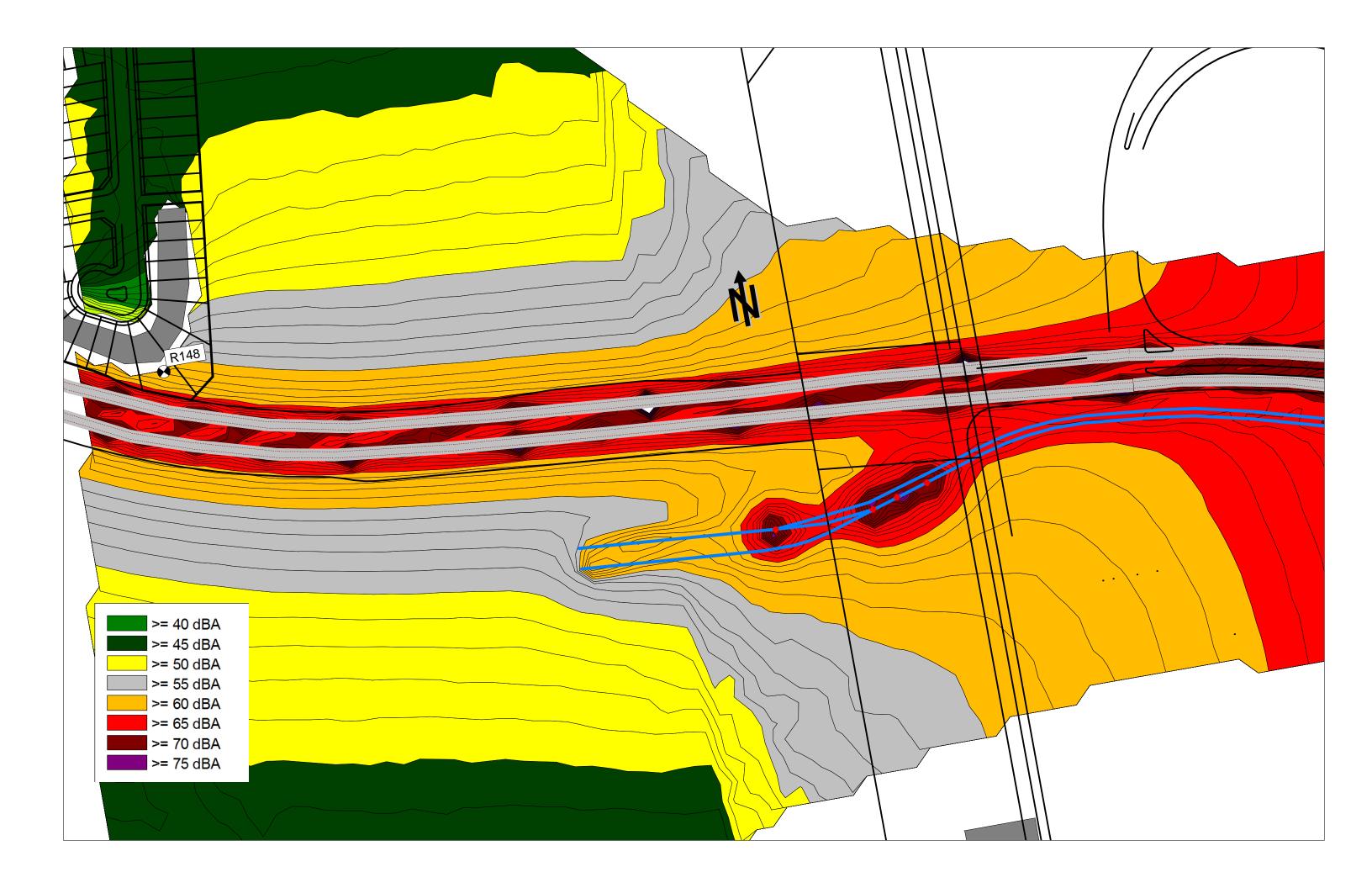




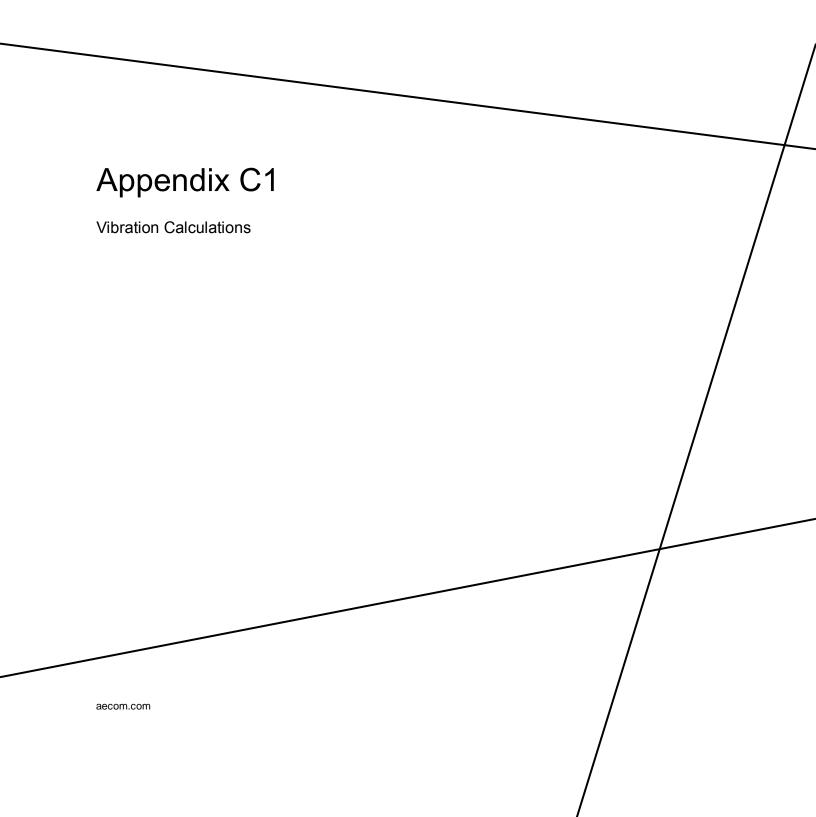












FTA Generalized Vibration Assessment - Operational Vibration Assessment

Efficient Propagation - 60 km/h

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	N/A	N/A
Office	84.0	0.40	29.7	9.0
Residential Day	78.0	0.20	69.1	21.0
Residential Night, Operating Rooms	72.0	0.10	138.0	42.0
High sensitivity	65.0	0.05	259.4	79.0

Efficient Propagation - 60 km/h - elevated

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	N/A	N/A
Office	84.0	0.40	N/A	N/A
Residential Day	78.0	0.20	13.3	4.0
Residential Night, Operating Rooms	72.0	0.10	42.8	13.0
High sensitivity	65.0	0.05	98.6	30.0

Efficient Propagation - 60 km/h - special track

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	52.7	16.0
Office	84.0	0.40	111.7	34.0
Residential Day	78.0	0.20	197.0	60.0
Residential Night, Operating Rooms	72.0	0.10	318.4	97.0
High sensitivity	65.0	0.05	364.0	111.0

Efficient Propagation - 50 km/h

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	N/A	N/A
Office	84.0	0.40	23.1	7.0
Residential Day	78.0	0.20	55.9	17.0
Residential Night, Operating Rooms	72.0	0.10	118.3	36.0
High sensitivity	65.0	0.05	223.3	68.0

Efficient Propagation - 50 km/h - elevated

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	N/A	N/A
Office	84.0	0.40	N/A	N/A
Residential Day	78.0	0.20	N/A	N/A
Residential Night, Operating Rooms	72.0	0.10	33.0	10.0
High sensitivity	65.0	0.05	82.2	25.0

Efficient Propagation - 50 km/h - special trackwork

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	42.8	13.0
Office	84.0	0.40	92.0	28.0
Residential Day	78.0	0.20	174.1	53.0
Residential Night, Operating Rooms	72.0	0.10	292.2	89.0
High sensitivity	65.0	0.05	358.0	109.0

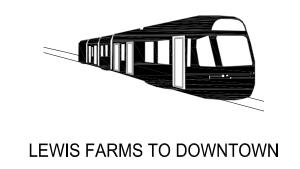
Efficient Propagation - 25 km/h

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	N/A	N/A
Office	84.0	0.40	N/A	N/A
Residential Day	78.0	0.20	23.1	7.0
Residential Night, Operating Rooms	72.0	0.10	55.9	17.0
High sensitivity	65.0	0.05	131.4	40.0

Efficient Propagation - 25 km/h - special trackwork

Space	Limit	Limit	Distance	Distance
	VdB	mm/sec	(ft)	(m)
Industrial / Workshop	90.0	0.80	16.6	5.0
Office	84.0	0.40	42.8	13.0
Residential Day	78.0	0.20	92.0	28.0
Residential Night, Operating Rooms	72.0	0.10	174.1	53.0
High sensitivity	65.0	0.05	308.6	94.0





VALLEY LINE WEST LRT

90% SION SUBMISSION

PRELIMINARY ENGINEERING DRAWINGS FOR:

Note: Transition zones required between all changes in track mitigation and changes from normal track to mitigated track.

LRT - TRACKWORK

DECEMBER 13, 2017

Note: For sections requiring >15 VdB of mitigation (crossovers in close promixity to residences), consider moving crossovers to less sensitive locations (commercial areas, bridges, LRT sections further from residences).

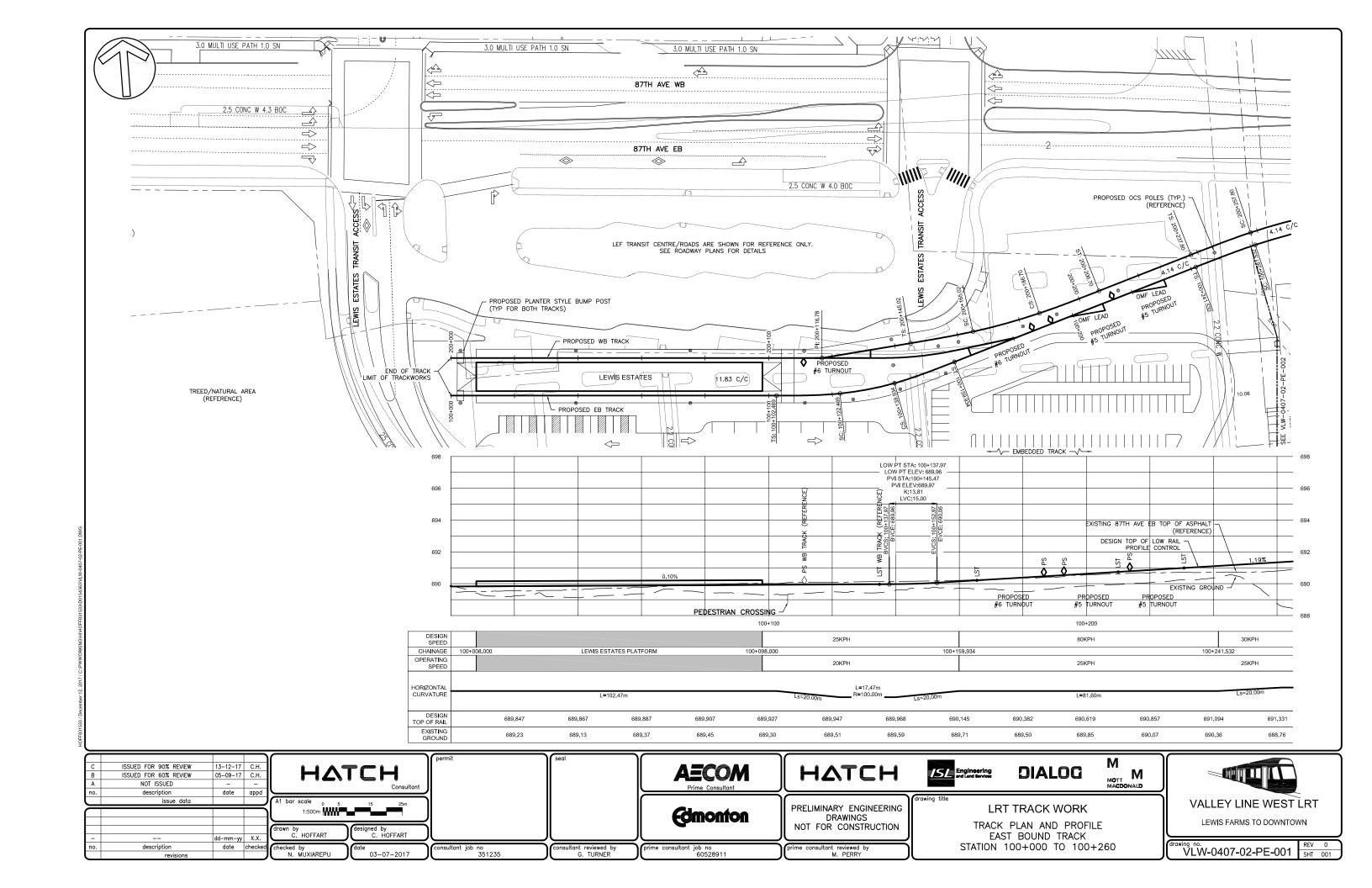


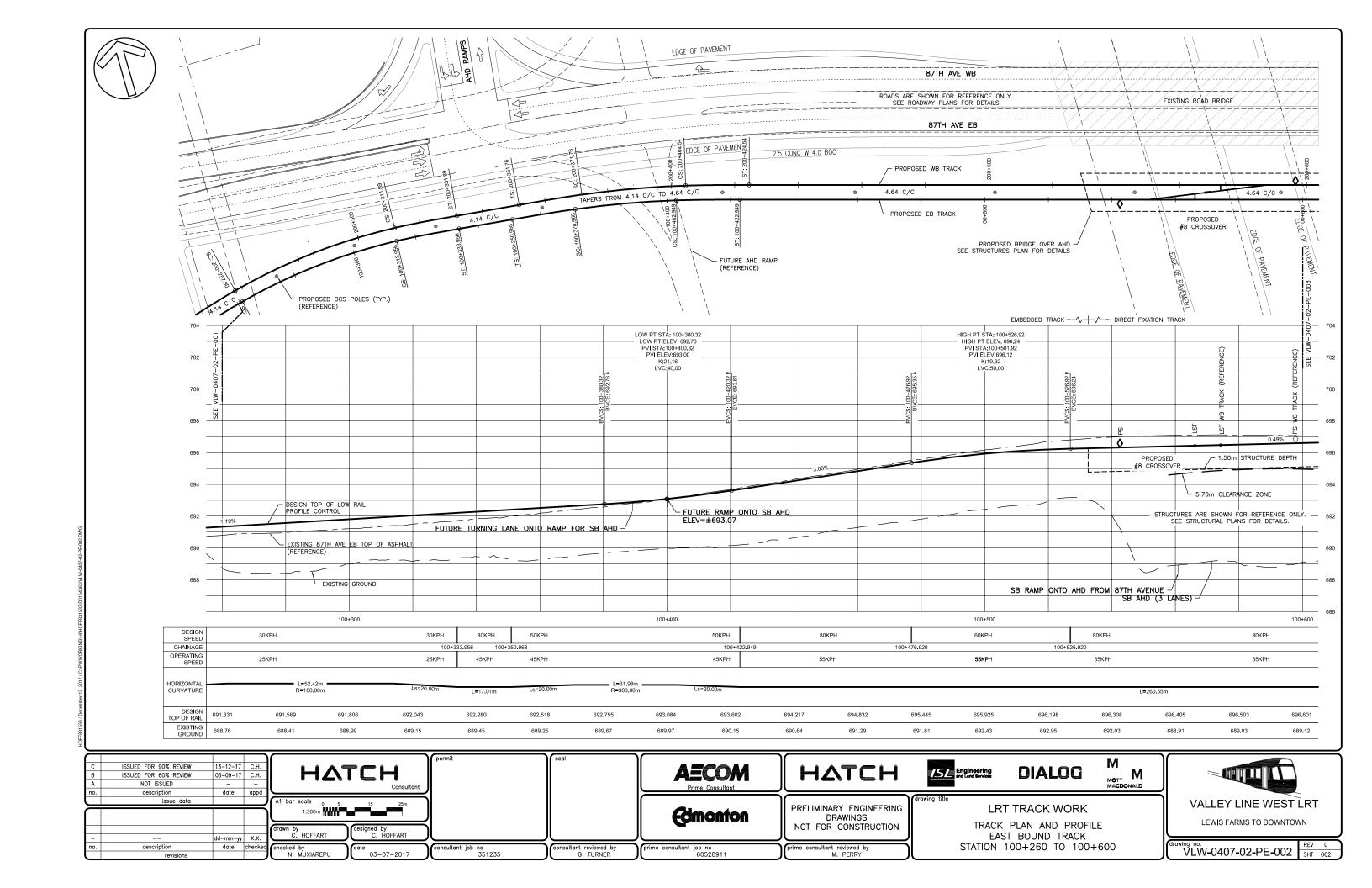


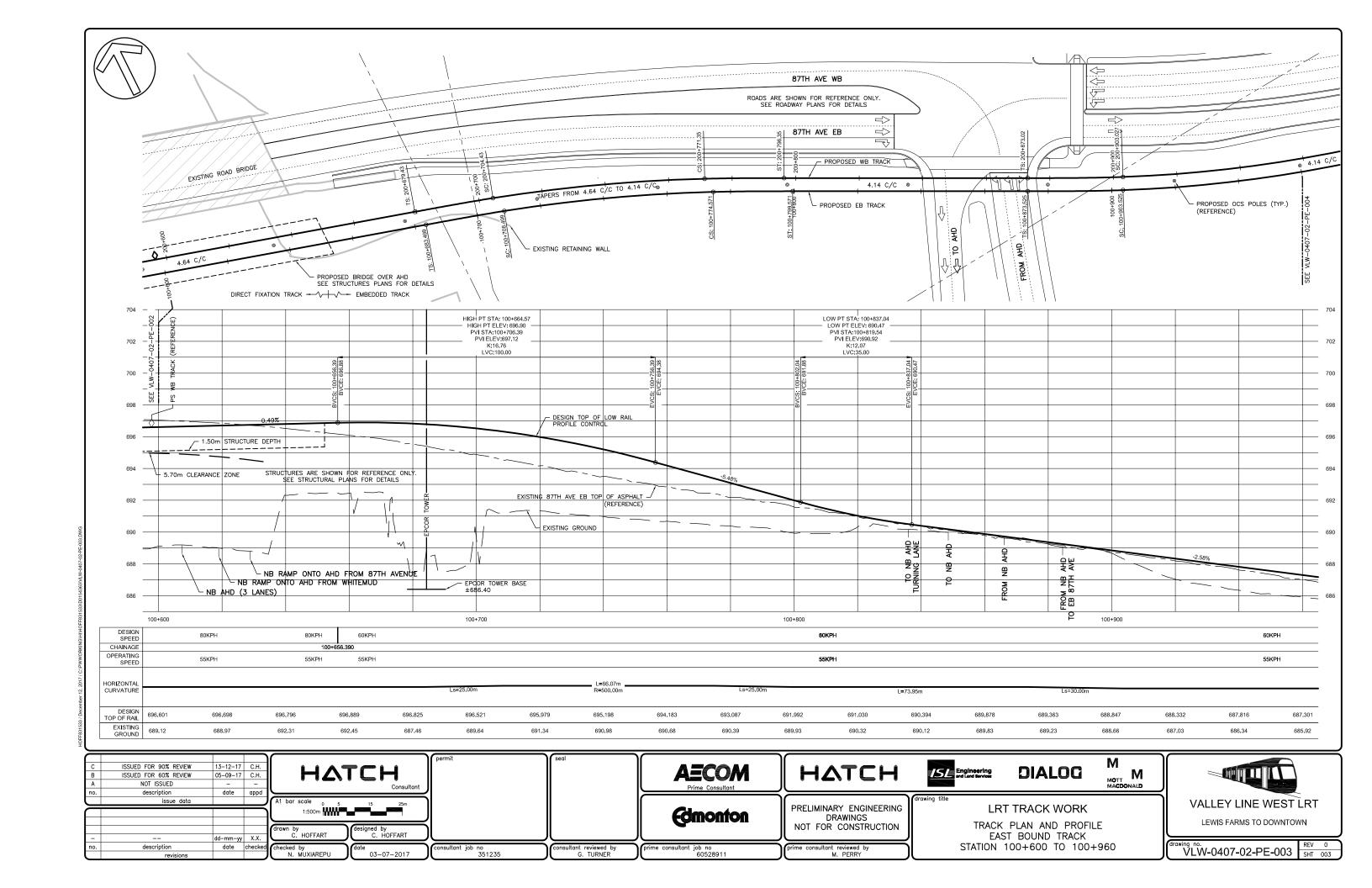


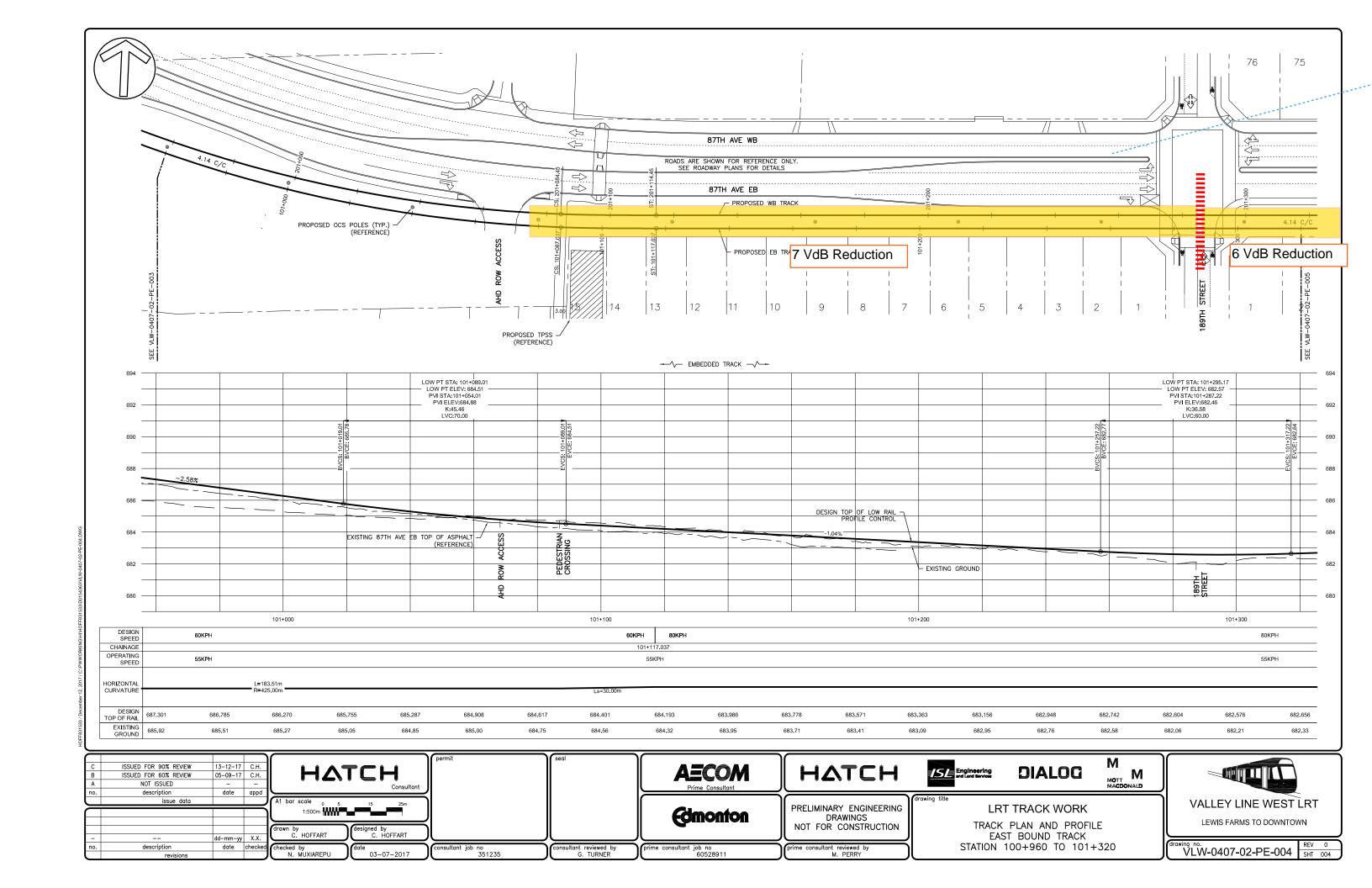


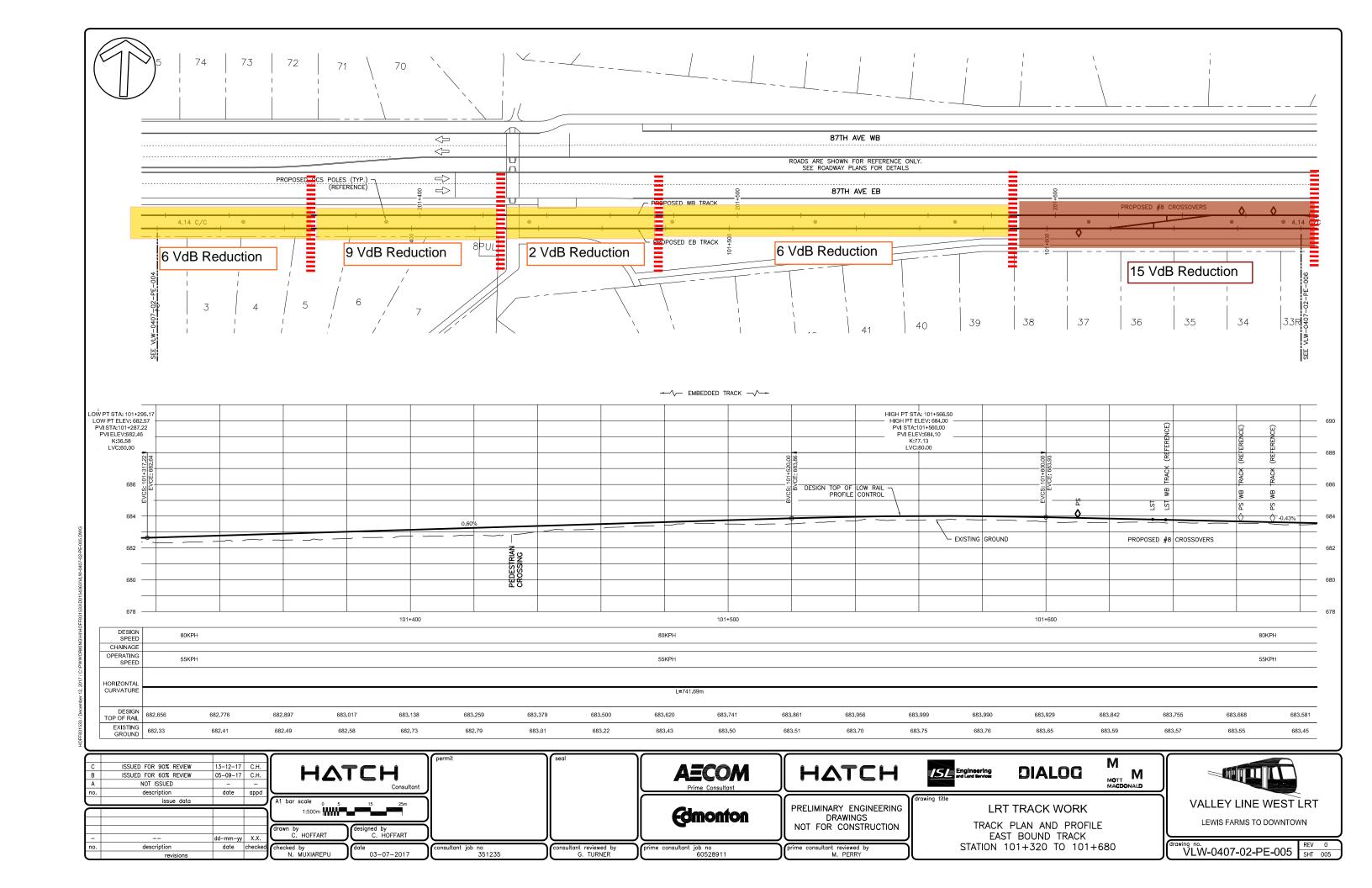


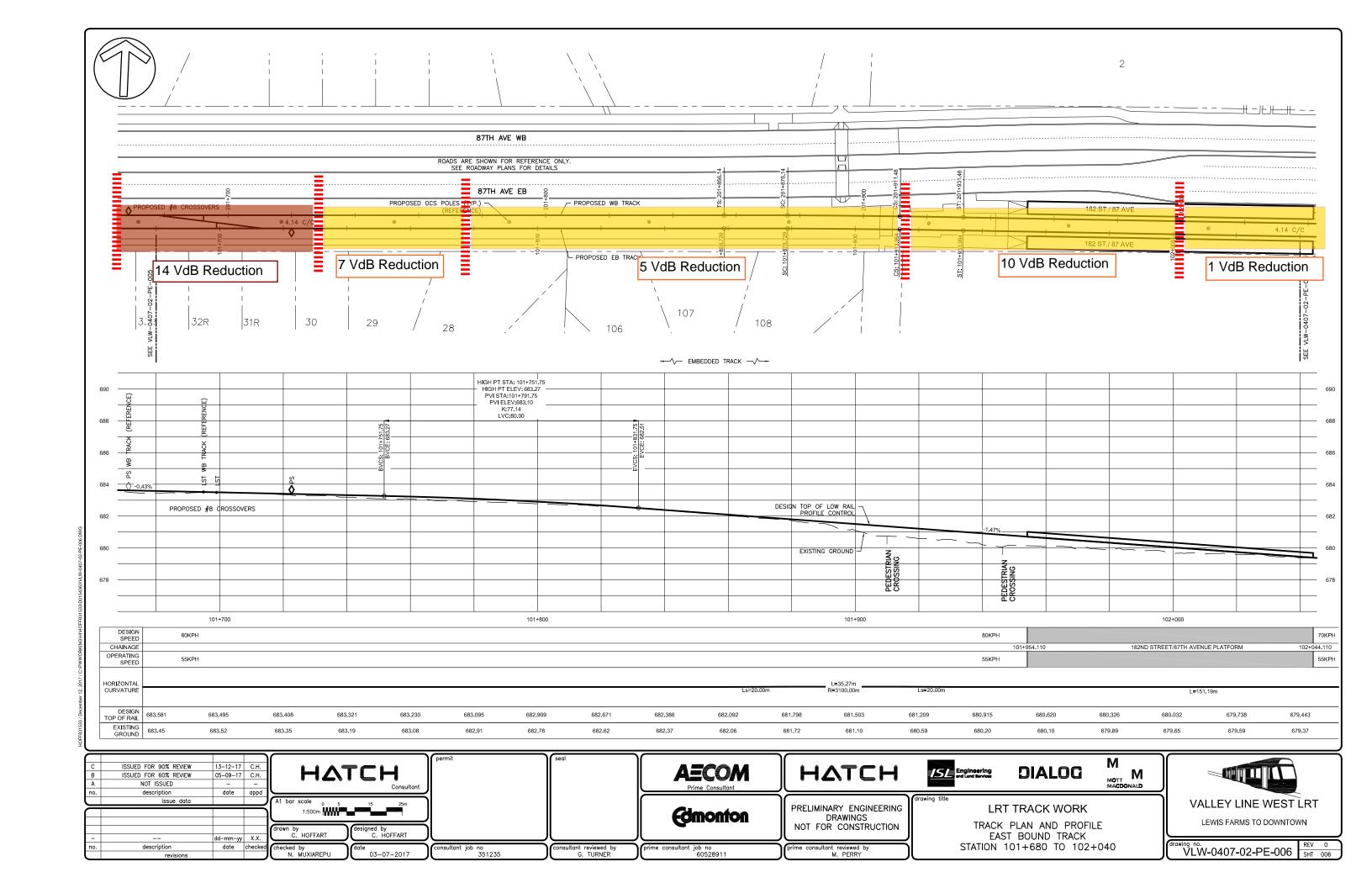


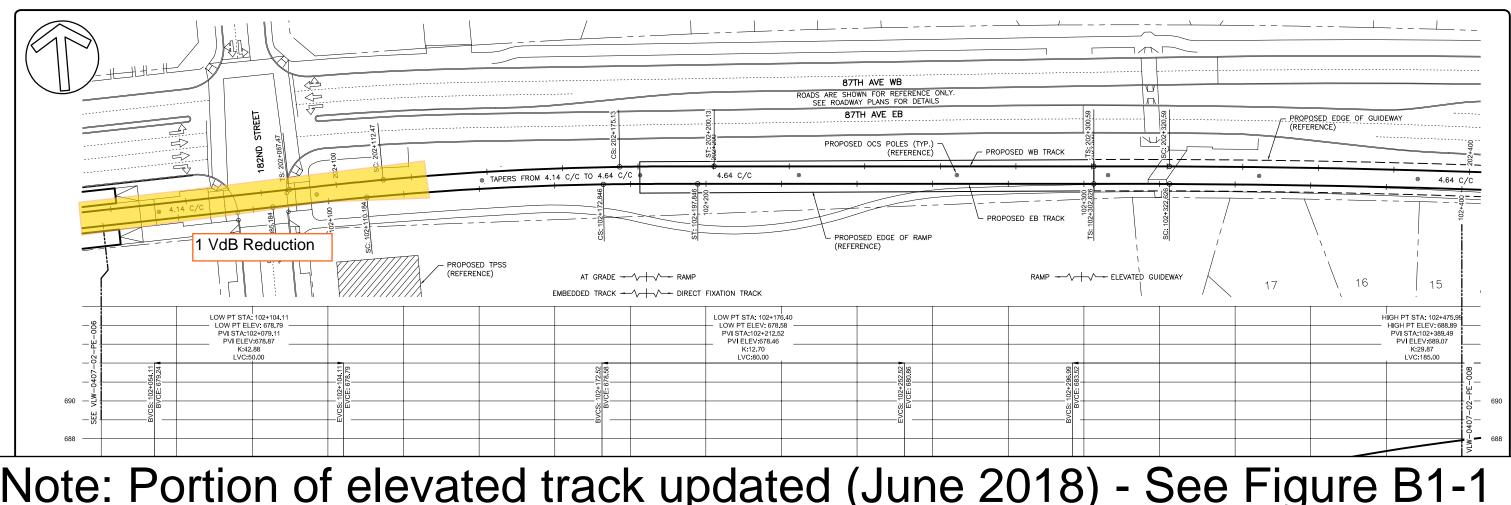




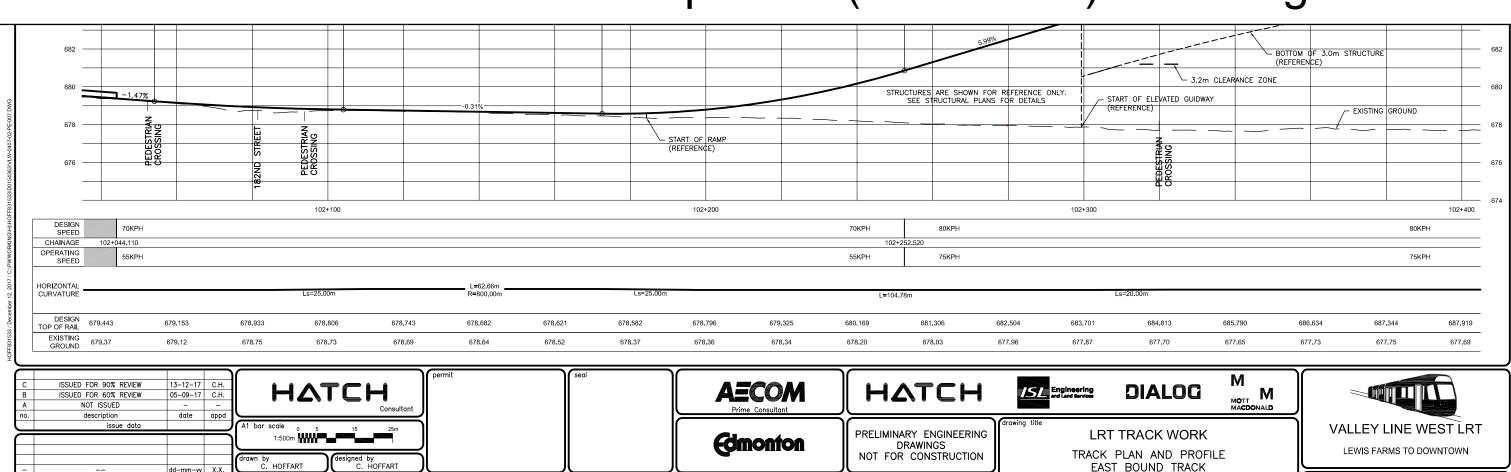








Note: Portion of elevated track updated (June 2018) - See Figure B1-1



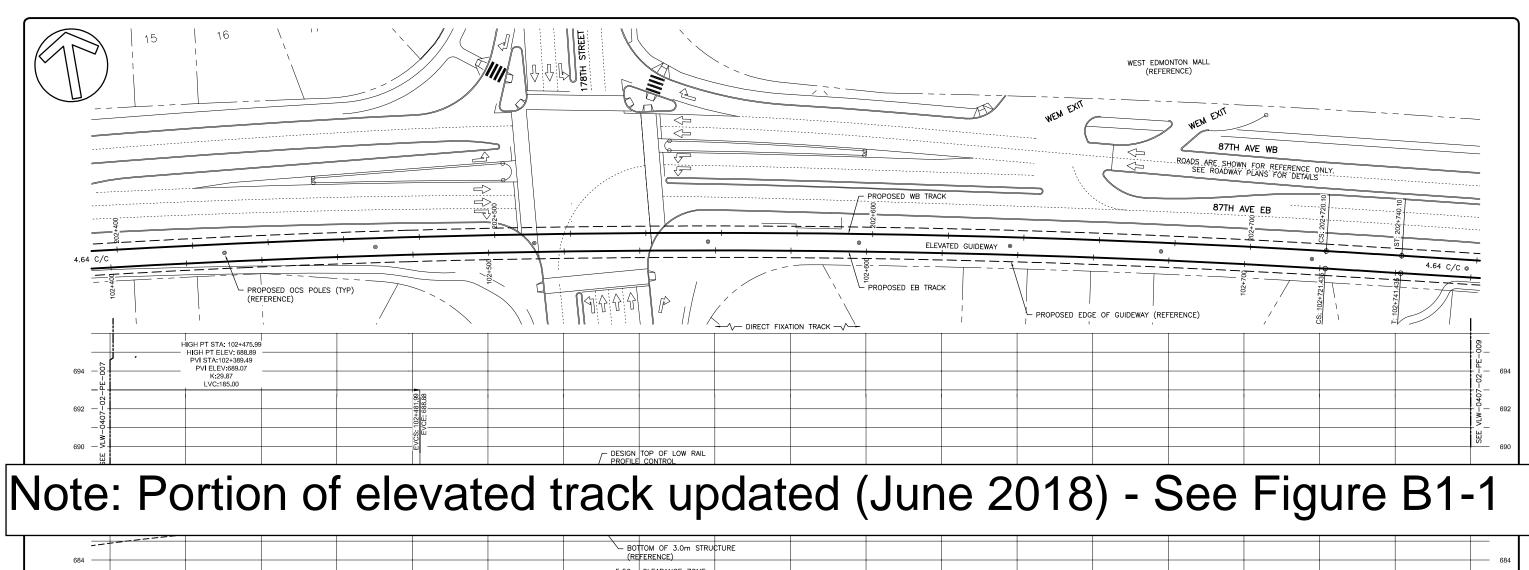
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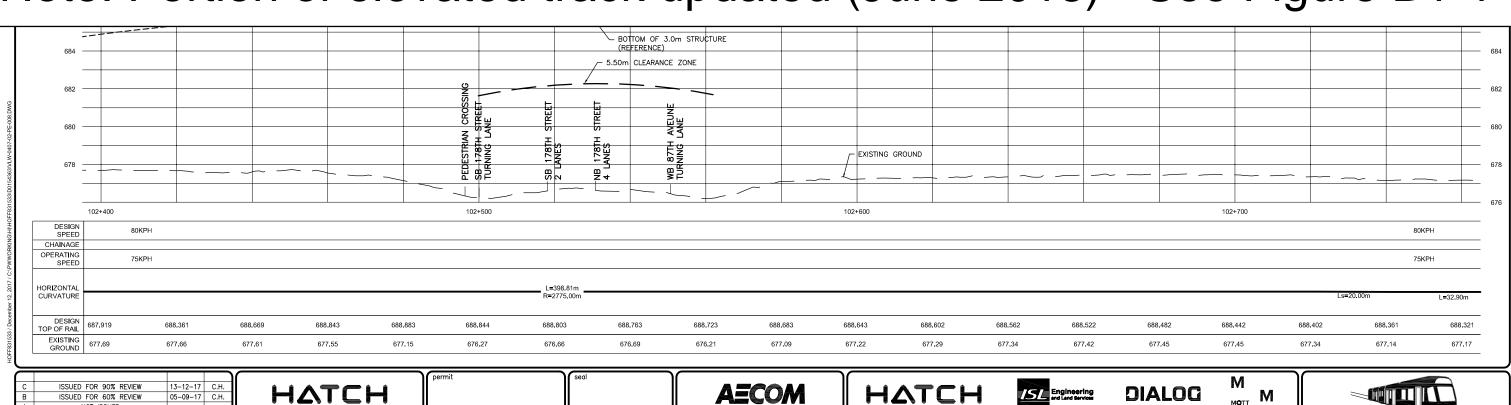
03-07-2017

description

STATION 102+040 TO 102+400

VLW-0407-02-PE-007 SHT 007





Edmonton

PRELIMINARY ENGINEERING

DRAWINGS

NOT FOR CONSTRUCTION

LRT TRACK WORK

TRACK PLAN AND PROFILE

EAST BOUND TRACK STATION 102+400 TO 102+760 VALLEY LINE WEST LRT

LEWIS FARMS TO DOWNTOWN

VLW-0407-02-PE-008 SHT 008

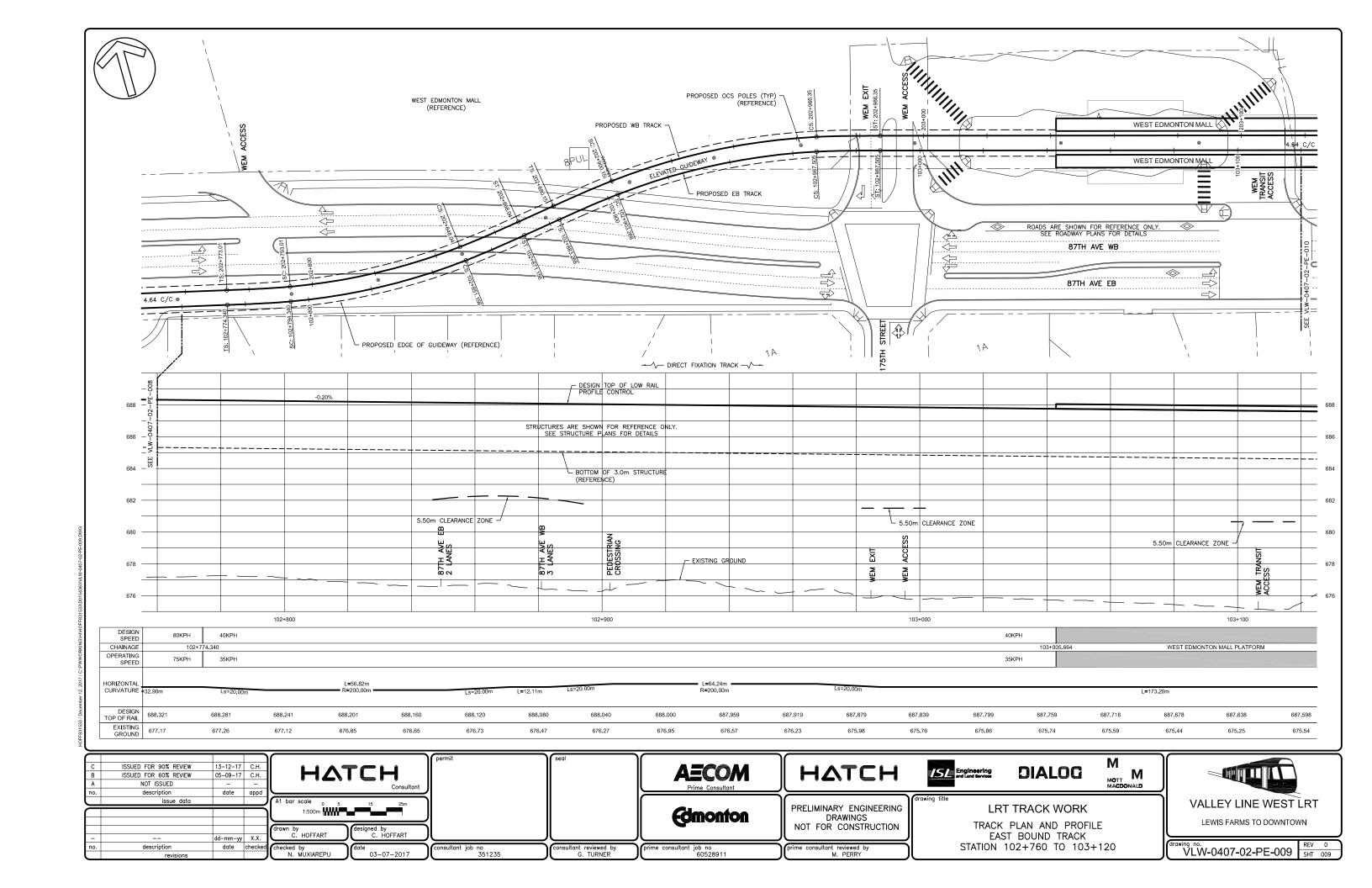
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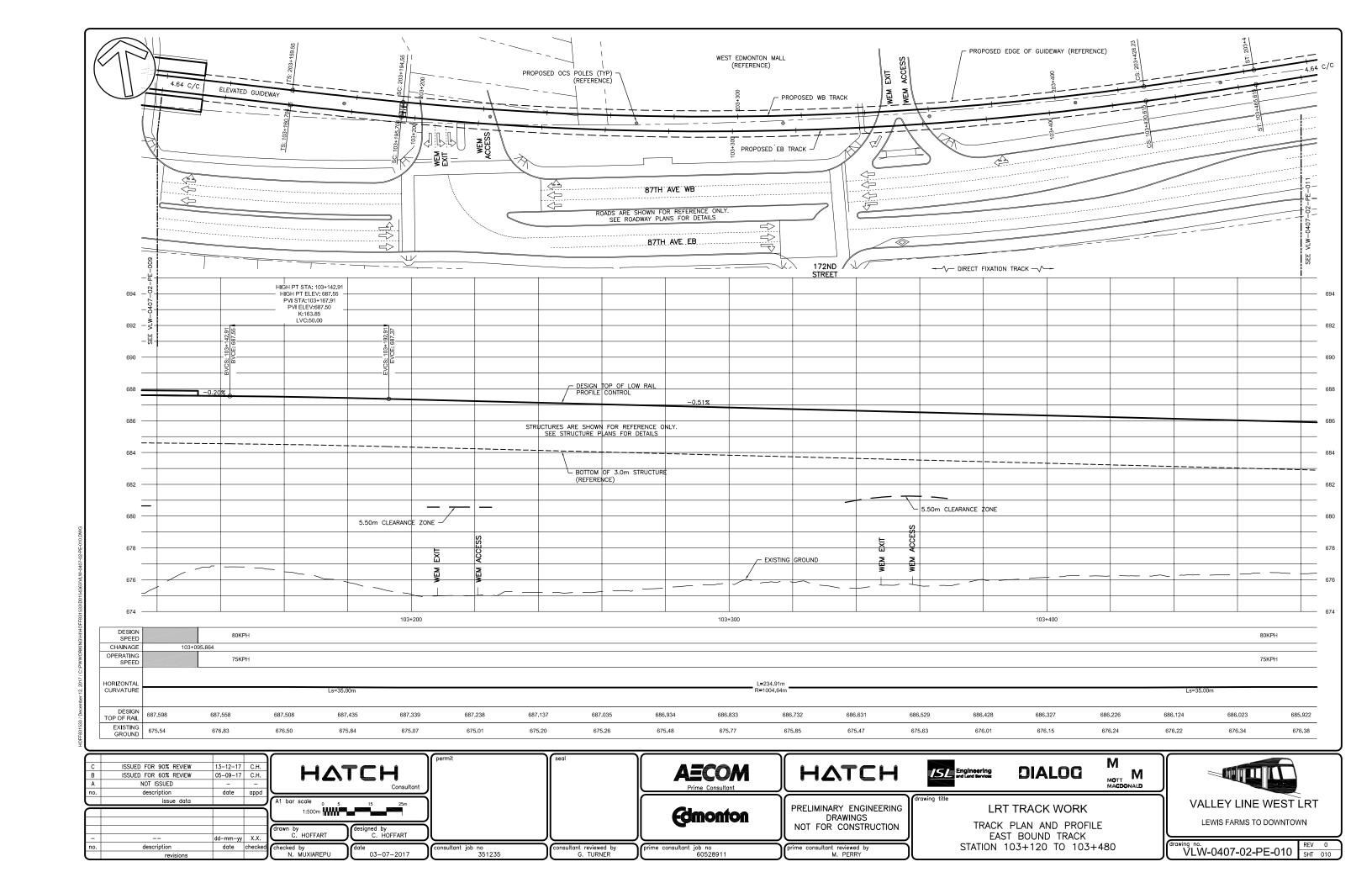
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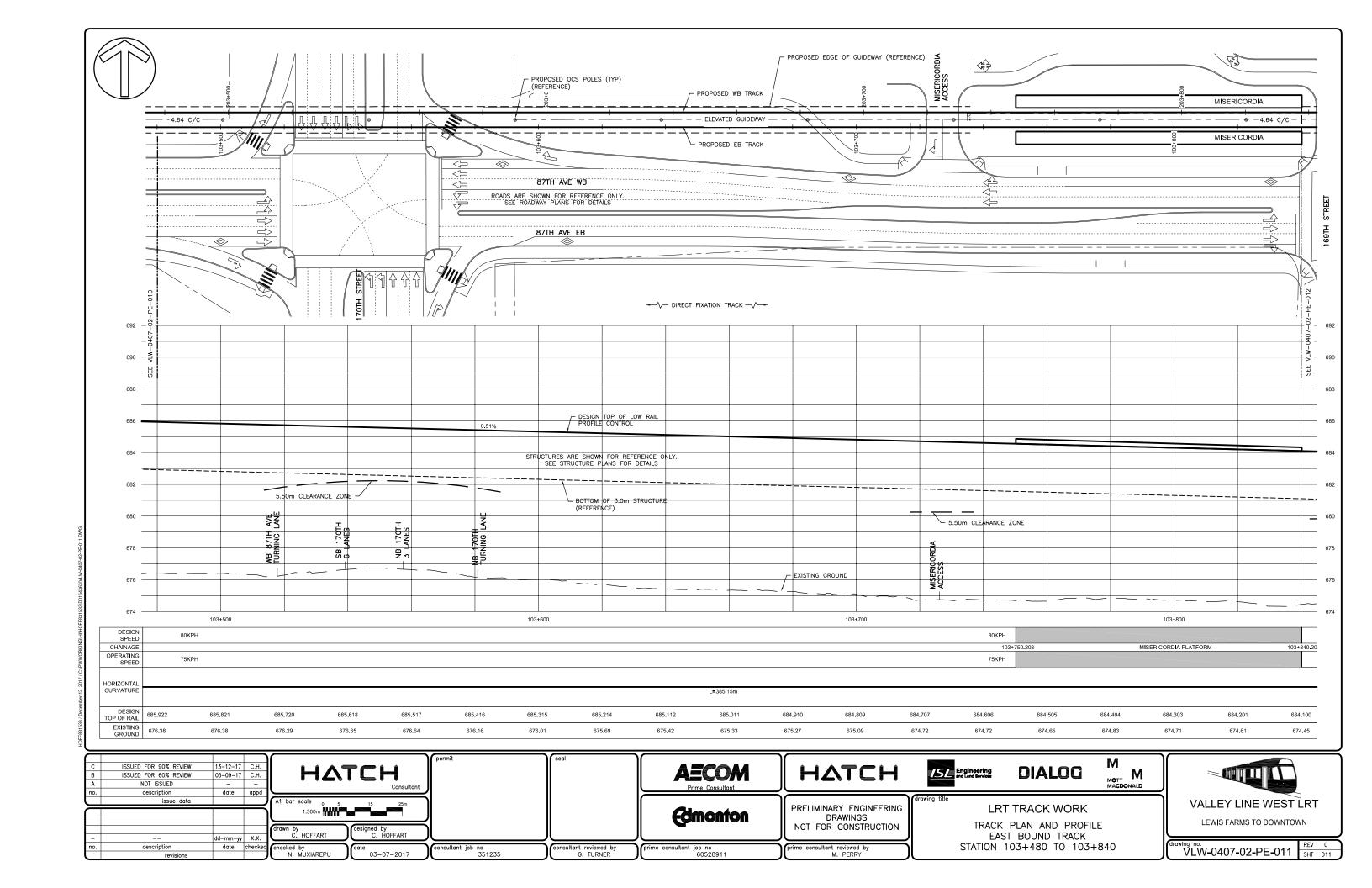
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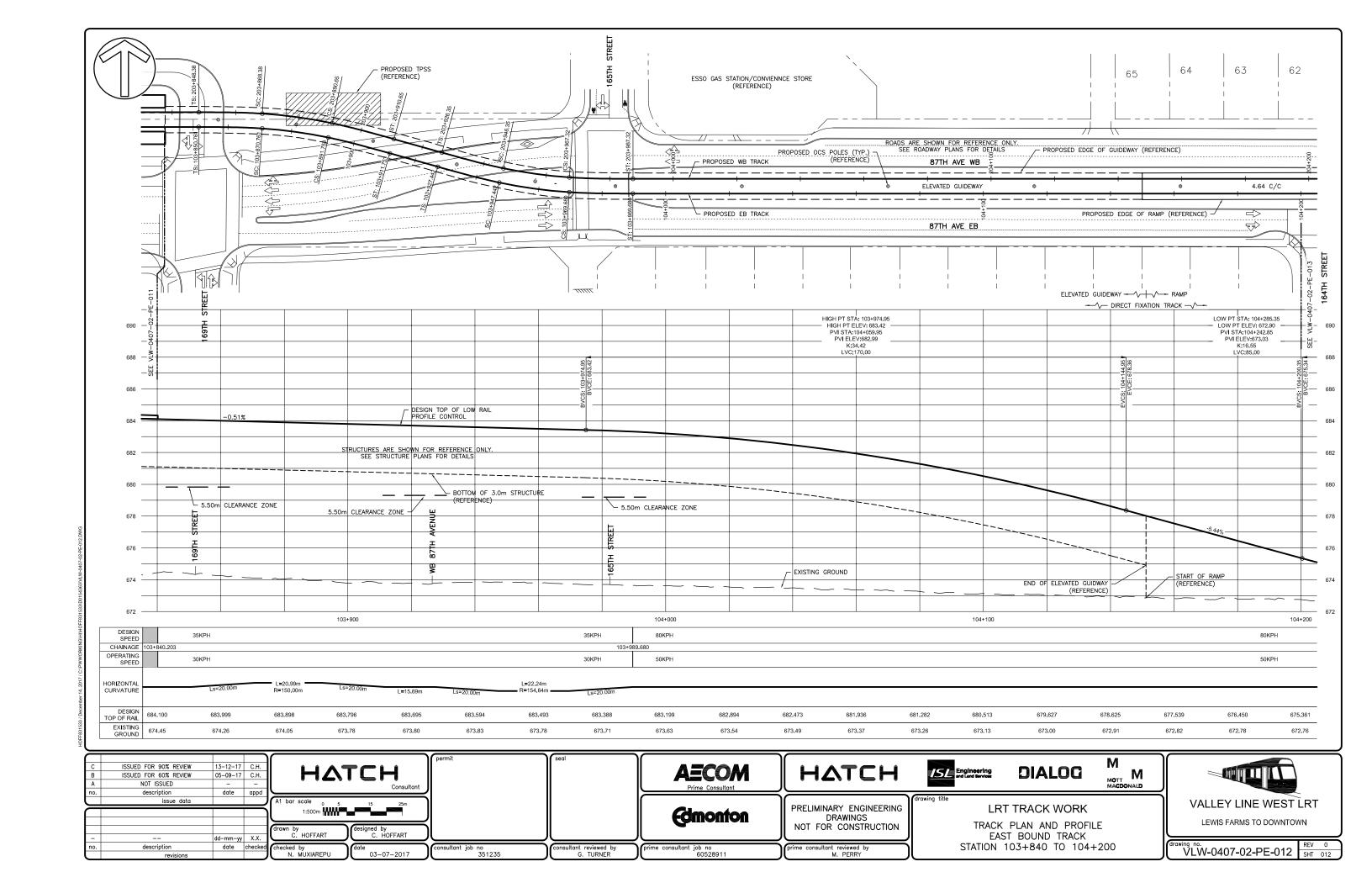
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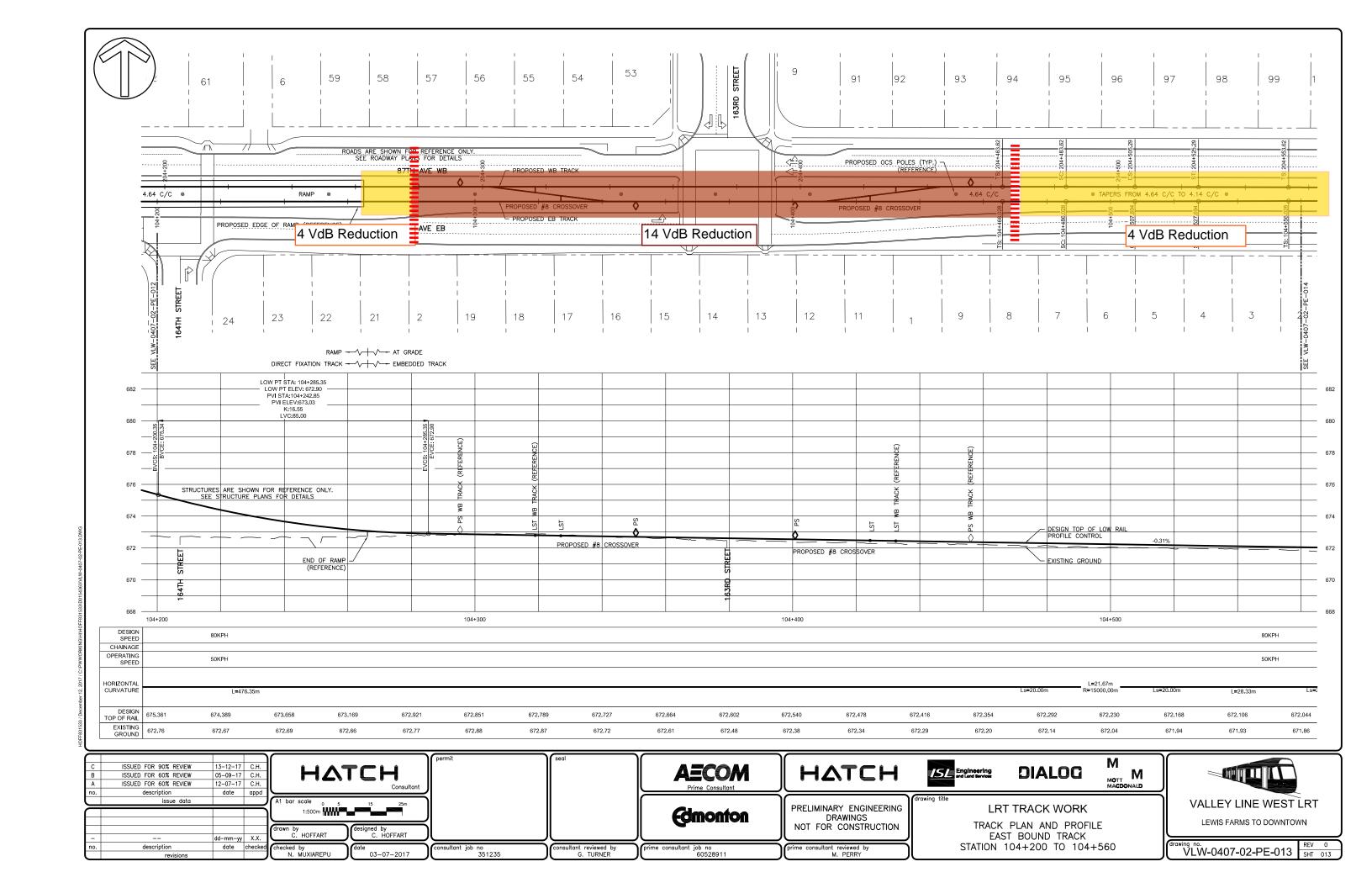
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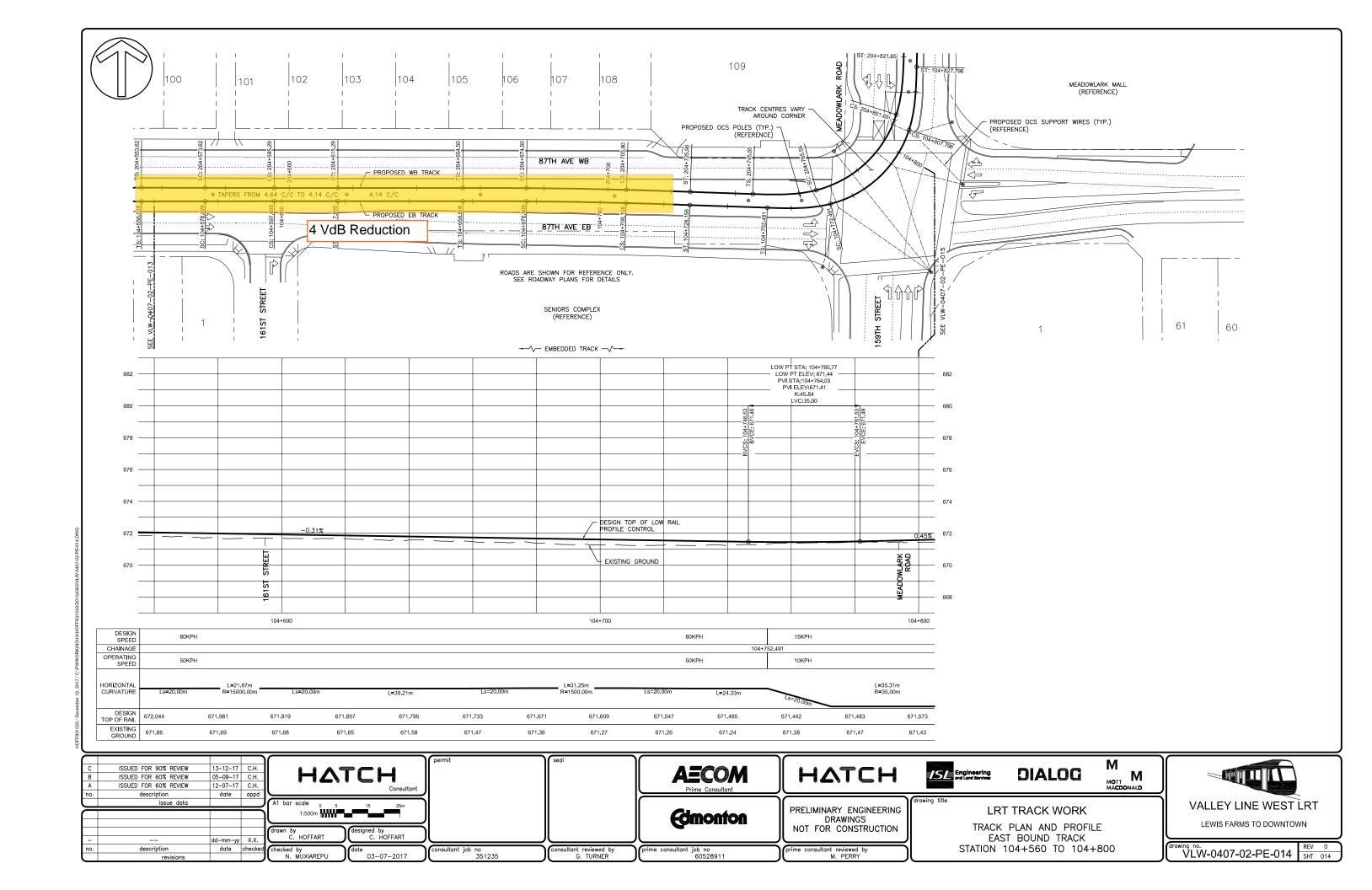


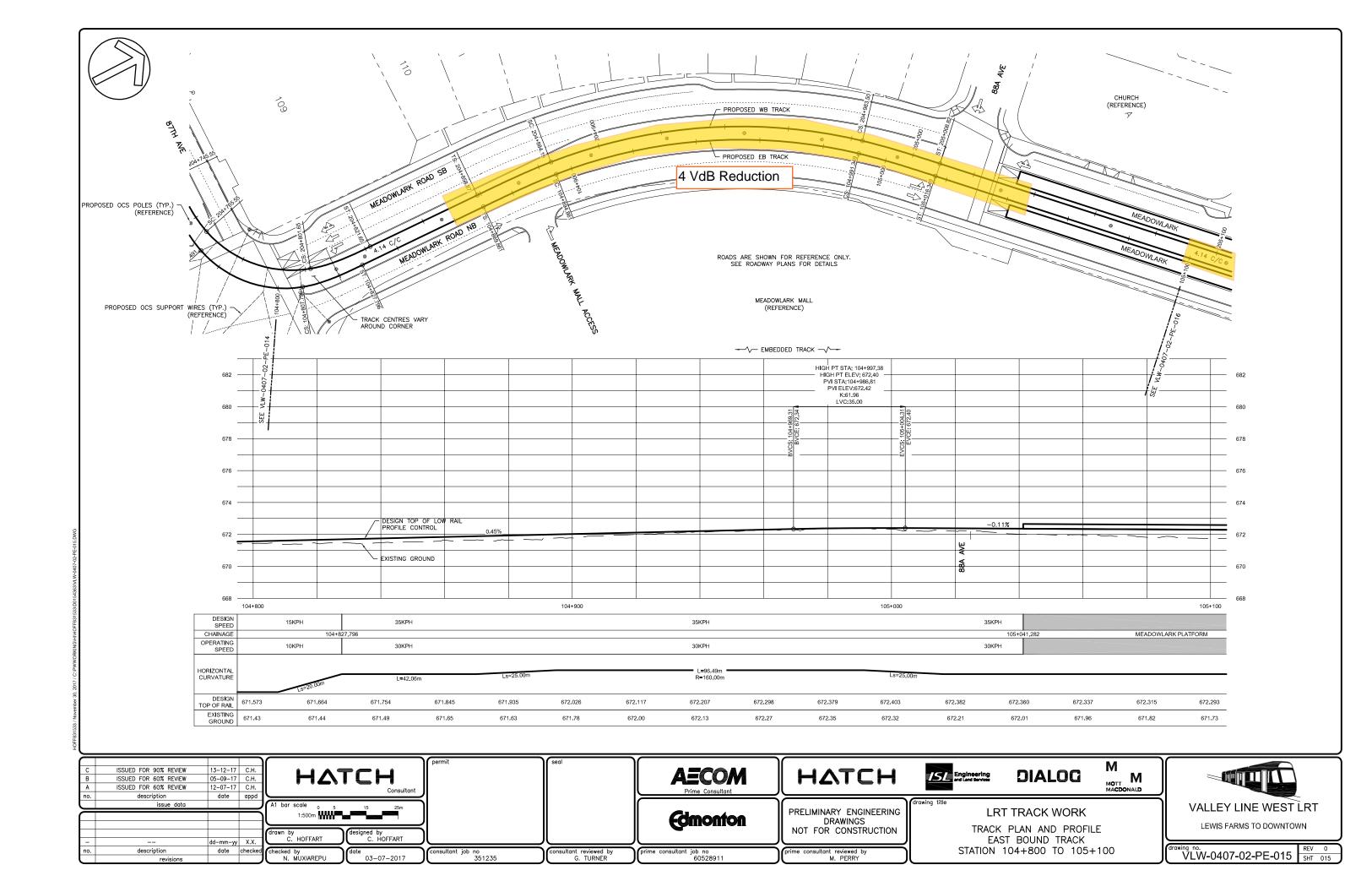


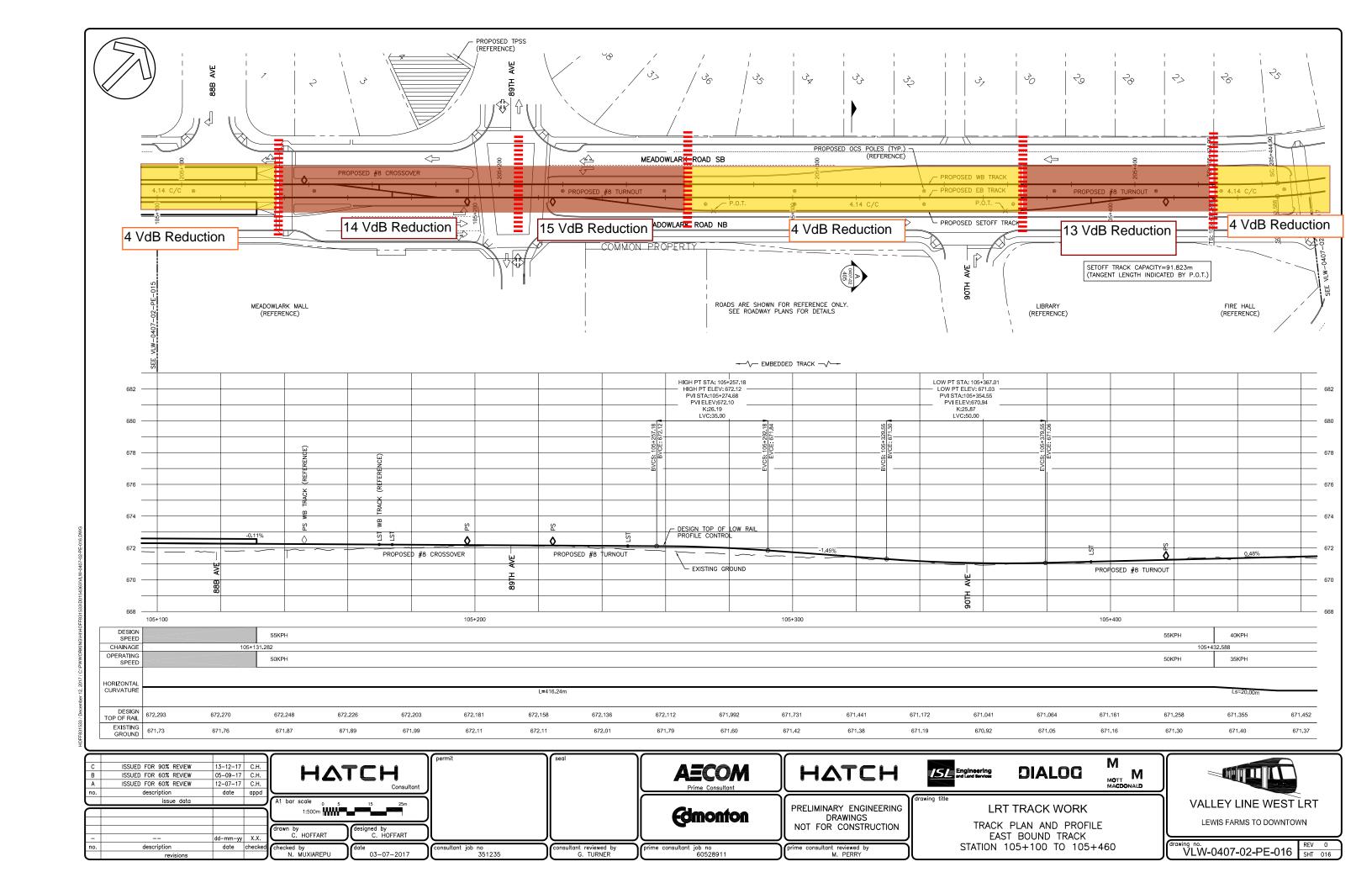


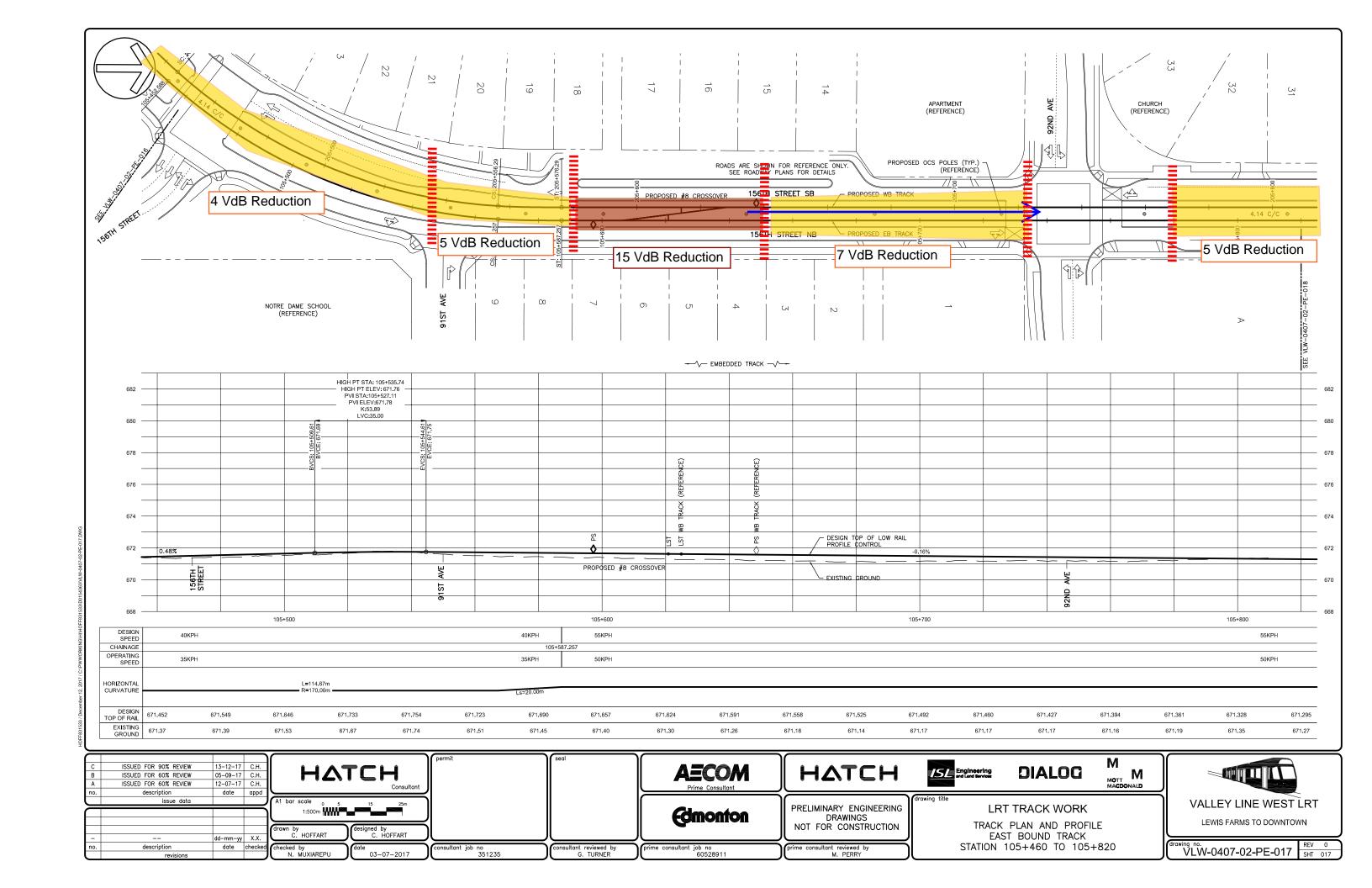


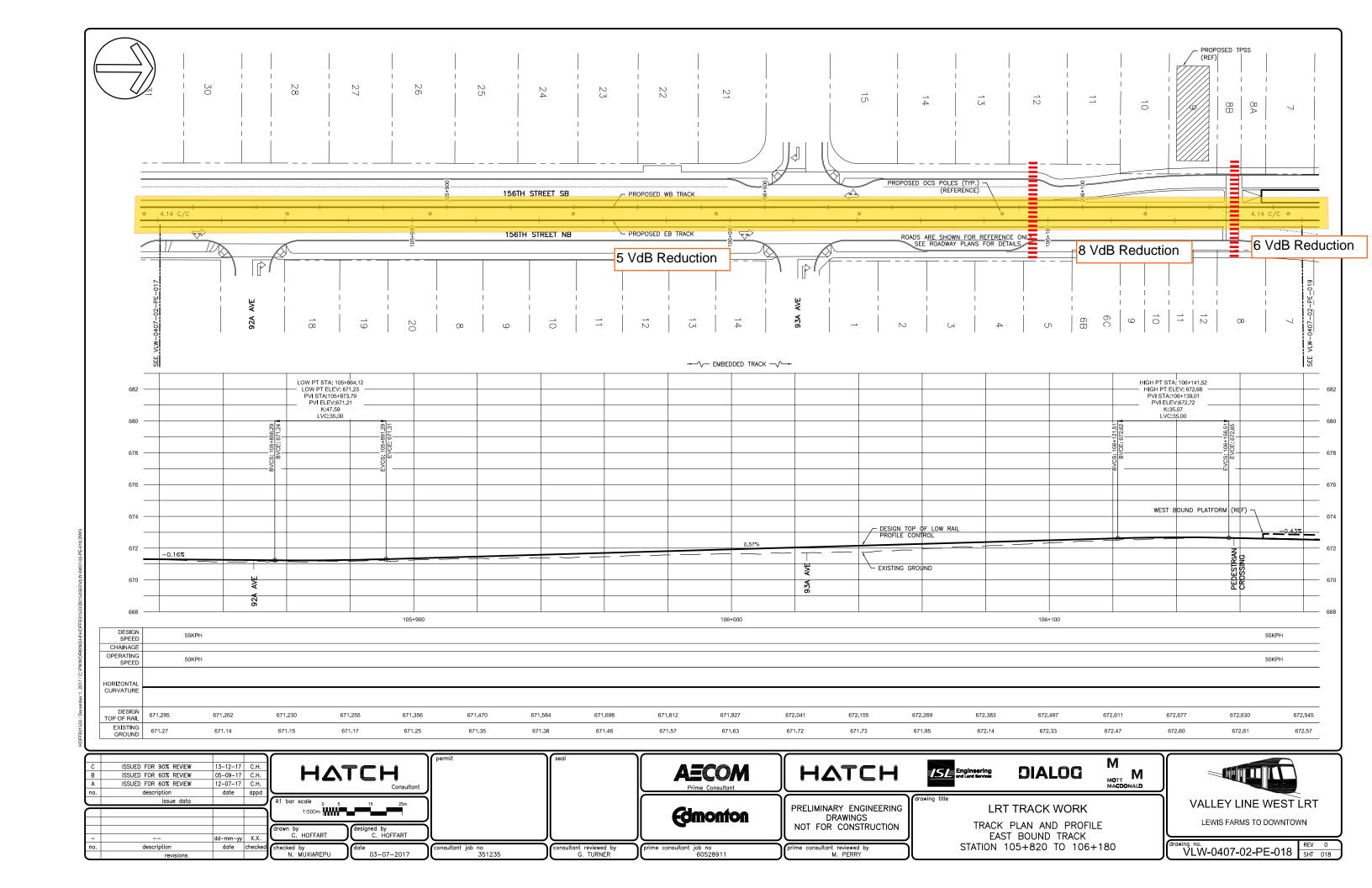


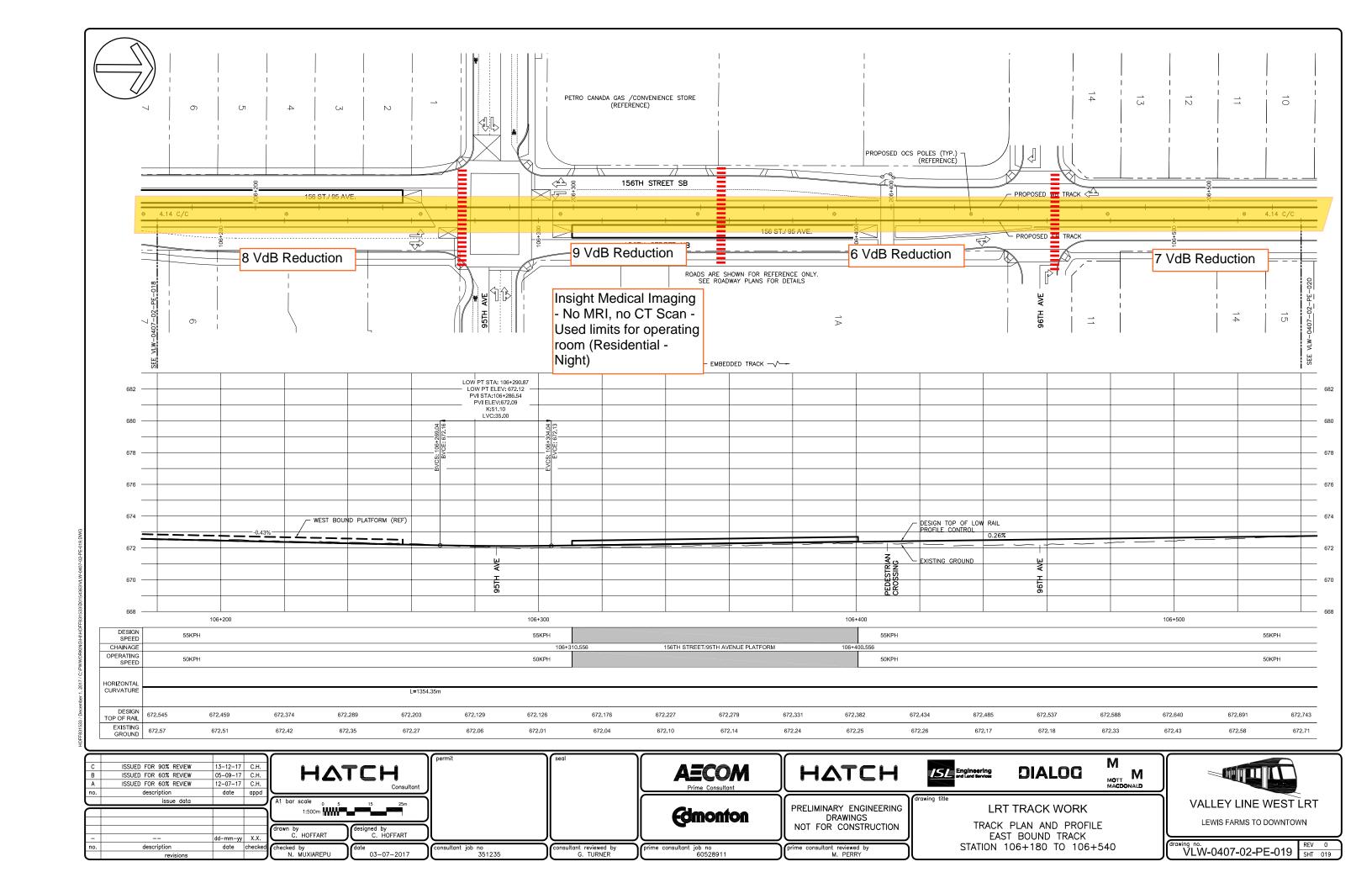


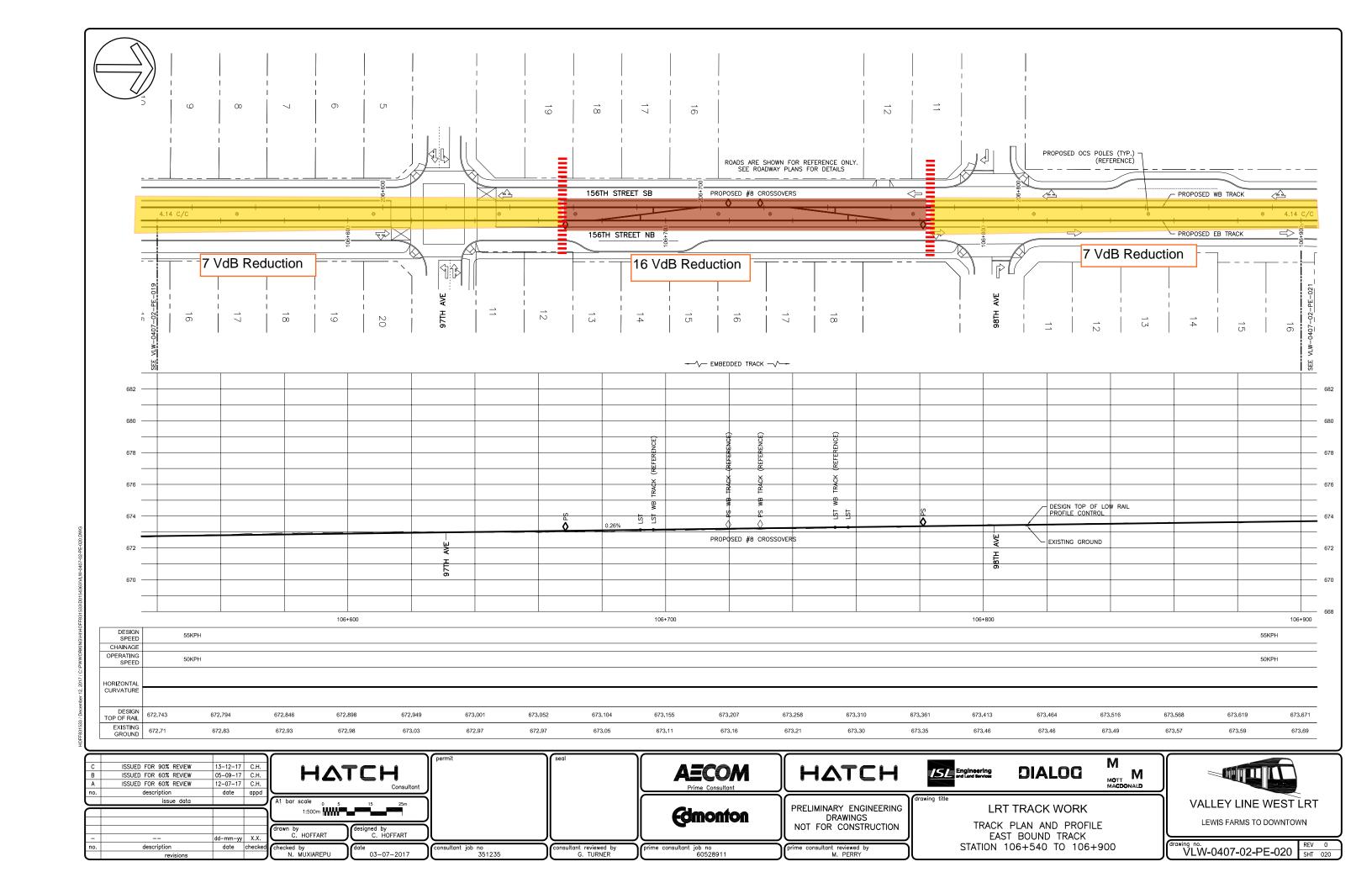


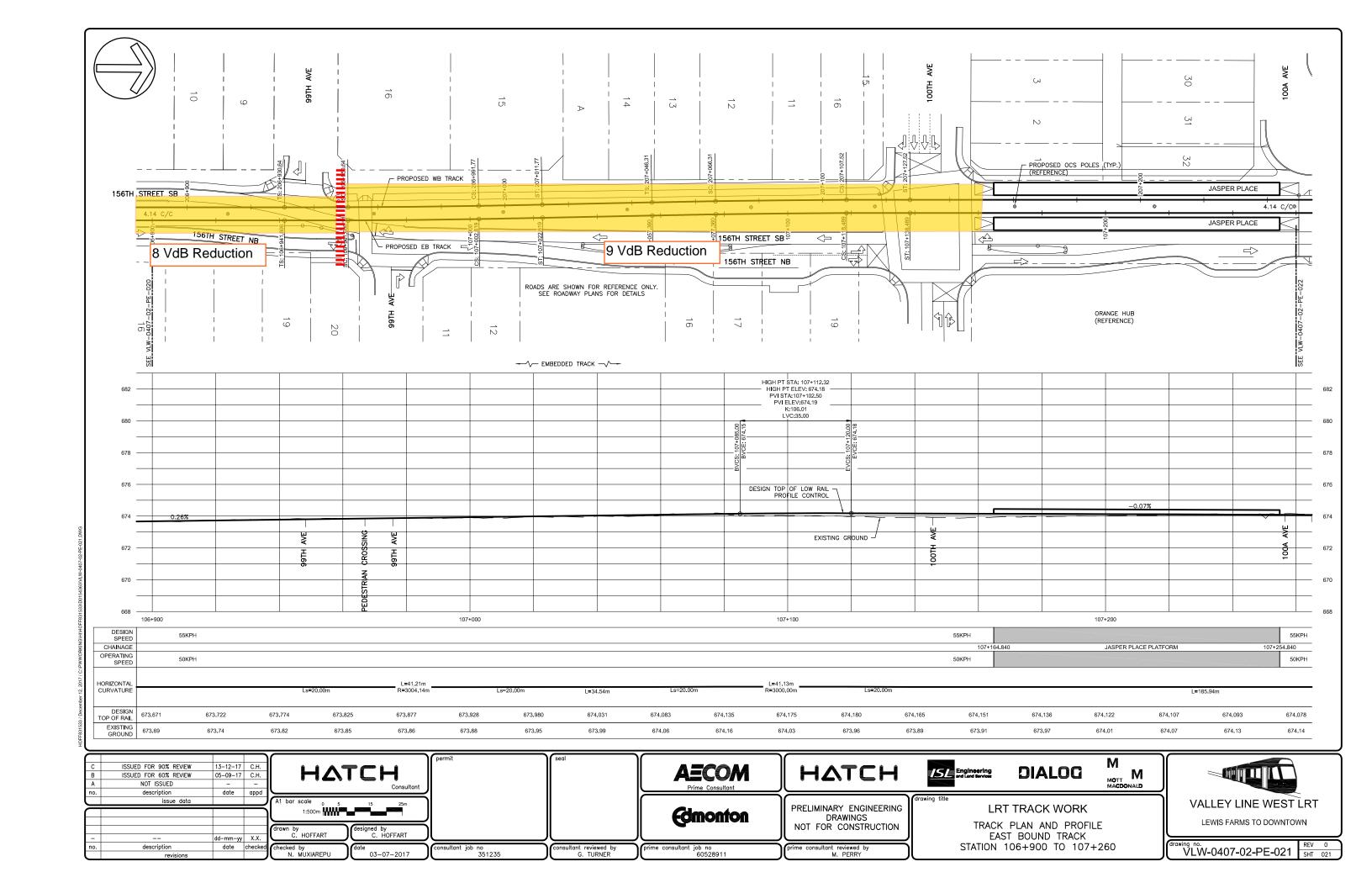


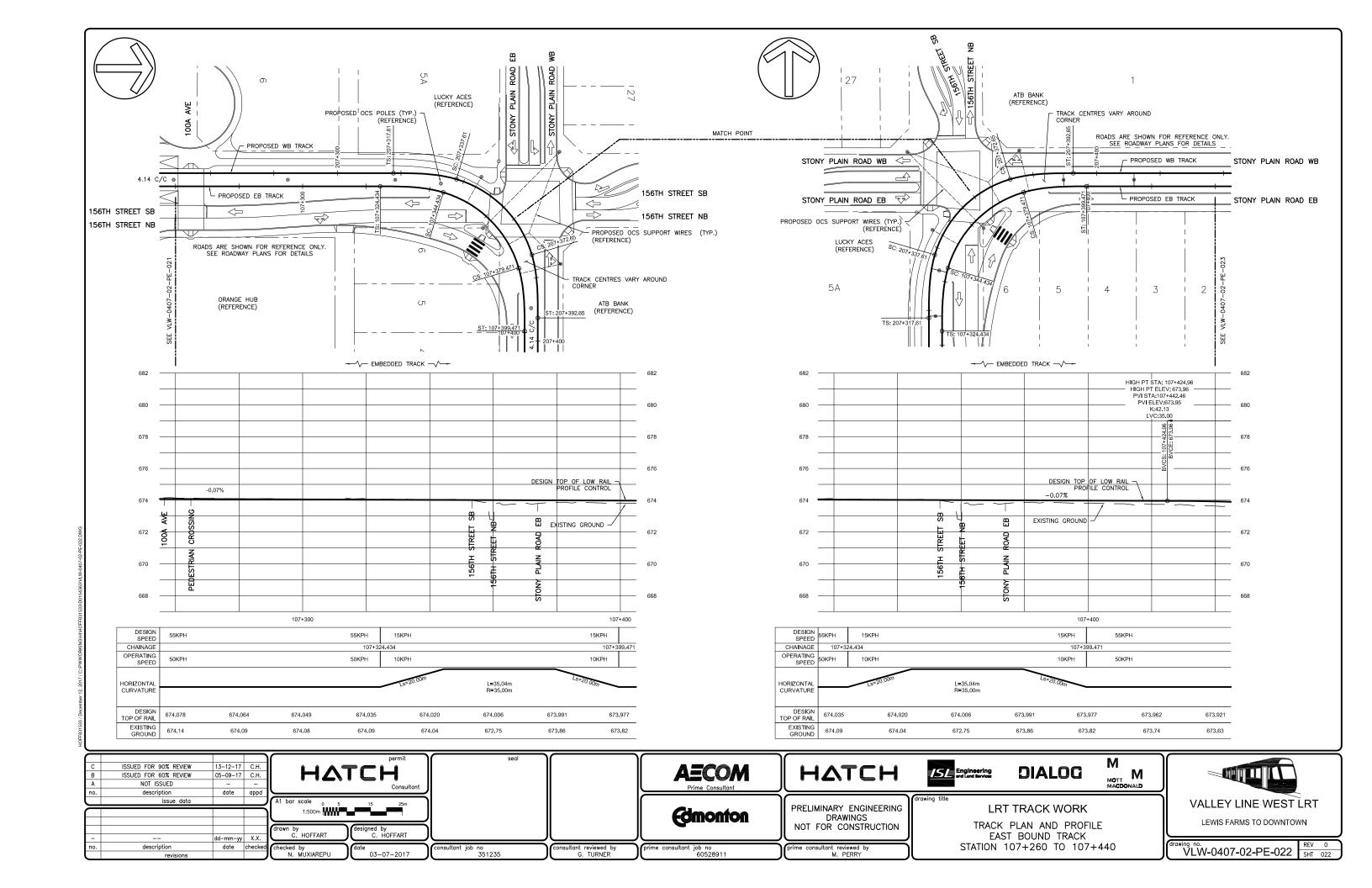


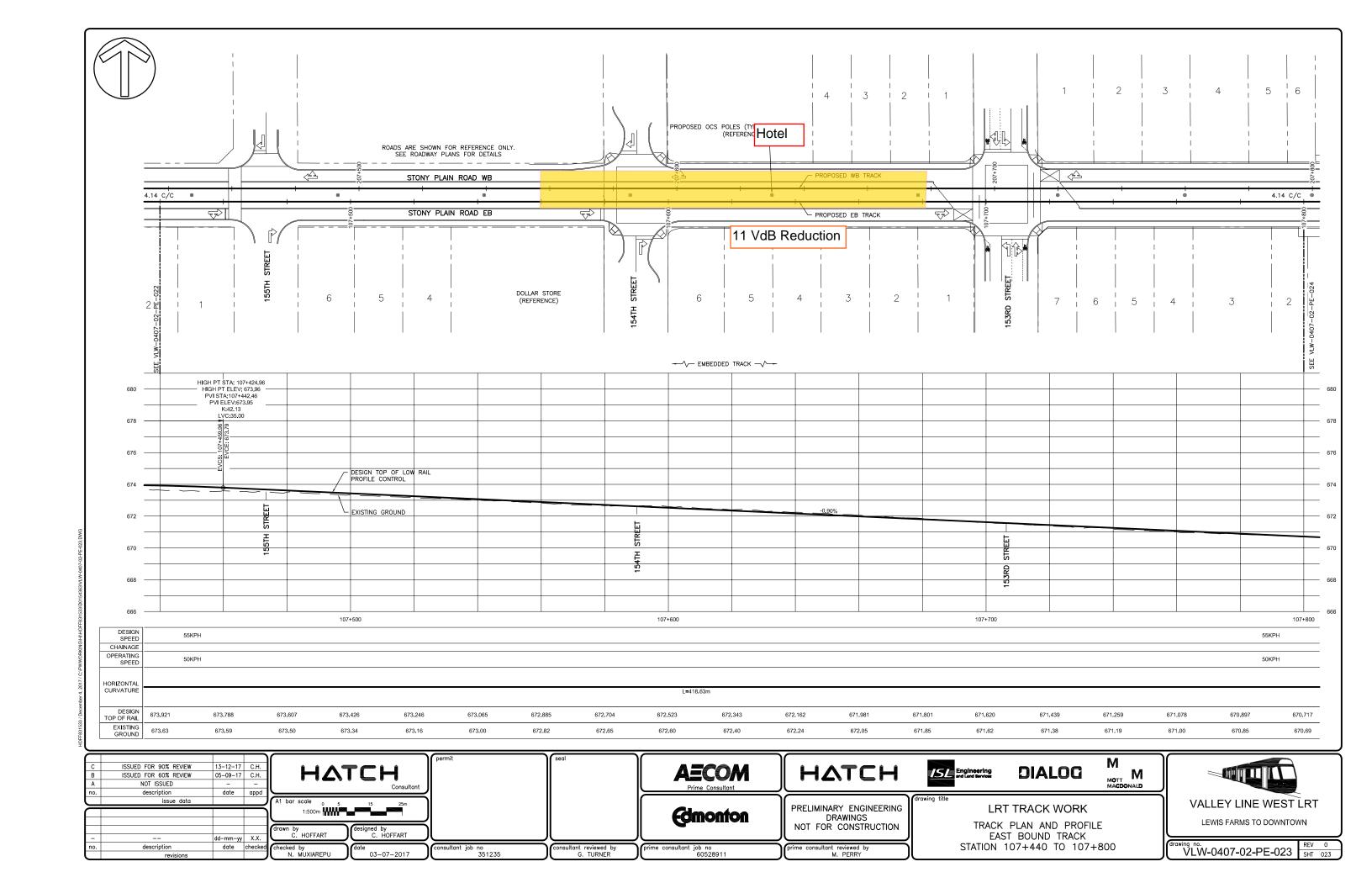


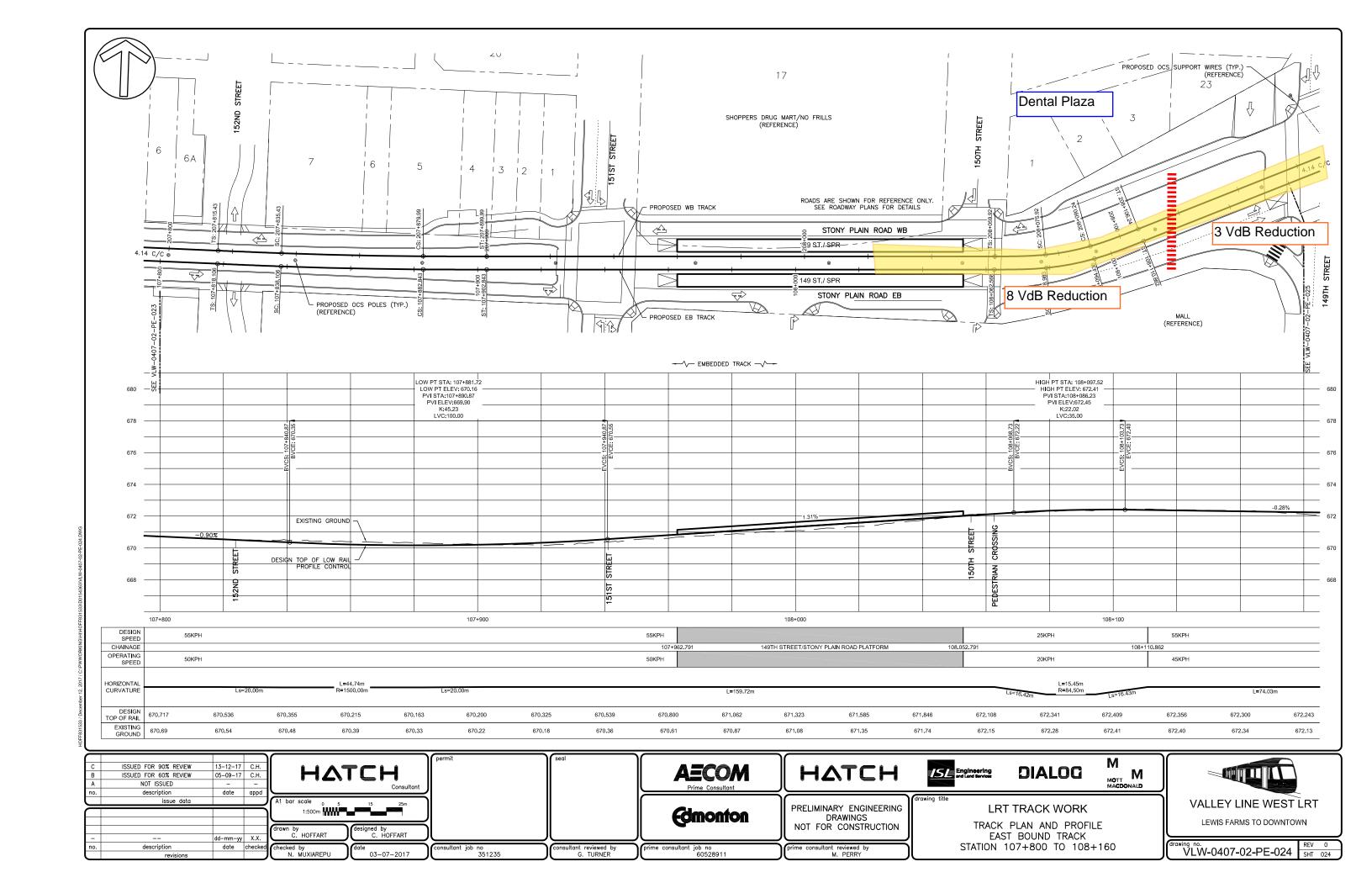


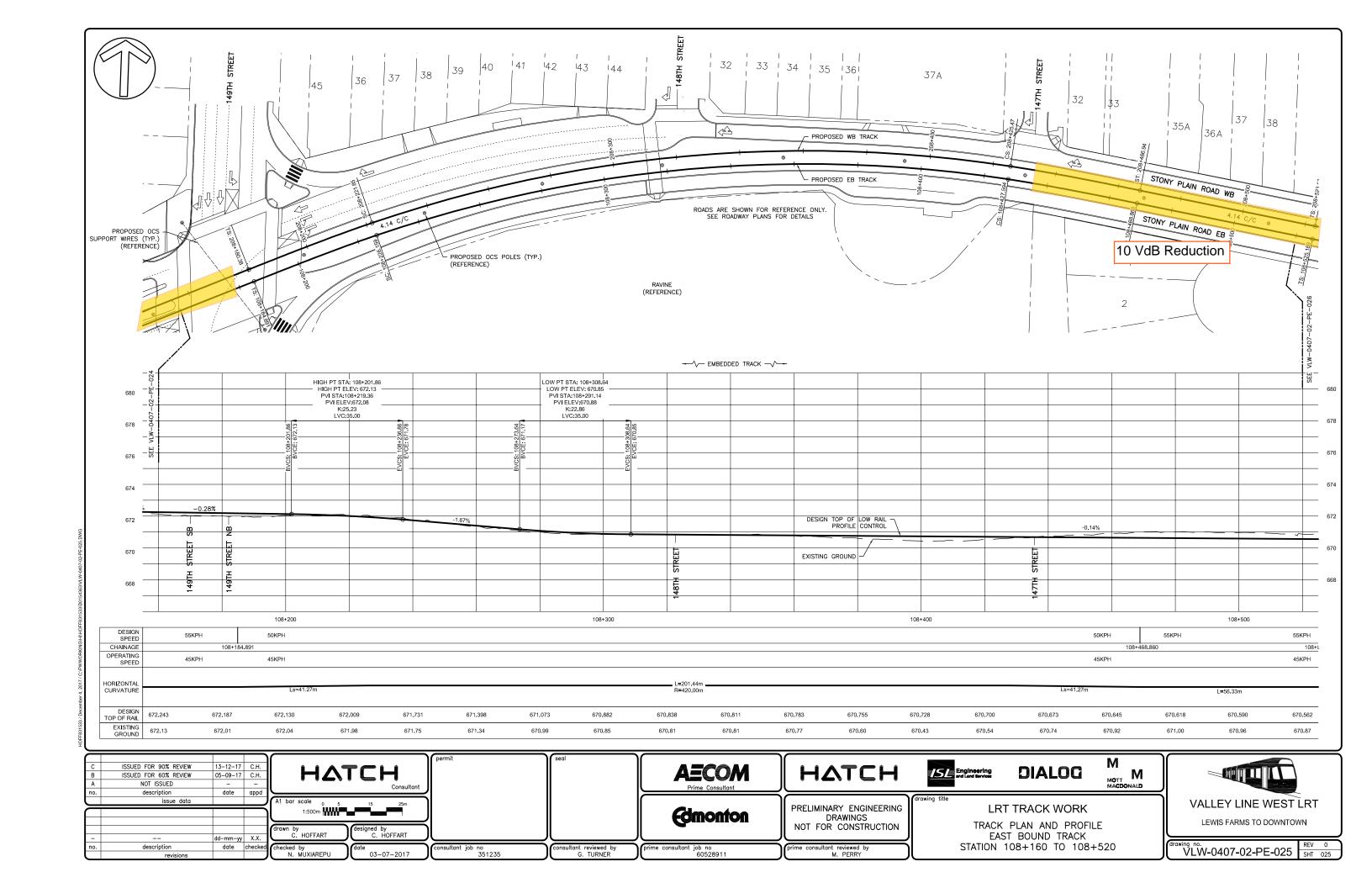


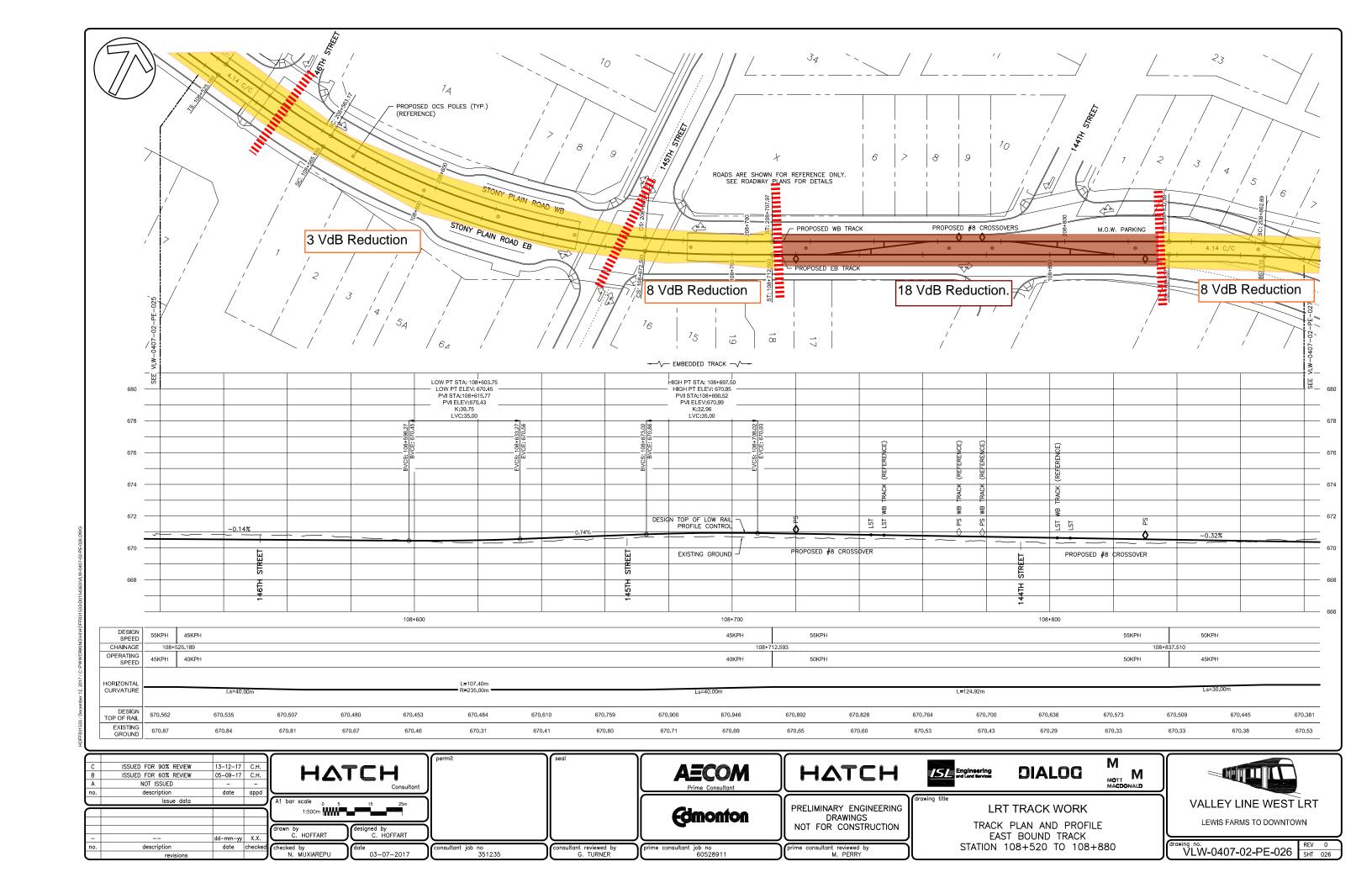


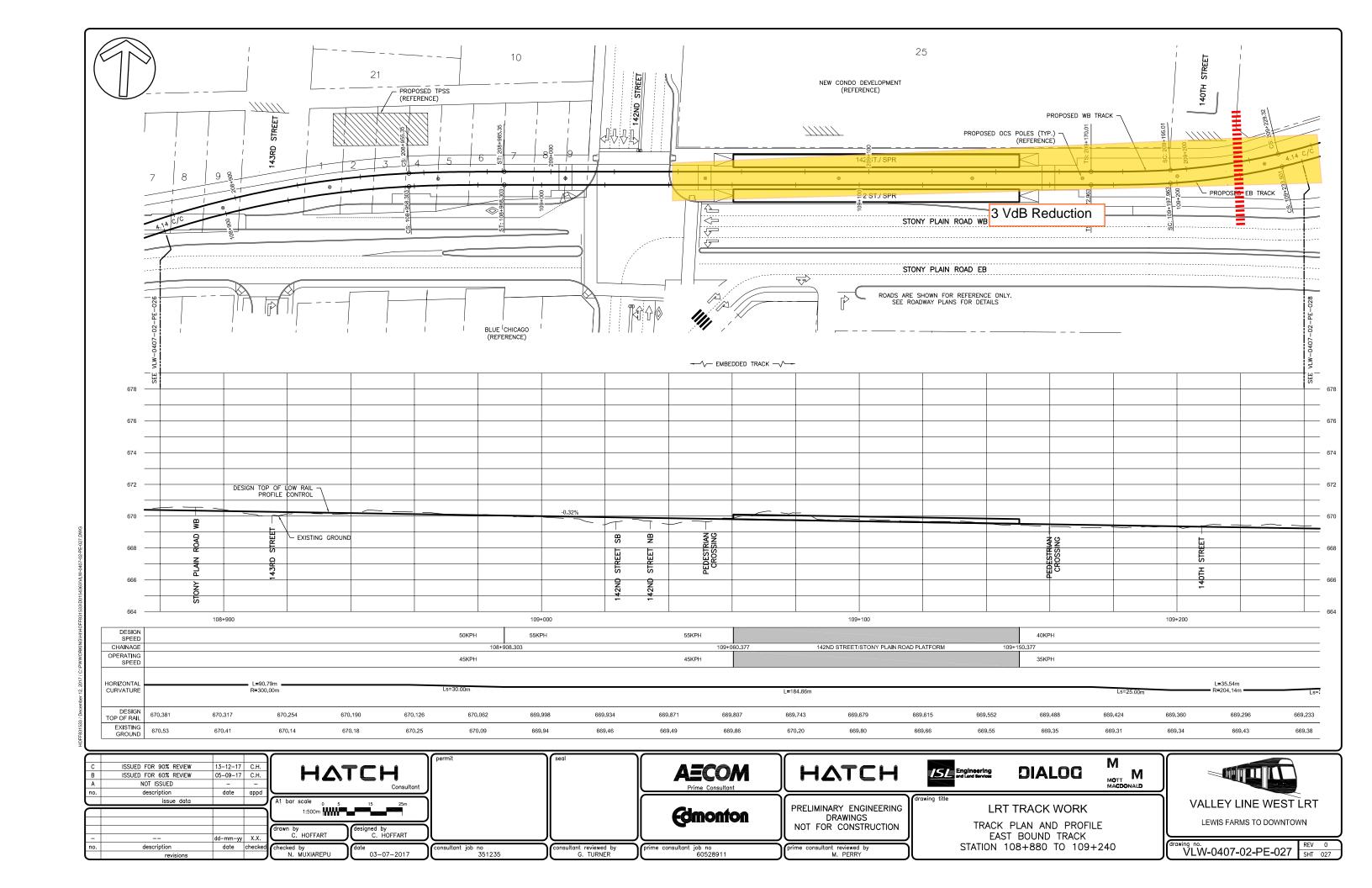


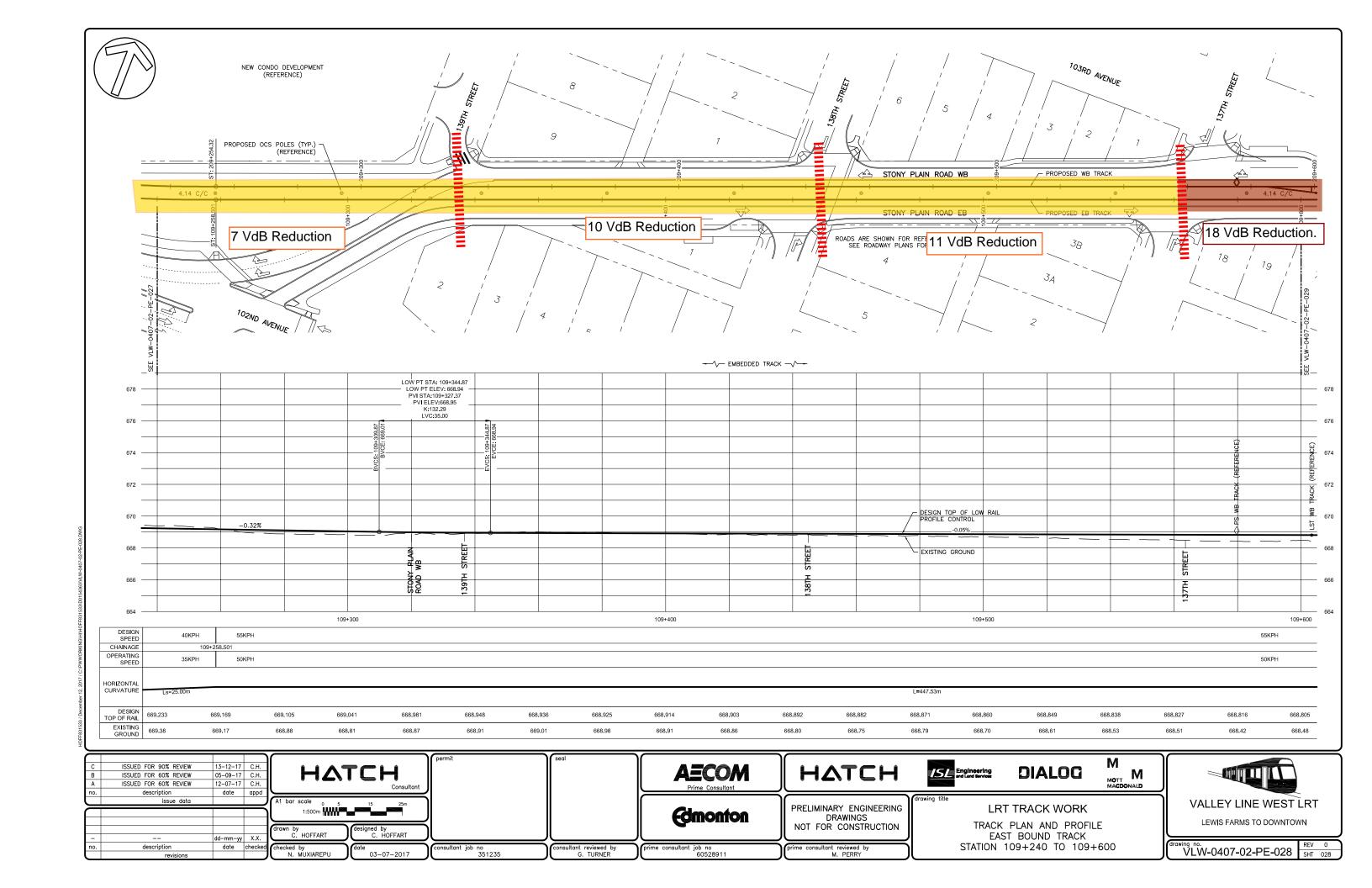


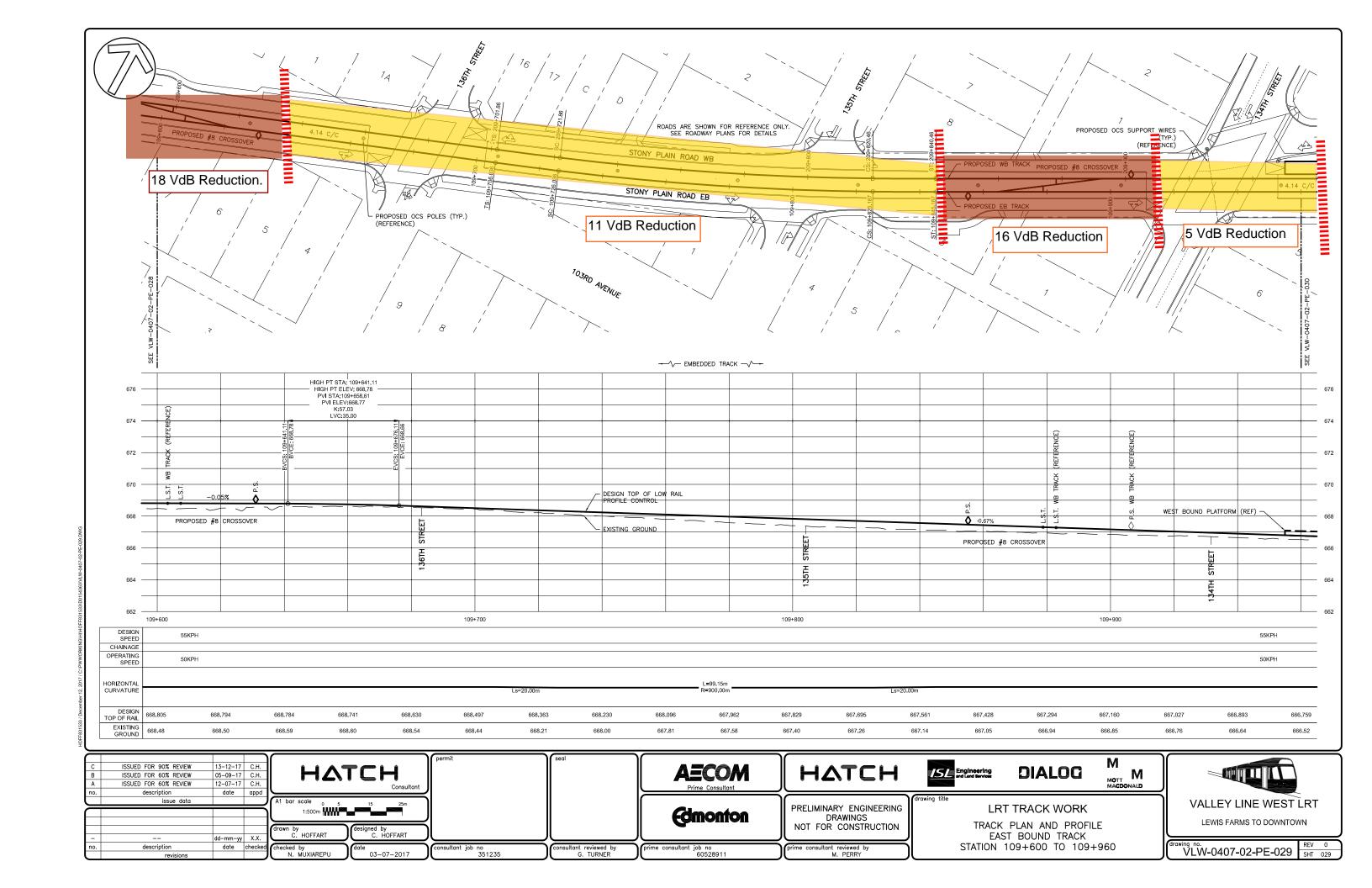


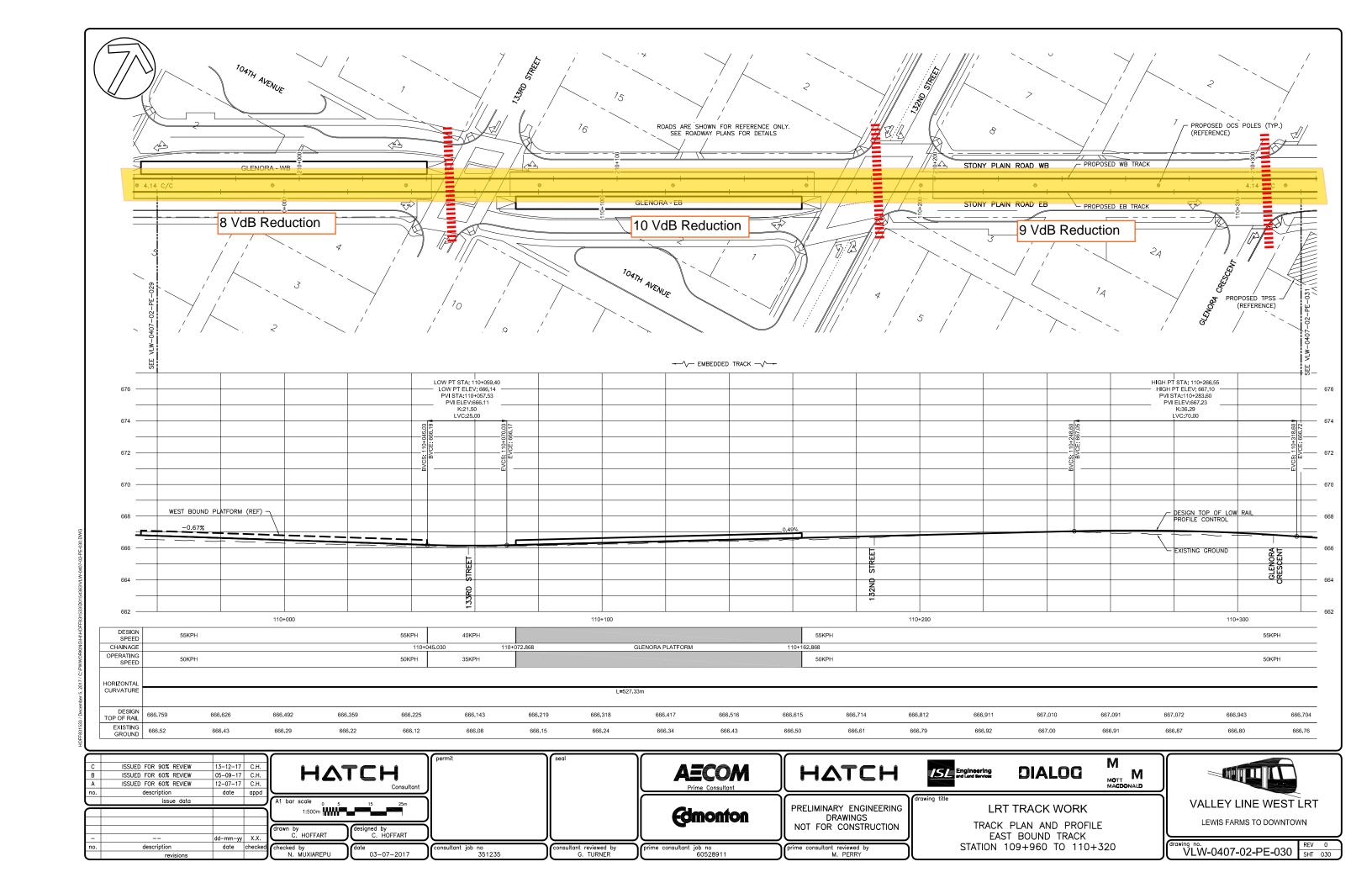


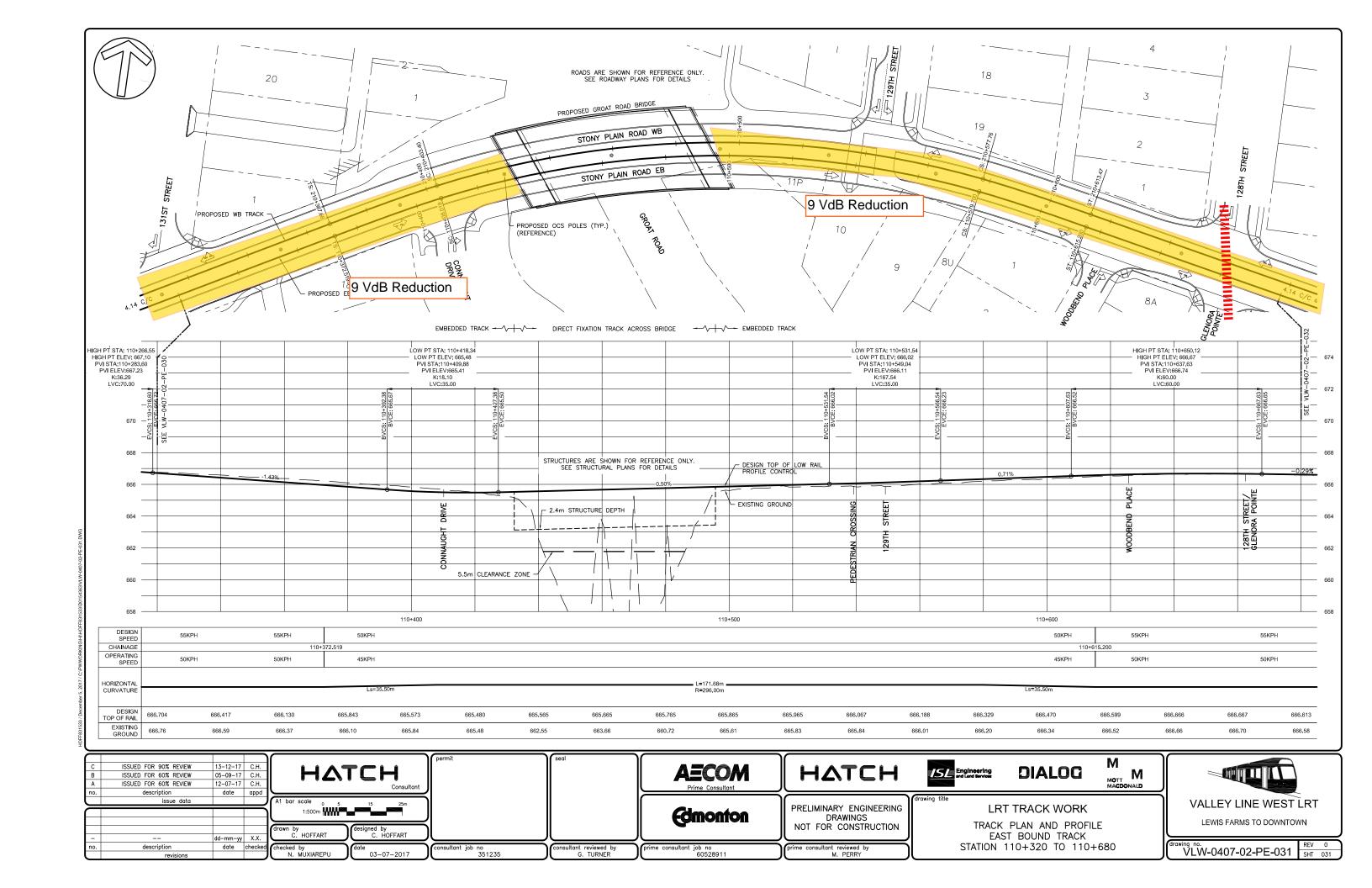


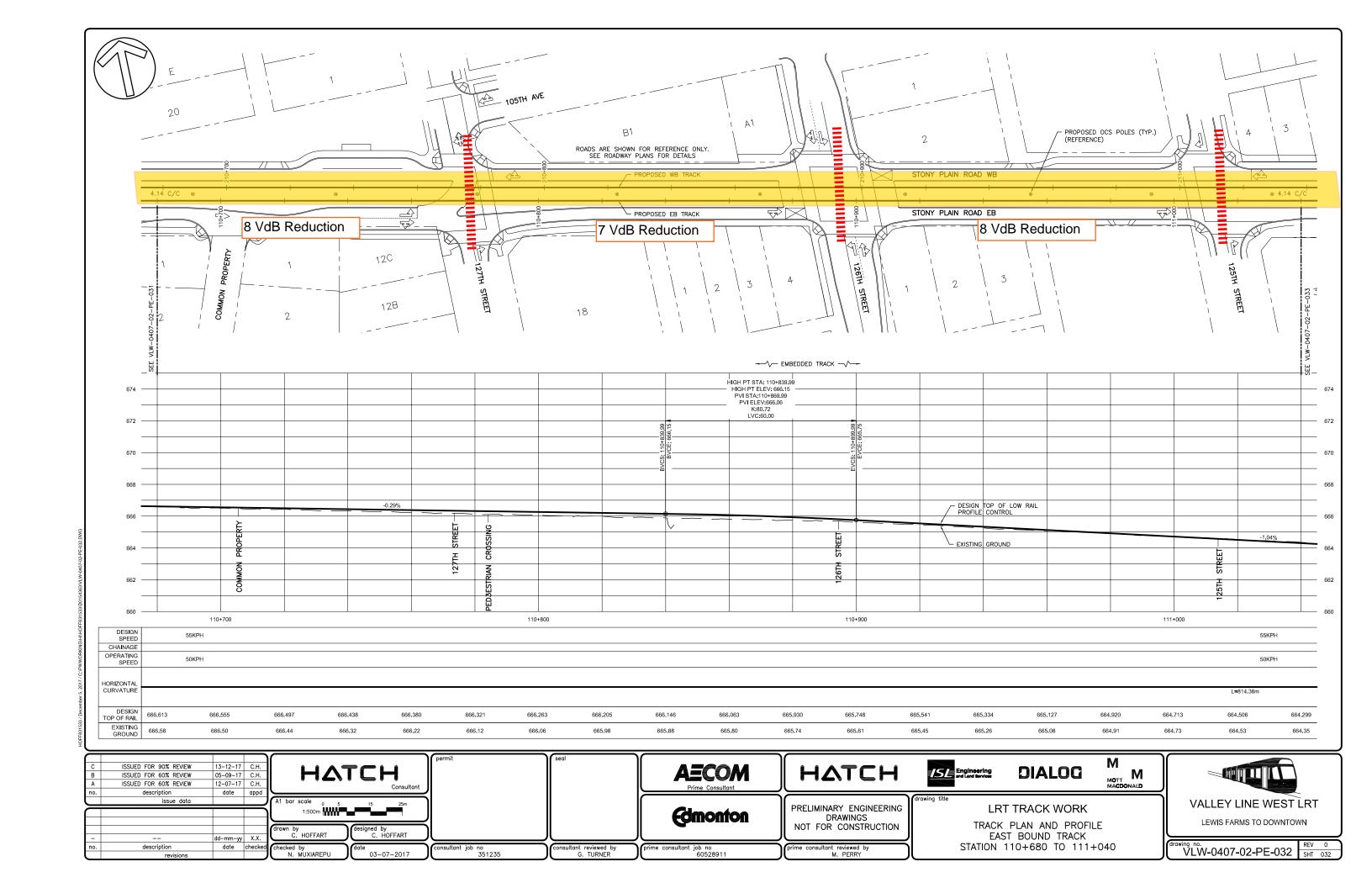


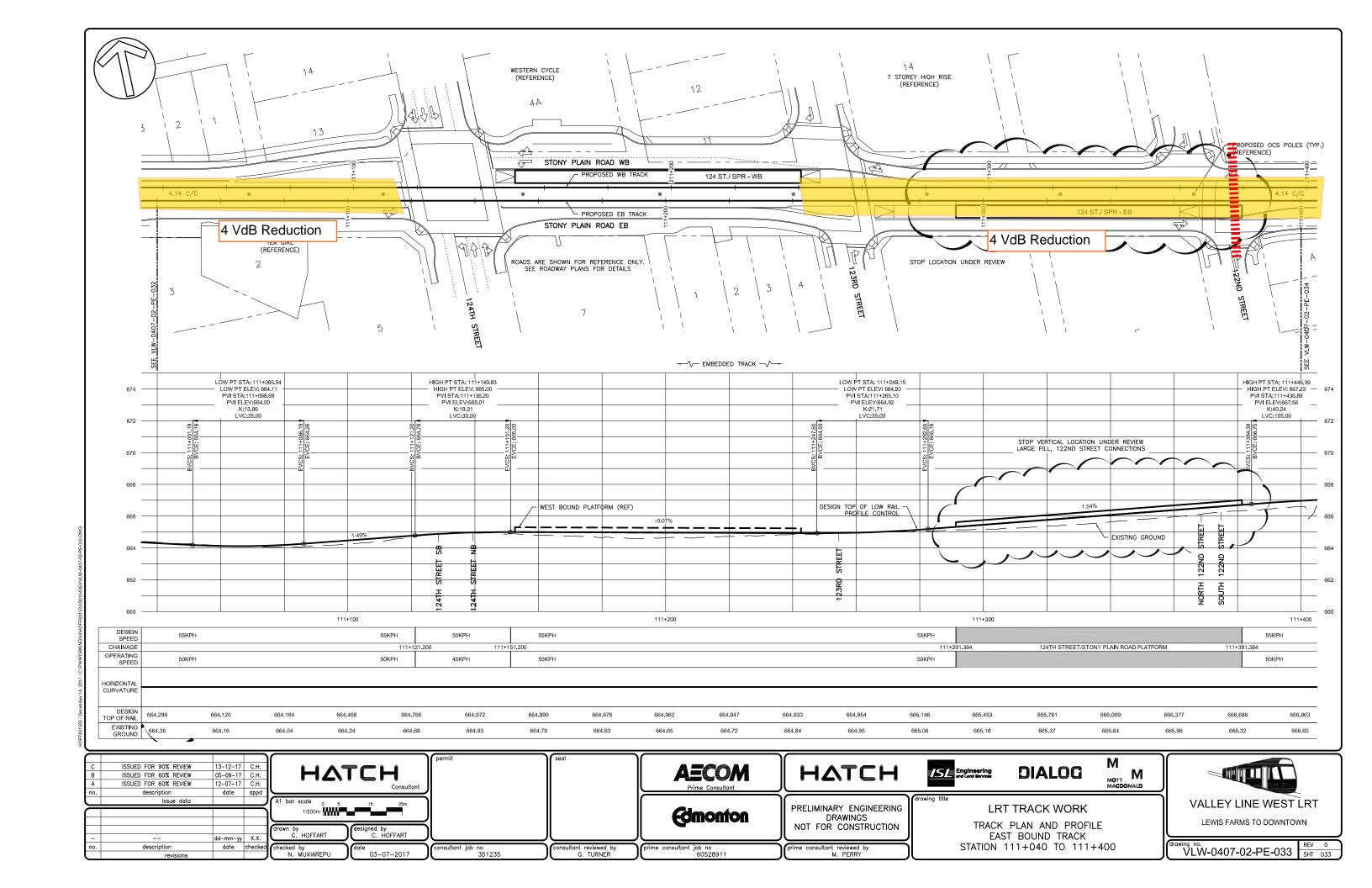


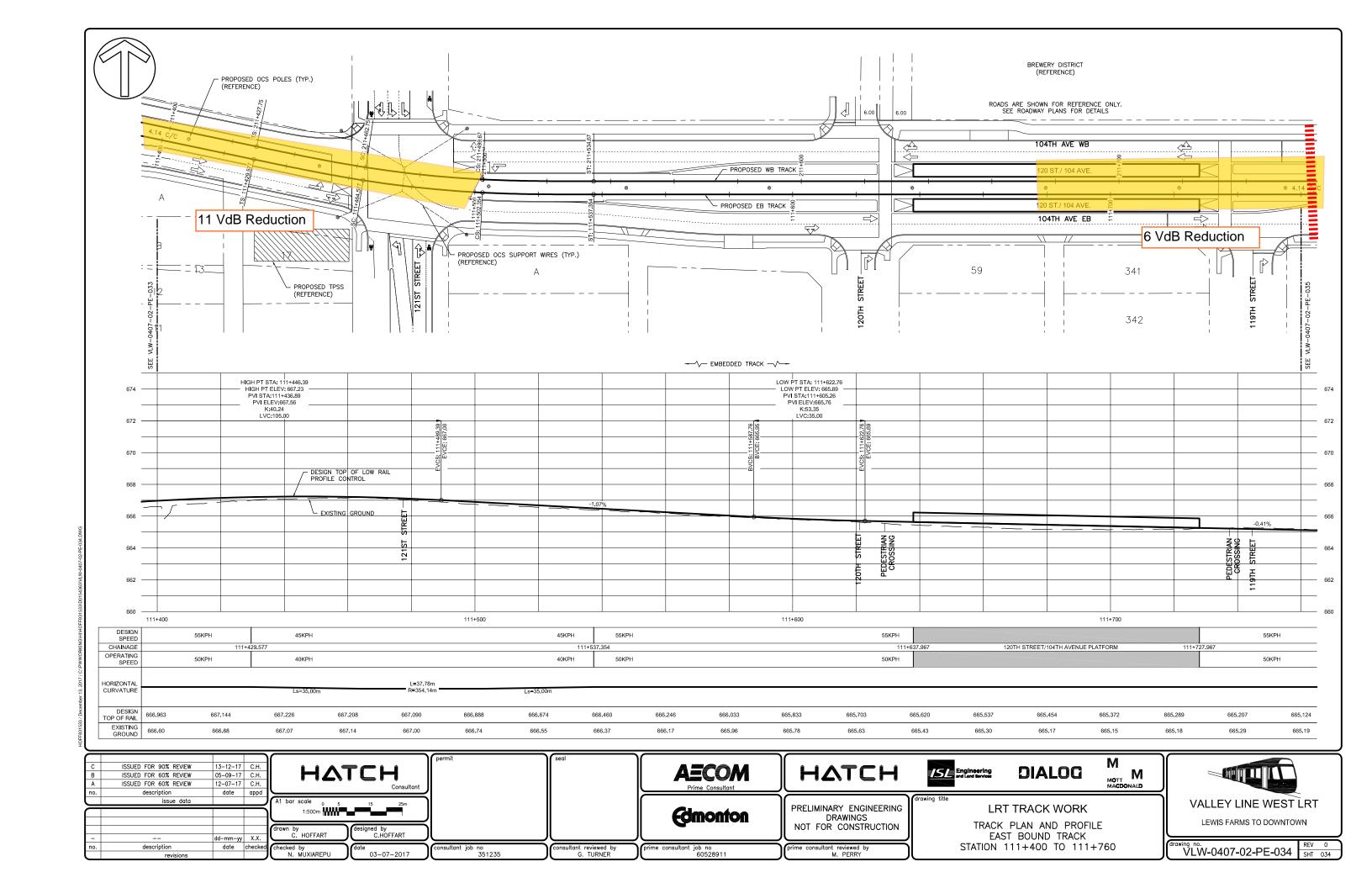


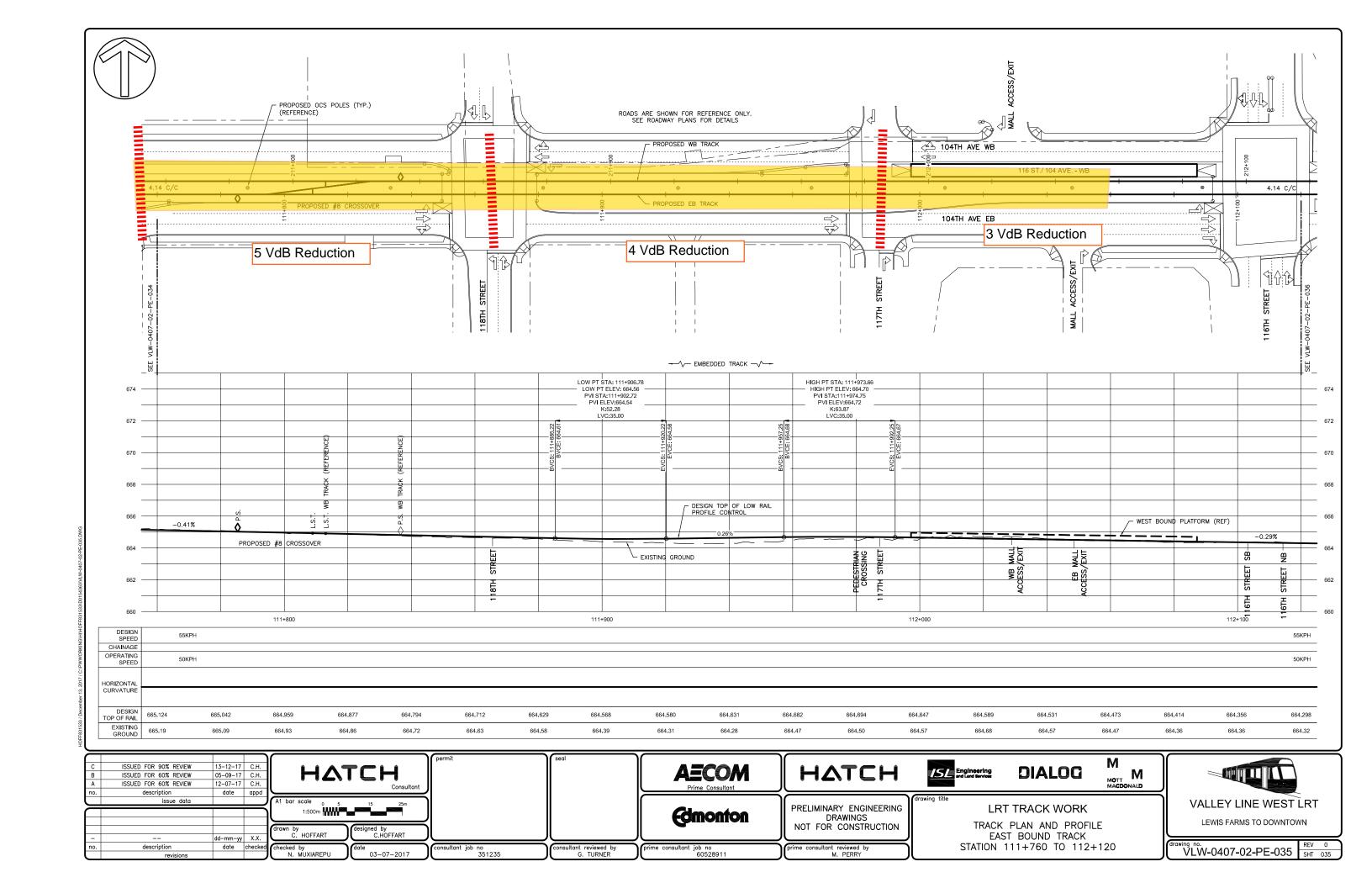


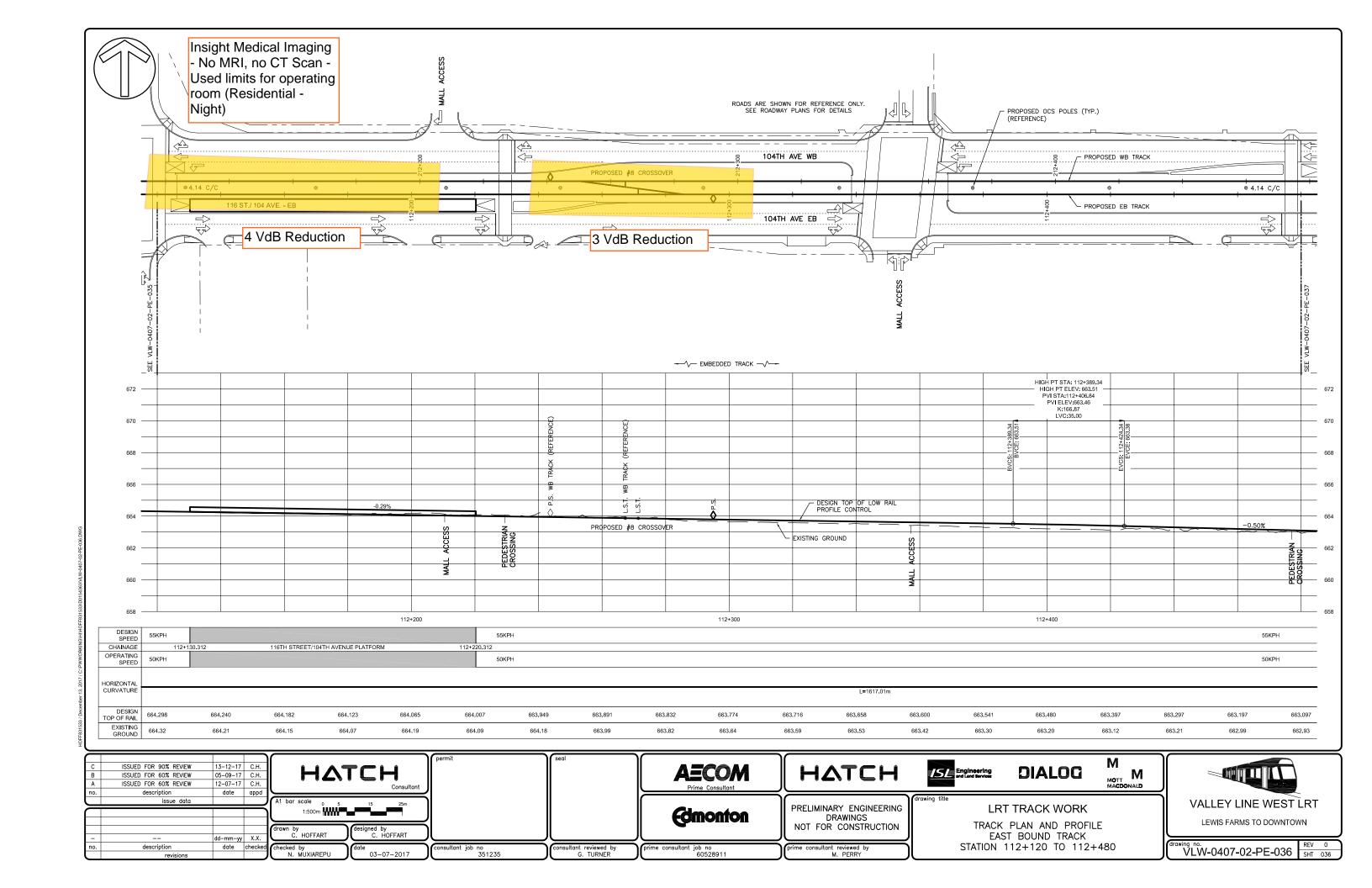


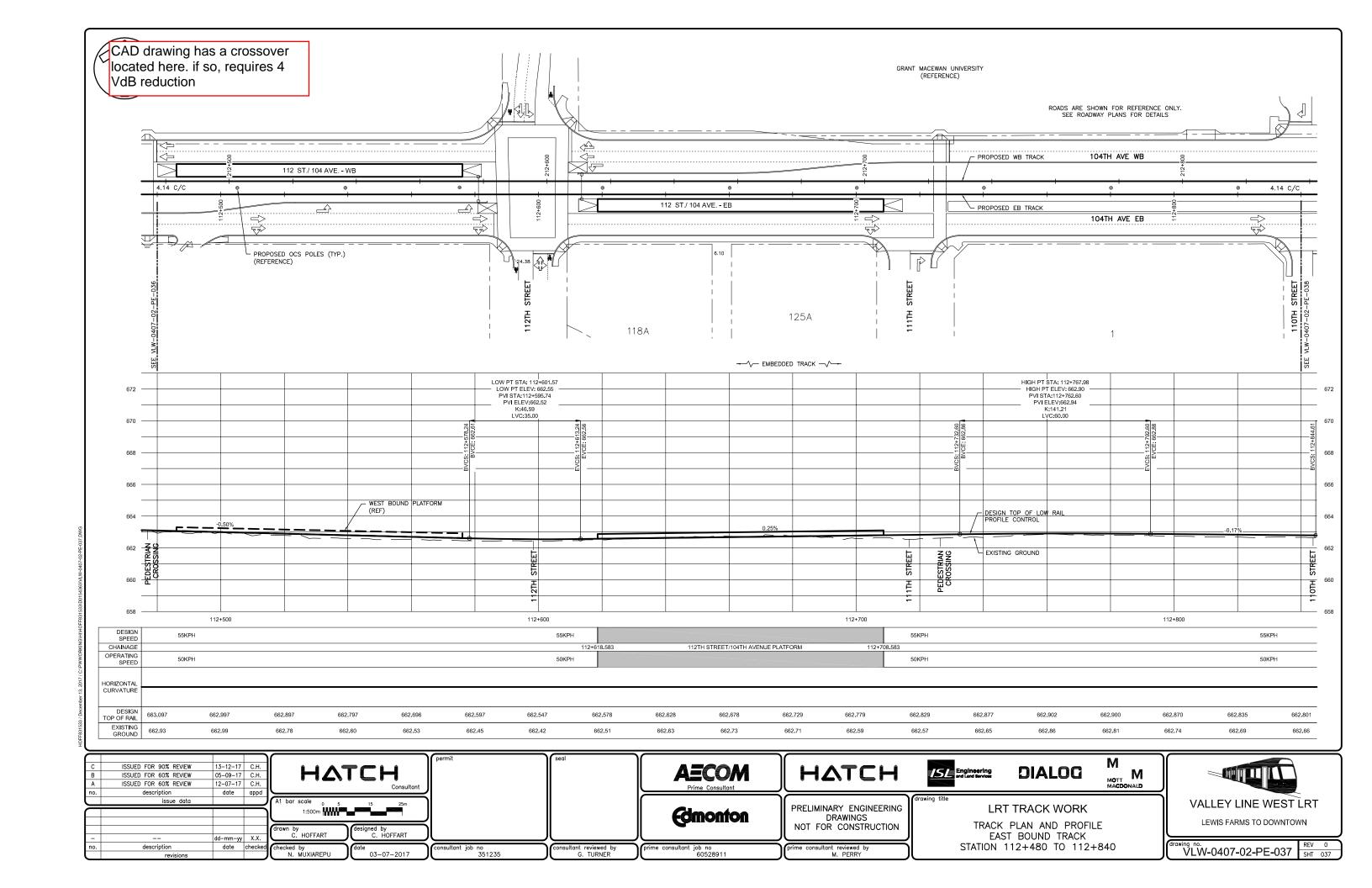


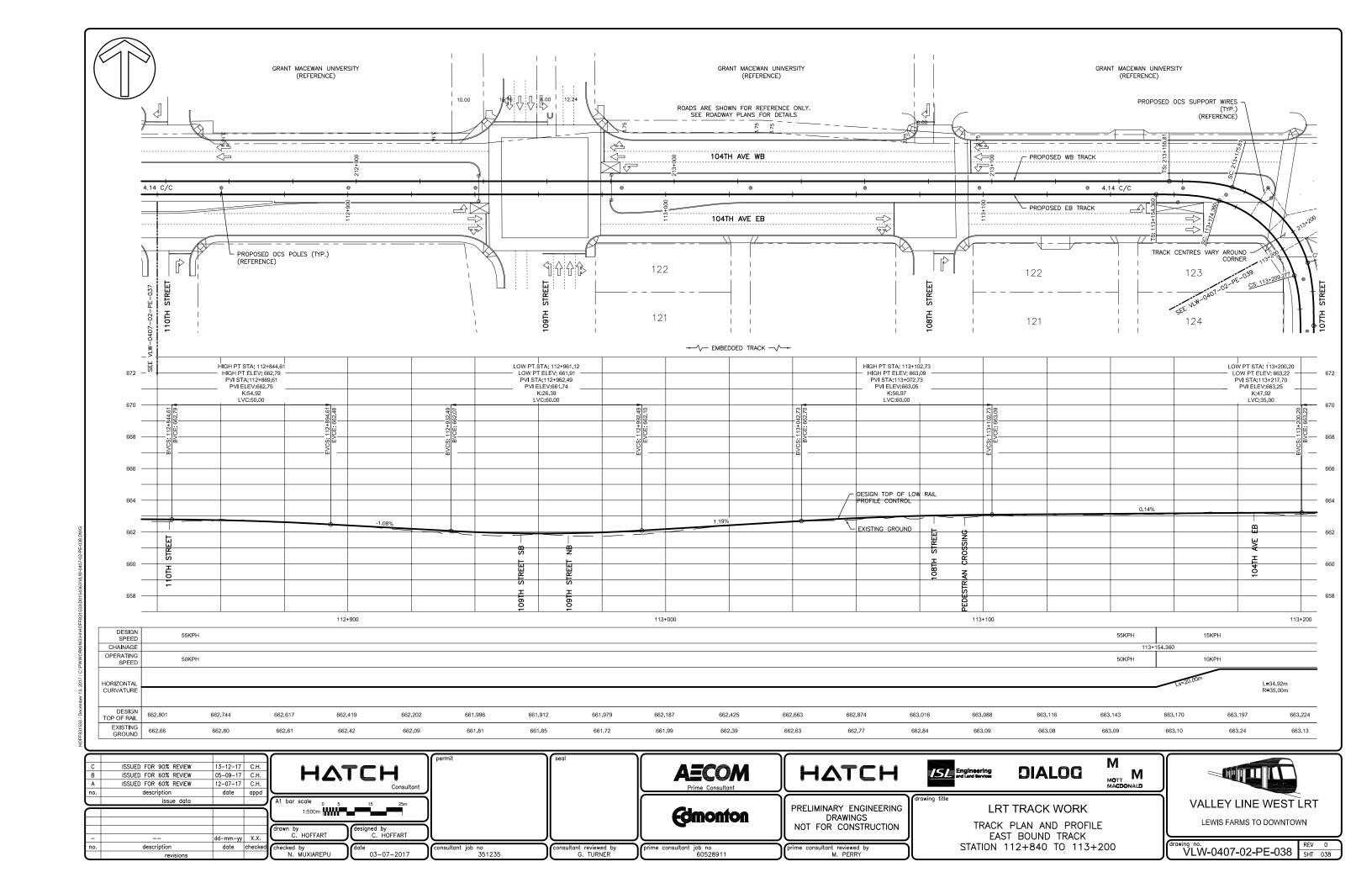


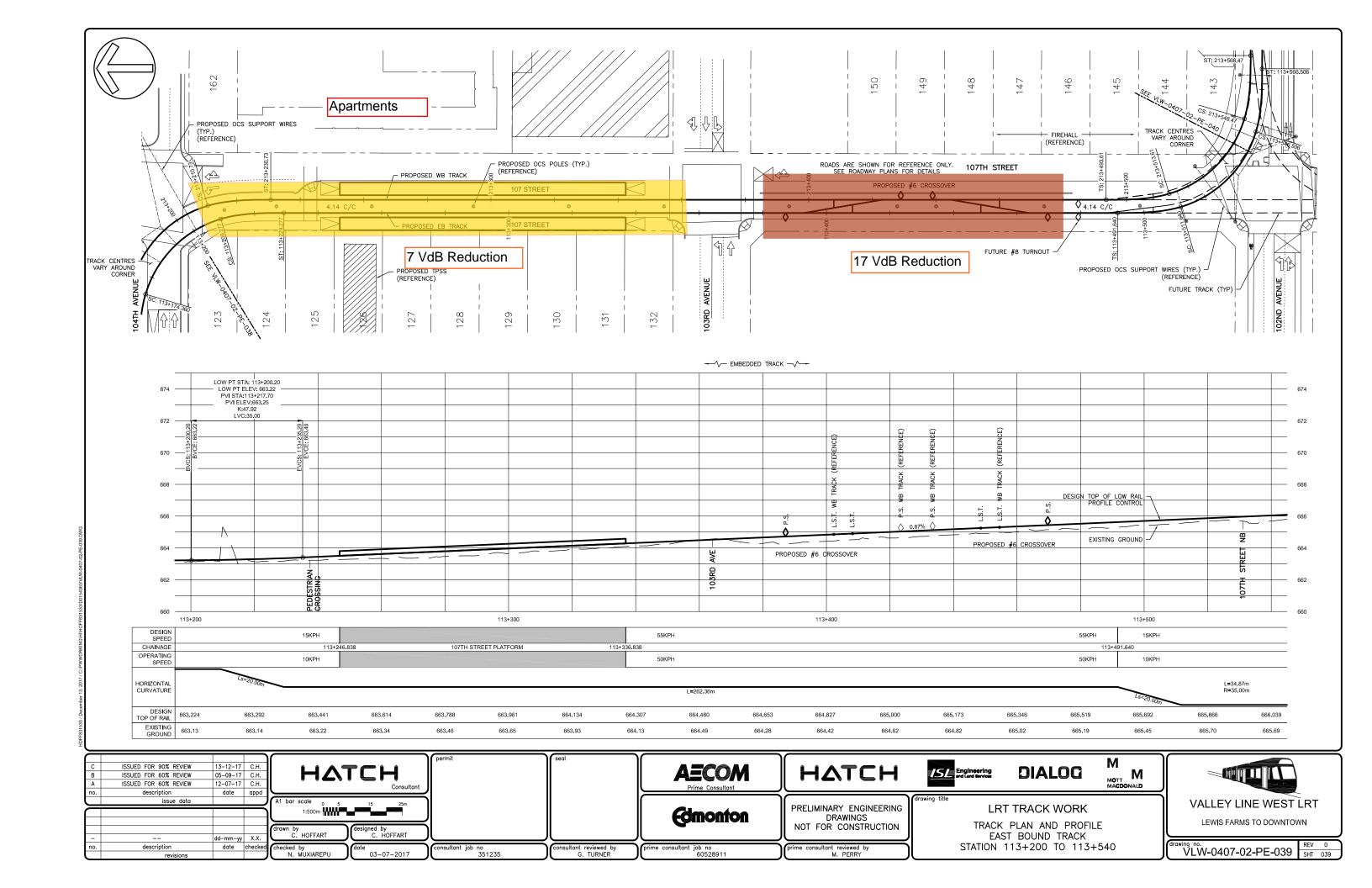


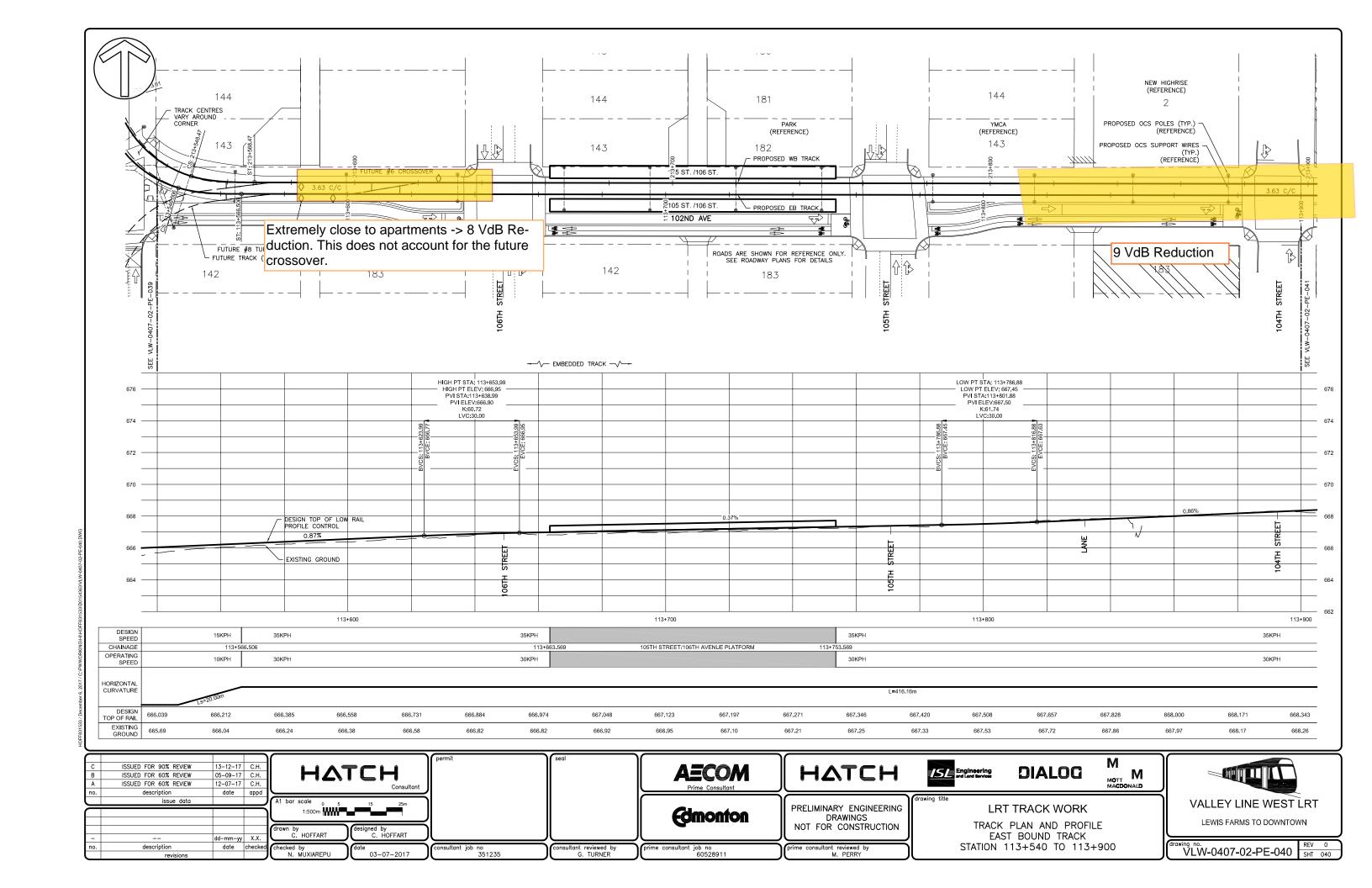


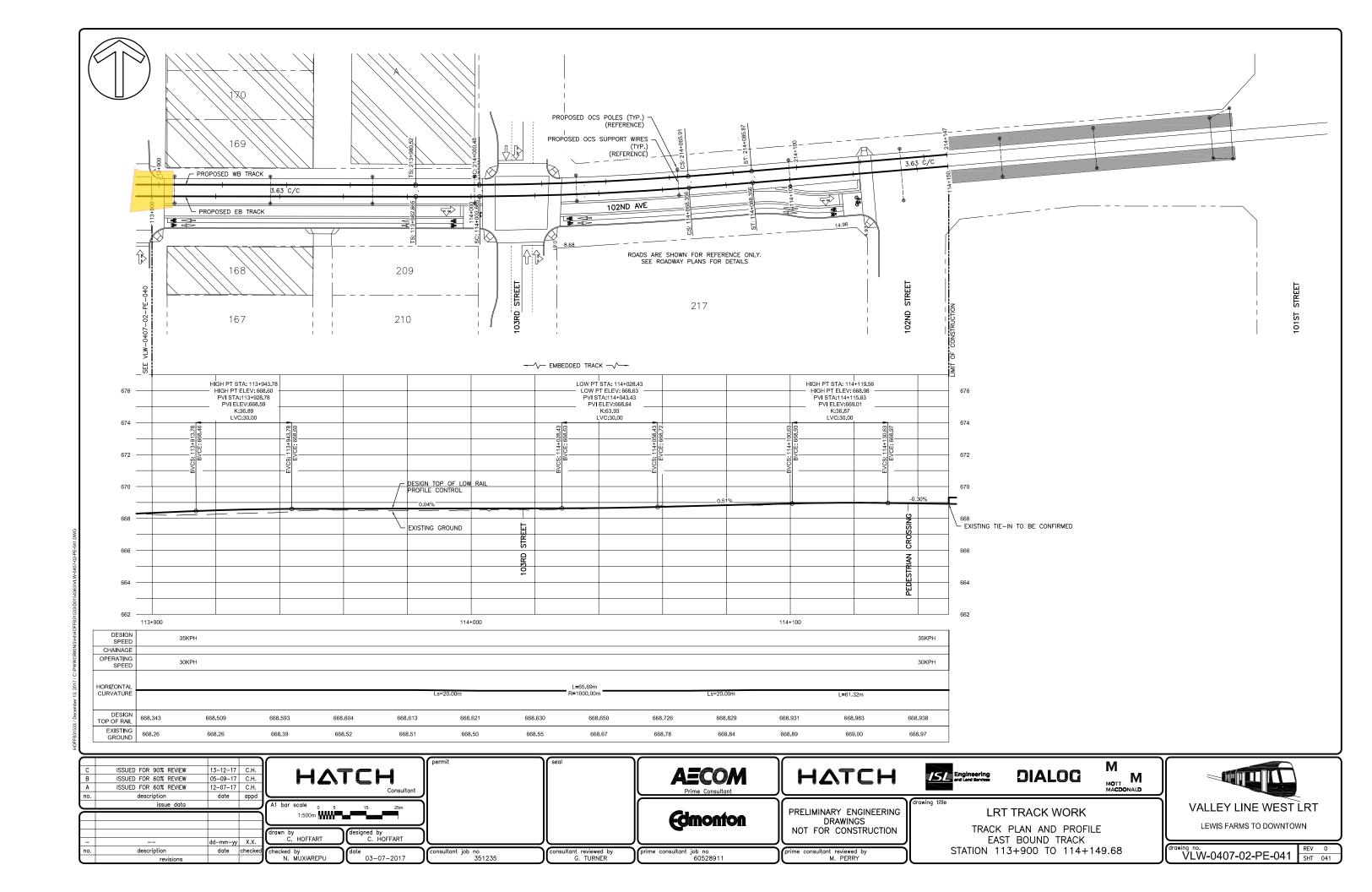












GROUND BORNE VIBRATION MITIGATION

Railway traffic is a source of ground borne vibration. Irregularities and imperfections in the rails and wheels produce dynamic vehicle track interaction forces that in turn generate stress waves in the supporting soil. Stress waves in the soil interact with foundations of adjacent buildings causing them to vibrate. This causes the floors, walls and ceilings to vibrate. Worn (or flat) wheels and tracks will increase vibration levels. Furthermore, special trackwork such as switches also increase the level of vibration. The impact from ground borne vibration from rail transit systems manifests in three main effects:

- Perceptible vibrations which are physically perceived by humans,
- Noise caused by vibrating items in buildings such as the rattling of windows and shaking of items on shelves or hanging on walls.
- Low frequency noises (rumbling noise or ground borne noise) caused by ground borne vibration radiating from vibrating room surfaces and perceived by the human ear as sound.

The key elements of the vibration environment can be described with the Source-Path-Receiver concept shown in Figure 1. The source of vibration is the train wheels rolling on the rails that create vibration energy transmitted through the tracks into the ground. The path taken by vibrations is through the ground and into nearby buildings. The receivers are people or vibration-sensitive activities in the buildings into which the vibrations pass. Vibrations are influenced by variables such as the:

- Speed of the train;
- Vehicle suspension;
- · Condition of the wheels and track;
- Track support system;
- Depth and geology of the soil layering;
- Construction of the track and tunnel;
- Depth of tunnel and distance away from it;
- Type and construction of the building where the receiver of the vibration is positioned;
- Interior acoustical absorption.

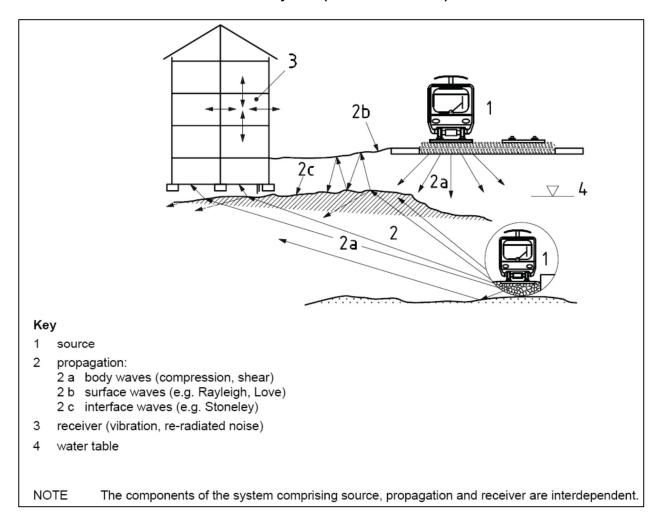
The purpose of vibration mitigation is to minimize the adverse effects that the project ground borne vibration will have on sensitive land uses. Following the Source-Path-Receiver concept, there are essentially three main mitigation strategies for vibration control:

- 1. Controlling vibration at the source: Reduction of noise and vibration at source can be achieved by isolating the track superstructure, eliminating the running surface discontinuities, regular maintenance of the rail running surface, regular wheel re-profiling, selecting the appropriate type of rail vehicle, and reducing the speed of rail vehicles. Rail vibration isolation can be achieved through the installation of resilient rail fasteners, resilient supported ties, booted ties, tire-derived aggregate, ballast mats or floating slabs. Such rail and track vibration isolation system increase the elasticity of the track superstructure and provide a reduction in transmitted vibration.
- 2. Controlling the transmission of vibration: Distance is one of the most effective mitigation measures against noise and vibration, although geological make-up and terrain also have an effect. Annoyance from railway vibrations is inversely proportional to distance from railway tracks. In new developments, locating the sensitive land use away from the railway lines can reduce vibration effects. For existing structures, ground vibrations from rail operations can also be reduced through the installation of trenches between the line and the receivers in a similar

manner to noise barriers. Trenches can be either left open or filled with an alternative material if open trenches are considered undesirable. Note that trenches would only be effective in reducing vibration from above ground (surface) rail operations and will not typically have any effect on vibration generated by underground railways.

3. Controlling vibration at the receiver: In some circumstances, it is practical to modify the impacted building to reduce the vibration levels. Special building methods can be used to modify ground-borne vibration being transmitted into the building structure such as isolation of foundation and footings using resilient elements and rubber bearing pads or springs. Vibration isolation of buildings generally consists of supporting the building foundation on elastomer pads similar to bridge bearing pads. This approach is particularly important for shared-use facilities such as office space above a transit station or terminal. Vibration isolation of buildings is rarely an option for existing buildings. Normal applications are possible only for new construction. Alternatively, the floor upon which the vibration-sensitive equipment is located could be stiffened and isolated from the remainder of the building or the equipment could be locally isolated from the floor and building.

Figure 1 Ground-borne Vibrations from Trains Example of Source, Propagation and Receiver System (Source: ISO 14837)



SYSTEM-WIDE OPERATIONAL VIBRATION MITIGATION

One of the most effective forms of ground borne vibration mitigation is to attempt to reduce vibration at the source. Source vibration reduction can be normally accomplished through vehicle specifications. There are several additional operational measures that can reduce vibration levels at the source. Table A provides a list of operational and maintenance measures that should be performed on a regular basis and the benefit that each of the measures would provide. It is recommended to implement a system wide vibration reduction strategy as shown in Table A. These strategies are effective in reducing the vibration generation in the first space. For example, problems with rough wheels or rails can increase vibration levels by as much as 20 VdB in extreme cases, negating the effects of even the most effective vibration control measures. It is rare that practical vibration control measures will provide more than 15 to 20 VdB attenuation. Therefore, maintenance procedures can significantly reduce ground borne noise and vibration.

Table A: System-Wide Light Rails Operational Mitigation

Operational Measure	System Benefit
Rail Grinding and Replacement	As rails wear, both noise and vibration levels from light rail operations can increase. By grinding or replacing worn rails, noise and vibration levels will remain at the projected levels. Rail grinding or replacement is normally performed every 3 to 5 years.
Wheel Truing and Replacement	Wheel truing is a method of grinding down flat spots (commonly called "wheel flats") on the vehicle wheels. Flat spots occur primarily because of hard braking. When flat spots occur they can cause increases in both the noise and vibration levels produced by the light rail vehicles.
Vehicle Specifications and Maintenance	Rail vehicle should have low unsprung weight, soft primary suspension, minimum metal-on-metal contact between moving parts of the truck (bogie), and smooth wheels that are perfectly round. A limit for the vertical resonance frequency of the primary suspension should be included in the specifications for any new vehicle. Vehicle maintenance includes performing scheduled and general maintenance on items such as suspension system, brakes, wheels, and slip-slide detectors. Keeping the mechanical systems on the light rail vehicles in top condition will also help to maintain the projected levels of noise and vibration.
Operator Training	Operators should be trained to operate light rail vehicles at speeds to avoid "hard-braking," which can cause wheel flats and damage the track. Furthermore, by training operators to identify potential wheel flats and other mechanical problems with the trains, proper maintenance can be performed in a timely manner.

Operational Measure	System Benefit
Location and Design of Special Trackwork	Turnouts are a major source of vibration impact when they are located in sensitive areas because the impacts of vehicle wheels over rail gaps at track turnout locations increases ground borne vibration by about 10 VdB. Careful review of crossover and turnout locations during the preliminary engineering stage to minimize potential vibration impacts. When feasible, relocate special trackwork to a less vibration-sensitive area. If turnouts cannot be relocated away from sensitive areas, install spring frogs to eliminate gaps at crossovers and help reduce vibration levels.

SITE SPECIFIC VIBRATION MITIGATION MEASURES

In addition to the overall strategy a number of methods have been developed to control ground-borne vibrations. Vibration is generally treated by reducing the dynamic forces associated with the source or with isolation techniques. The source may be isolated from the ground or structure, thereby reducing vibration propagation towards receiver buildings. Another alternative is to make adjustments to the vibration transmission path by the use of trenches to control ground borne vibration, to reduce surface waves, analogous to controlling airborne noise with sound barriers. Alternatively, structures and buildings may be isolated from sources.

The actual values of building vibration induced by sources are a function of the vibration characteristics of the source, ground conditions, building foundations and building construction material and techniques. To be effective, all of these measures must be optimized for the frequency spectrum of the vibration. The common vibration mitigation methods are presented in Table B. Given that the track and vehicles are in good condition, the options for further reductions can be achieved by implementing one or more of the listed measures on specific segments of the alignment where it is needed. The reduction in ground borne vibration provided by these measures is strongly dependent on the frequency content of the vibration, soil properties and the design and support of the track. Different conceptual vibration isolating track designs are depicted in Figure 2. The degree of vibration impact will determine the extent of mitigation required and the mix of vibration control measures to be adopted as a mitigation strategy.

Where vibration mitigation affects stiffness of the track support (ex. Ballast mats), the static deflection of the track under the load of the train will be greater than the static deflection of conventionally supported track. At the connections to standard track, some sort of smooth transition is required in order to avoid impulsive forces that could be very damaging to the subgrade, and cause impulsive ground vibration, discomfort to passengers and rapid fatigue damage to the track components themselves.

Table B: Site specific Vibration Mitigation Measures

Mitigation Measure	Description
Ballast Mats	A ballast mat consists of a rubber or other type of elastomer pad that is placed under the ballast. Depending on the soil properties, an asphalt or concrete layer under the ballast may be required. Ballast mats are less effective if placed directly on the soil or the sub-ballast. Most applications of this procedure are found in tunnels or on bridges. Ballast mats can provide 10 to 15 VdB attenuation at frequencies above 25 to 30 Hz.

Mitigation Measure	Description
Resilient Rail Fasteners	Resilient fasteners are used to fasten the rails to the ties or to the concrete track slabs. By making use of fasteners that are less stiff in the vertical direction, it is possible to reduce the ground-borne vibration by as much as 4 to 8 VdB at frequencies above 30 to 40 Hz. Premium fasteners cost approximately \$300 per track-foot, about 6 times the cost of standard fasteners.
Resilient supported sleepers/ties	Resiliently supported tie systems involve attaching thick rubber pads directly to the underside of ties in ballast. By making use of rubber pads between the ties and the foundation it is possible to reduce the vibration by at least 10 VdB. The rails are fastened directly to the concrete ties using standard rail clips.
Booted sleepers/ties	Booted sleeper systems consist of concrete sleepers surrounded by elastic boots that are molded into the concrete slab of the track. These perform in the same way as resilient supported sleepers/ties but the design is integrated with a slab track. They are particularly appropriate for transit systems with vibration problems in the 20 to 30 Hz range and are typically effective in reducing vibration by 10 VdB.
Tire-Derived Aggregate	Also known as shredded tires, a typical Tire-Derived Aggregate (TDA) installation consists of an underlayment of 300 mm of nominally 75 mm size tire shreds or chips wrapped with filter fabric, covered with 300 mm of sub-ballast and 300 mm of ballast above that to the base of the ties. This type of mitigation can only be used on ballast and tie track. Tests suggest that the vibration-attenuation properties of this treatment are midway between that of ballast mats and floating slab track. While this is a low-cost option, it has only recently been installed on two U.S. light rail transit systems—in San Jose and Denver—and its long-term performance is unknown.
Floating slab track	Floating slabs consist of a "floating concrete rail slab" sitting within a concrete trough separated by an elastic quality polyurethane foam sheet or other resilient material. The slab and sheet act as a light mass spring system.
	In high load situations, or where a high reduction in vibration is required, the ROW slab can be supported by resilient pads (or steel coil springs) on a concrete foundation. This second engineered option is more expensive and generally used in very specific circumstances.
	The tracks are then mounted on or within the floating slab depending on the need for direct fixation or embedded rail. Vibration mitigation can be improved by selecting isolation materials for the rail fixing. This mitigation method may provide up to a 15 VdB reduction in vibration. The design frequency of typical continuous or double-tie floating slabs is 16Hz. However, the isolation frequency of low-frequency floating slabs may be on the order of 5 – 8Hz.

Mitigation Measure	Description
	Associated schematic of a typical Light Mass Spring System
	Calculation of Insulation Loss for Light-Mass-Spring-System 25 20 15 10 15 10 15 4 5 6.3 8 10 12.5 16 20 25 31.5 40 50 63 80 100 125 160 200 Frequency in Hz Associated schematic of a typical Light Mass Spring System
Trenches	A trench can be an effective vibration barrier if it changes the propagation characteristics of the soil. It can be open or solid. Open trenches can be filled with materials such as styrofoam. Solid barriers can be constructed with sheet piling, rows of drilled shafts filled with either concrete or a mixture of soil and lime, or concrete poured into a trench.

Mitigation Measure	Description
Building Modifications	For existing buildings, if vibration-sensitive equipment is affected by train vibration, the floor upon which the vibration-sensitive equipment is located could be stiffened and isolated from the remainder of the building. For new buildings, the building foundation should be supported by elastomer pads similar to bridge bearing pads.
Embedded Rail	Embedded rail is set into the surface of the right of way (ROW). The system generally consists of a concrete slab with a rubber booted rail cast within the slab itself. More traditionally, in freeze thaw conditions, the rail is set into a rebated pocket in the concrete and the pocket is filled with a polyurethane grout. Both the rubber booted option and the polyurethane grout options inherently reduce vibration by acting as a floating track. Performance varies depending on the supplier of the embedded rail system.
	Associated schematic of a typical embedded rail detail
Flange Bearing Frog	Flange bearing frogs (FBF), or jump frogs, have been successfully used to reduce both noise and vibration by enabling the wheel's flange to run along the frog groove, thus lifting the train tread off the rail as it progresses past the rail gap at the switch point location. Although historically used in rail yards, the FBF is becoming more commonly used in light rail mainline operations when speed and geometry permits.
	Associated schematic of a typical Flange Bearing Frog

Figure 2 Different conceptual vibration isolating track designs (Source: ISO 14837)

